



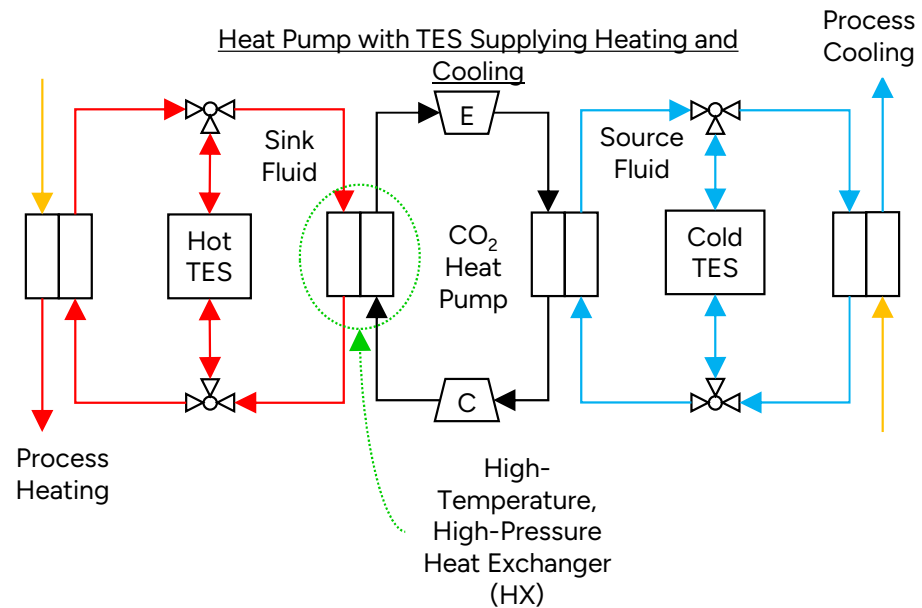
# Impact of Cooling Fluid on the Design and Performance of a Supercritical CO<sub>2</sub> Heat Exchanger for Applications in High-Temperature Heat Pumps

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# Introduction: Motivation

- High industrial energy consumption for heating and cooling
- Potential of high-temperature heat pumps (HTHPs) with thermal energy storage (TES) for decarbonization
- CO<sub>2</sub> as a working fluid
- Importance of heat sink design



# Introduction: Heat Exchanger Types

Printed Circuit Heat Exchanger (PCHE)

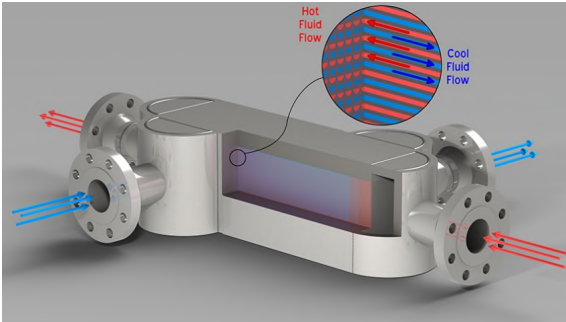


Image source: <https://www.vpei.com/diffusion-bonded-microchannel-heat-exchangers/>

Plate and Fin Heat Exchanger (PFHE)

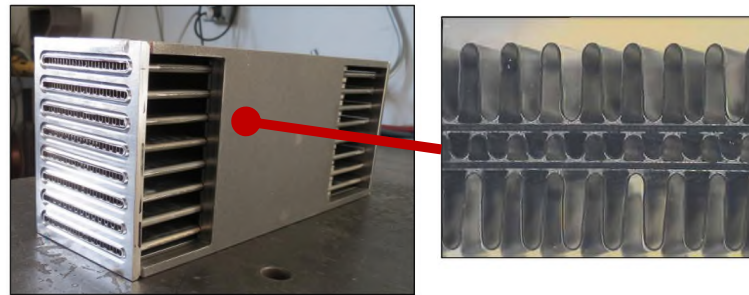


Image source: [21]

Shell and Tube Heat Exchanger (STHE)

