

# Center for Advanced Turbomachinery and Energy Research (CATER)

Cycle Innovation and Optimization  
Aerodynamics, Heat Transfer and Durability

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University R&D Panel  
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Cycle Innovation and Optimization  
Aerodynamics, Heat Transfer and Durability

Acknowledging  
Students from the group  
present in the audience:

Ofek Amasay  
Emmanuel Gabriel-Ohanu  
Akim Khlyapov  
Adil Riahi  
Ryan Wardell

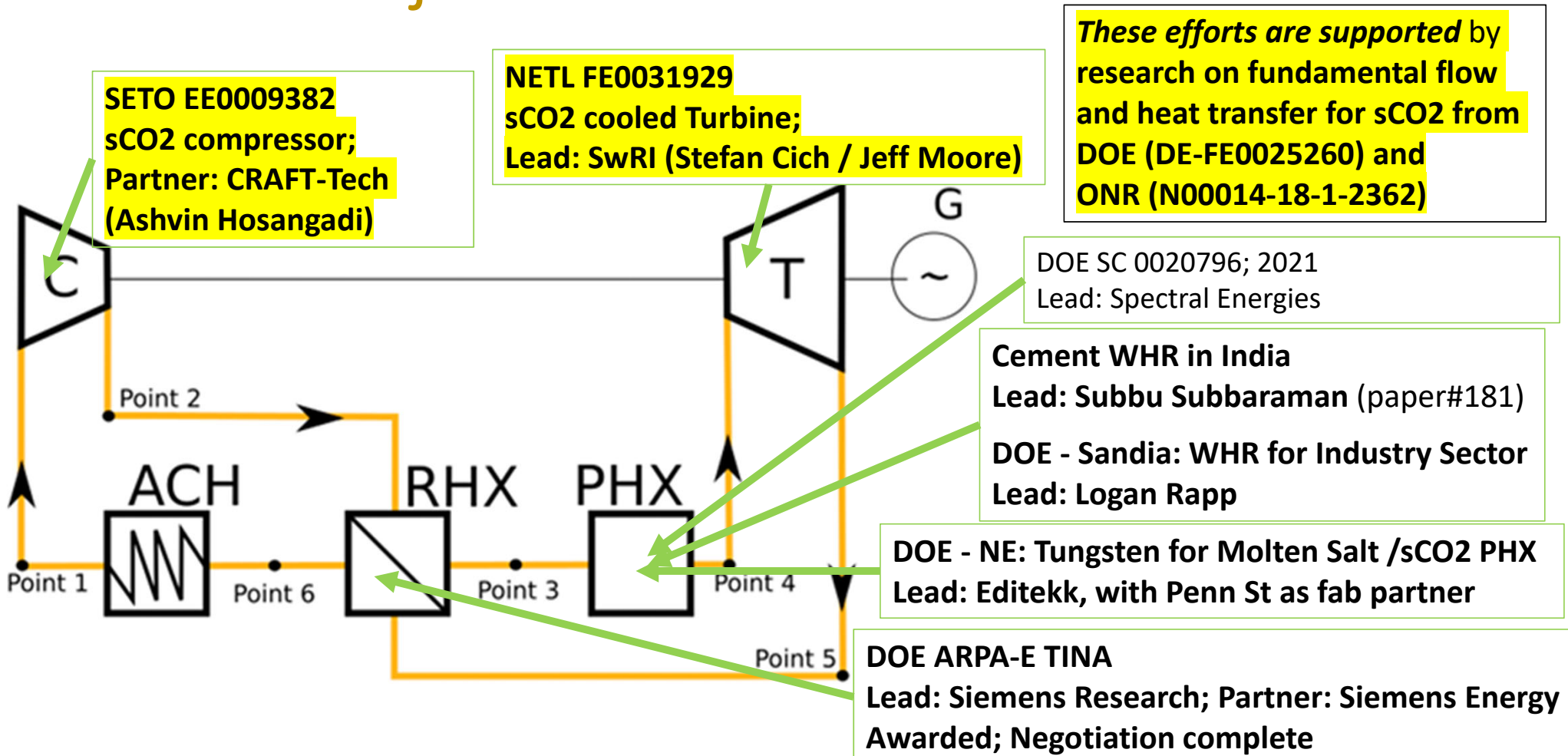
Notable Past Members:

Dr. Akshay Khadse (Nikola)  
Ian Cormier (8 Rivers)  
Dr. Ankur Deshmukh (Siemens)  
Dr. Mahmood M. (Mitsubishi)  
Josh Schmitt (SwRI)