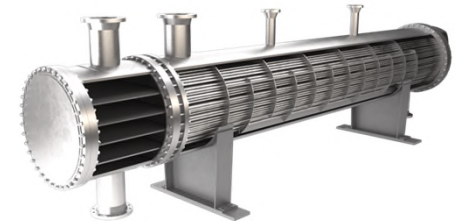


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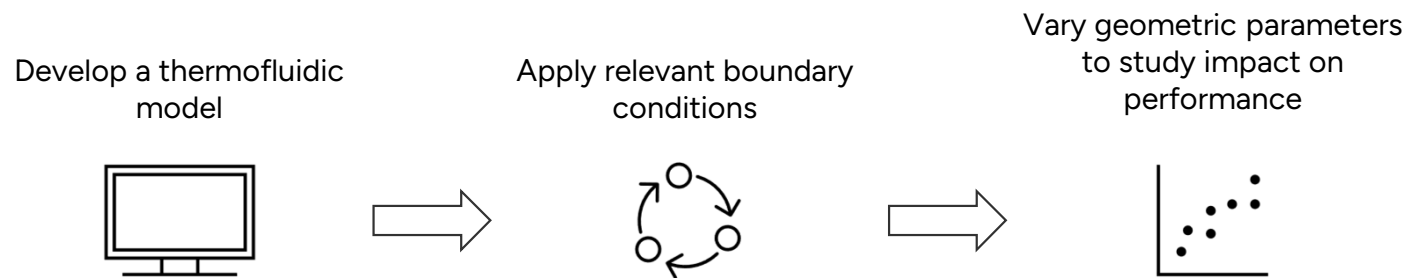


# Introduction: Sink Fluids

- Thermal oil
  - + Suitable for high temperature, low pressure operation
  - Higher cost
  - Flammability
- Molten salt
  - + Suitable for high temperature, low pressure operation
  - + Potential to serve as TES
  - Higher cost
  - Corrosiveness
- Air
  - + Safe, nontoxic
  - + Readily available
  - Poor heat transfer performance



# Methodology: Overview





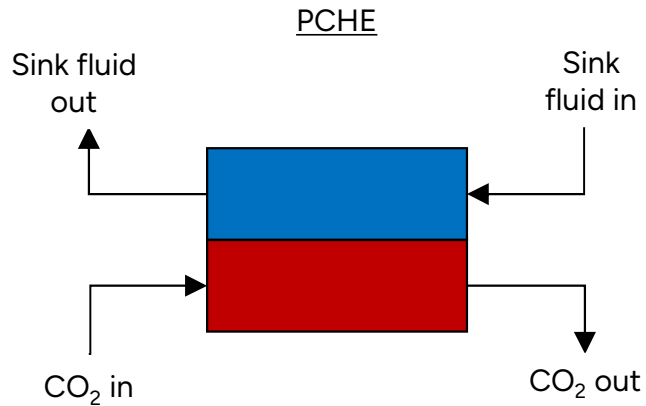
# Methodology: Fluid Properties

- Oil: Duratherm 600 [7]
- MS: HITEC [9]
- Air: dry air properties from EES using equation of state developed by Lemmon et al. (2000) [10]
- CO<sub>2</sub>: properties from EES using equation of state developed by Span and Wagner (1996) [11]

Table 1: Representative properties of fluids

Fluid	Density (kg/m <sup>3</sup> )	Viscosity (Pa-s)	Specific Heat (J/kg-K)	Thermal Conductivity (W/m-K)
Oil (20 °C)	840	0.1002	1858	0.1405
Oil (100 °C)	787	0.0053	2114	0.136
Molten salt (200 °C)	1940	7.43e-3	1562	0.435
Air (20 °C, 5 bar)	5.953	1.827e-5	1013	0.02601
Air (100 °C, 5 bar)	4.665	2.195e-5	1015	0.03172
CO <sub>2</sub> (critical point: 30.98 °C, 73.77 bar)	500.6	3.493e-5	2.872e6	0.09122
CO <sub>2</sub> (250 °C, 200 bar)	218.9	2.956e-5	1287	0.04405

# Methodology: Boundary Conditions



**Table 3: Boundary conditions, with nominal value included in parenthesis**

Fluid	Inlet Temperature (°C)	Inlet Pressure (bar)	Mass flowrate per cross-sectional area (kg/m <sup>2</sup> -s)
CO <sub>2</sub>	250, 300 (250)	200	20
Oil	50	1	5-20 (10)
MS	150	1	10-20 (20)
Air	20	5	10-20 (20)

# Methodology: PCHE Geometry

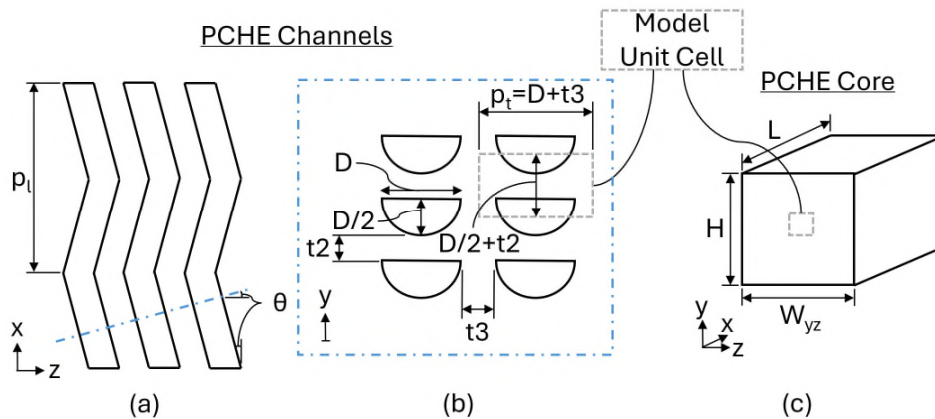
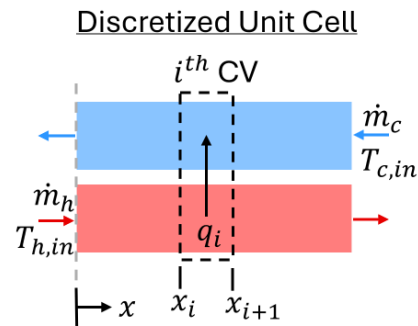


Table 4: PCHE geometric parameters, with nominal value included in bold

Parameter	Symbol	Value	Units
Diameter of semicircular channel	$D$	1.3, <b>1.5</b> , 1.7	mm
Plate thickness	$D/2 + t_2$	1.5	mm
Transverse pitch	$p_t$	1.75, <b>2.05</b> , 2.3	mm
Longitudinal pitch	$p_l$	8	mm
Channel angle	$\theta$	40	°
Length	$L$	0.25-75	m

- Material: SS316L
- Cases for parametric study ( $\text{CO}_2$  channel diameter [mm]/sink channel diameter [mm])
  - Same diameter: 1.3/1.3, 1.5/1.5, 1.7/1.7
  - Different diameter: 1.3/1.5, 1.5/1.7
- HX Length (for minimum  $T_{\text{pinch}} < 10 \text{ }^\circ\text{C}$ )
  - Oil: 0.74 m
  - MS: 0.28 m
  - Air: 0.36 m

# Methodology: Thermofluidic Model



## Equations

$$q_i = \dot{m}(h_i - h_{i+1}), \text{ CO}_2 \text{ and air}$$

$$q_i = \dot{m}c_p(T_i - T_{i+1}), \text{ oil and MS}$$

$$q_i = \frac{T_{CO_2 \text{ avg},i} - T_{\text{sink avg},i}}{R_{\text{tot},i}}$$

$$R_{\text{tot},i} = R_{\text{conv CO}_2,i} + R_{\text{cond},i} + R_{\text{conv sink},i}$$

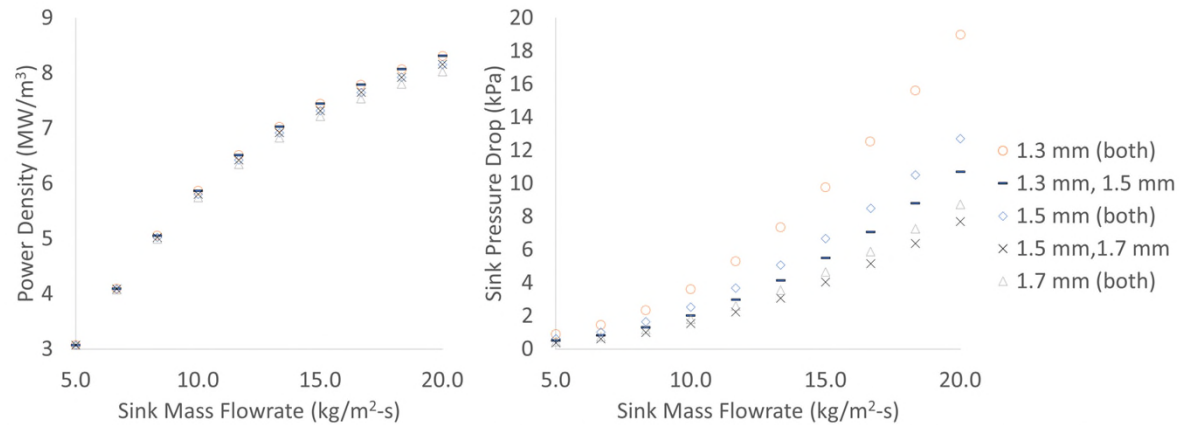
$$R_{\text{cond},i} = \frac{t^2}{k_{\text{wall}}A_{\text{wall},i}}, R_{\text{conv},i} = \frac{1}{htc_i A_{\text{conv},i}}, htc = \frac{Nu \cdot k}{D_h}$$

$$\Delta P_i = f_i \frac{L_{\text{channel,CV}}}{2D_h} \rho_i V_i^2$$

## Correlations

$Nu_{CO_2} = 0.475Re^{0.61}Pr^{0.17}, f_{CO_2} = 0.13Re^{-0.044}$	Saeed et al. (2020) $3000 \leq Re \leq 60000$ and $2.0 \leq Pr \leq 13$
$Nu = 4.089, f = \frac{15.78}{Re}$	Hesselgreaves (2001) $Re \leq 2300$
$Nu = \frac{\frac{f}{8}(Re - 1000)Pr}{1 + 12.7(Pr^{2/3} - 1)\sqrt{f/8}}$	Gnielinski (1976) $2300 \leq Re \leq 5 \times 10^6$ and $0.5 \leq Pr \leq 2000$
$f = (0.790 \ln(Re) - 1.64)^{-2}$	Petukhov (1970) $3000 \leq Re \leq 5 \times 10^6$

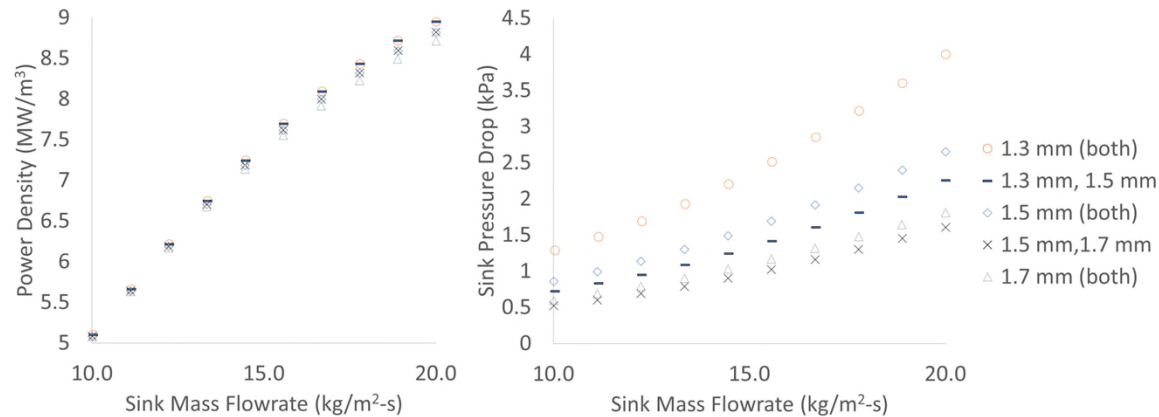
# Results: Parametric Study, Oil



**Figure 2: Parametric data for oil with a CO<sub>2</sub> inlet temperature of 250 °C and a heat exchanger core length of 0.74 m.**

- Performance metrics
  - Power density: 3-8.3 MW/m<sup>3</sup>
  - Sink-side pressure drop: 0.44-19.0 kPa
- Best cases
  - Highest power density: 1.3/1.5 case
  - Lowest  $\Delta P$ : 1.5/1.7 case
- 1.5/1.7 => 1.3/1.5
  - 1.24% increase in power density, 35% increase in  $\Delta P$  (1.26% and 35%, respectively, for 300 °C inlet temperature)

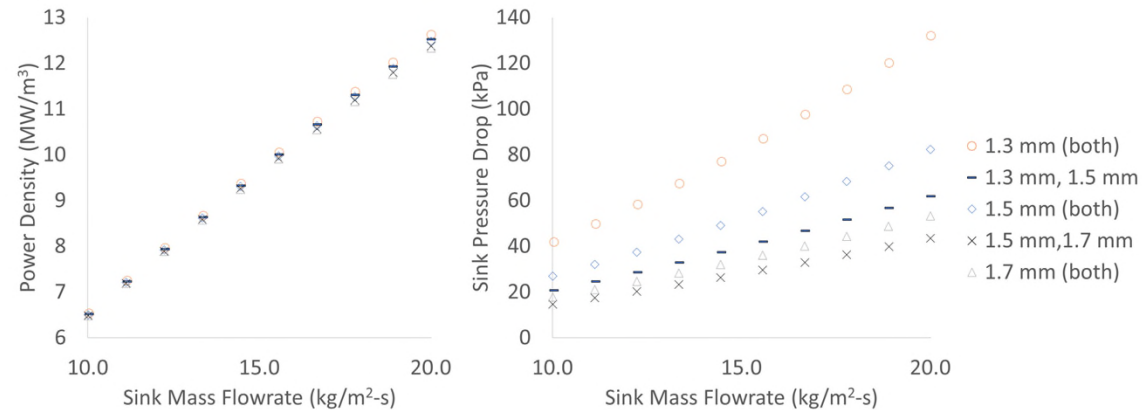
# Results: Parametric Study, MS



**Figure 3: Parametric data for MS with a CO<sub>2</sub> inlet temperature of 250 °C and a heat exchanger core length of 0.28 m.**

- Performance metrics
  - Power density: 5-9 MW/m<sup>3</sup>
  - Sink-side pressure drop: 0.6-4.0 kPa
- Best cases
  - Highest power density: 1.3/1.5 case
  - Lowest  $\Delta P$ : 1.5/1.7 case
- 1.5/1.7 => 1.3/1.5
  - 0.91% increase in power density, 39% increase in  $\Delta P$  (0.96% and 38%, respectively, for 300 °C inlet temperature)

# Results: Parametric Study, Air



**Figure 4: Parametric data for air with a CO<sub>2</sub> inlet temperature of 250 °C and a heat exchanger core length of 0.36 m.**

- Performance metrics
  - Power density: 6.5-12.6 MW/m<sup>3</sup>
  - Sink-side pressure drop: 14.7-132 kPa
- Best cases
  - Highest power density: 1.3/1.3 case
  - Lowest  $\Delta P$ : 1.5/1.7 case
- 1.5/1.7 => 1.3/1.3
  - 1.3% increase in power density, 193% increase in  $\Delta P$  (1.44% and 196%, respectively, for 300 °C inlet temperature)



# Results: Parametric Study Summary

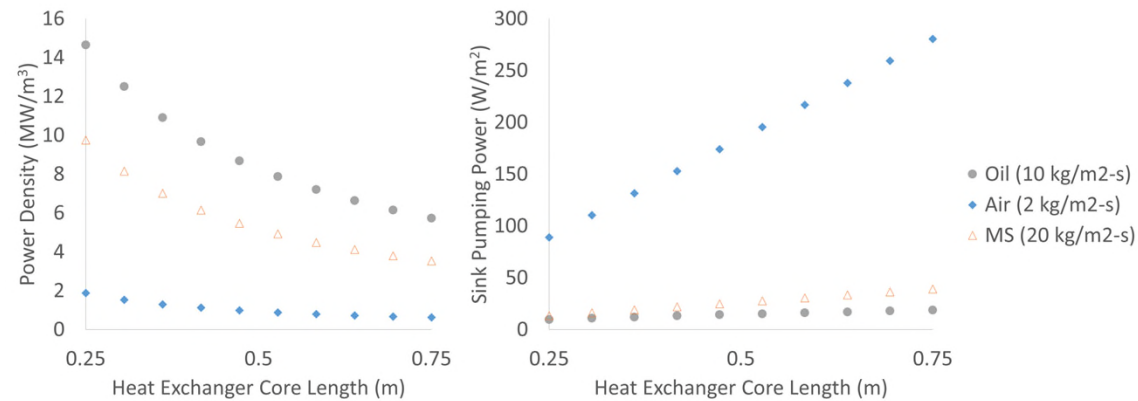
- For all fluids, 1.5/1.7 case was optimal
  - Decreasing channel size => slight increases in power density, significant increases in  $\Delta P$

Table 5: Parameters to achieve 0.5 MW HX for 250-300 °C CO<sub>2</sub> inlet temperature

Sink Fluid	HX Core Volume (m <sup>3</sup> )	HX Side Length (m)	CO <sub>2</sub> Outlet Temperature (°C)	Pumping Power (W)
Oil	0.0686-0.0862	0.30-0.34	110-114	1.56-2.2
MS	0.0386-0.0567	0.37-0.45	161-164	1.81-3.0
Air	0.0334-0.0404	0.30-0.34	107-114	15500-16400

- Observations
  - Higher inlet temperature of MS => higher CO<sub>2</sub> outlet temperature
  - Lower inlet temperature of air helps enhance heat transfer
  - Pumping power ( $\propto$  volumetric flowrate  $\cdot \Delta P$ ) is very high for air case
  - => Consider lower air flowrate to achieve lower pumping power

# Results: Varying HX Length



**Figure 5: PCHE performance with a CO<sub>2</sub> inlet temperature of 250 °C for oil, MS, and air at different core lengths.**

- 0.5 MW HX with air as sink (0.36 m length)
  - Volume: 0.314-0.383 m<sup>3</sup> (an order of magnitude larger than oil- and MS-cooled HXs)
  - Side length: 0.93-1.03 m (~3 times larger than oil- and MS-cooled HXs)
  - Pumping power: 133-140 W (~1-3 W for oil and MS)
- Average heat transfer coefficients for each fluid over various HX lengths
  - CO<sub>2</sub>: 4310-4350 W/m<sup>2</sup>-K
  - Oil: 517-524 W/m<sup>2</sup>-K
  - MS: 1817-1823 W/m<sup>2</sup>-K
  - Air: 157.5-161.3 W/m<sup>2</sup>-K



# Conclusions

- Investigated performance of PCHE as heat sink for high-temperature CO<sub>2</sub> HP
- Considered different sink fluids and variations in channel diameter
- Geometry
  - Optimal case aligned across fluids (1.5/1.7)
  - Marginal enhancements in power density and large increases in pressure drops with smaller channel diameters (larger channel diameters not possible with plate thickness selected)
- Sink fluids
  - Air
    - 8 x or 5 x size of MS- or oil-cooled HXs, respectively
    - Pumping power still 2 orders of magnitude larger
    - =>Hybrid design needed for feasibility with larger air-side flow passages
  - MS
    - Most compact HX
    - Higher CO<sub>2</sub> outlet temperature, corrosiveness, cost
    - Widely implemented with CO<sub>2</sub> applications (e.g., in CSP)
  - Oil
    - Reasonably compact (a little under 2 x size of MS-cooled HX)
    - Fire safety, cost
    - Less explored
- Future work: PCHE design to be developed and tested as part of a HTHP for the COMHP TES project, with thermal oil as the sink fluid



# COMHP TES

Compact Heat Pump and Thermal Energy Storage System for Industrial Applications

Validating a CO<sub>2</sub>-based high-temperature heat pump at KTH's Division of Heat and Power Lab

### Key Facts

Providing heating and cooling

- Heating up to 325 °C
- Cooling at 5 °C

Testing real industrial use cases

Project Consortium



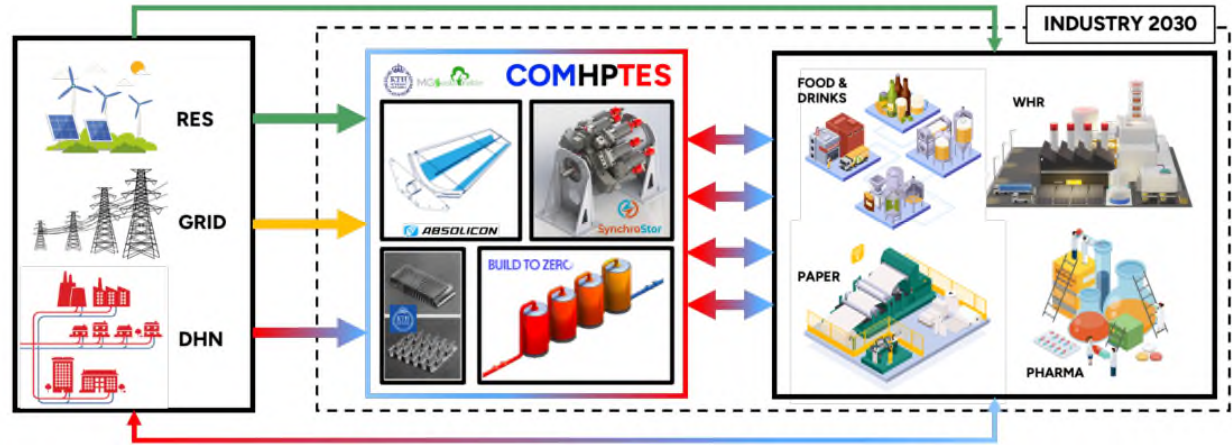
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Co-funded by the European Union





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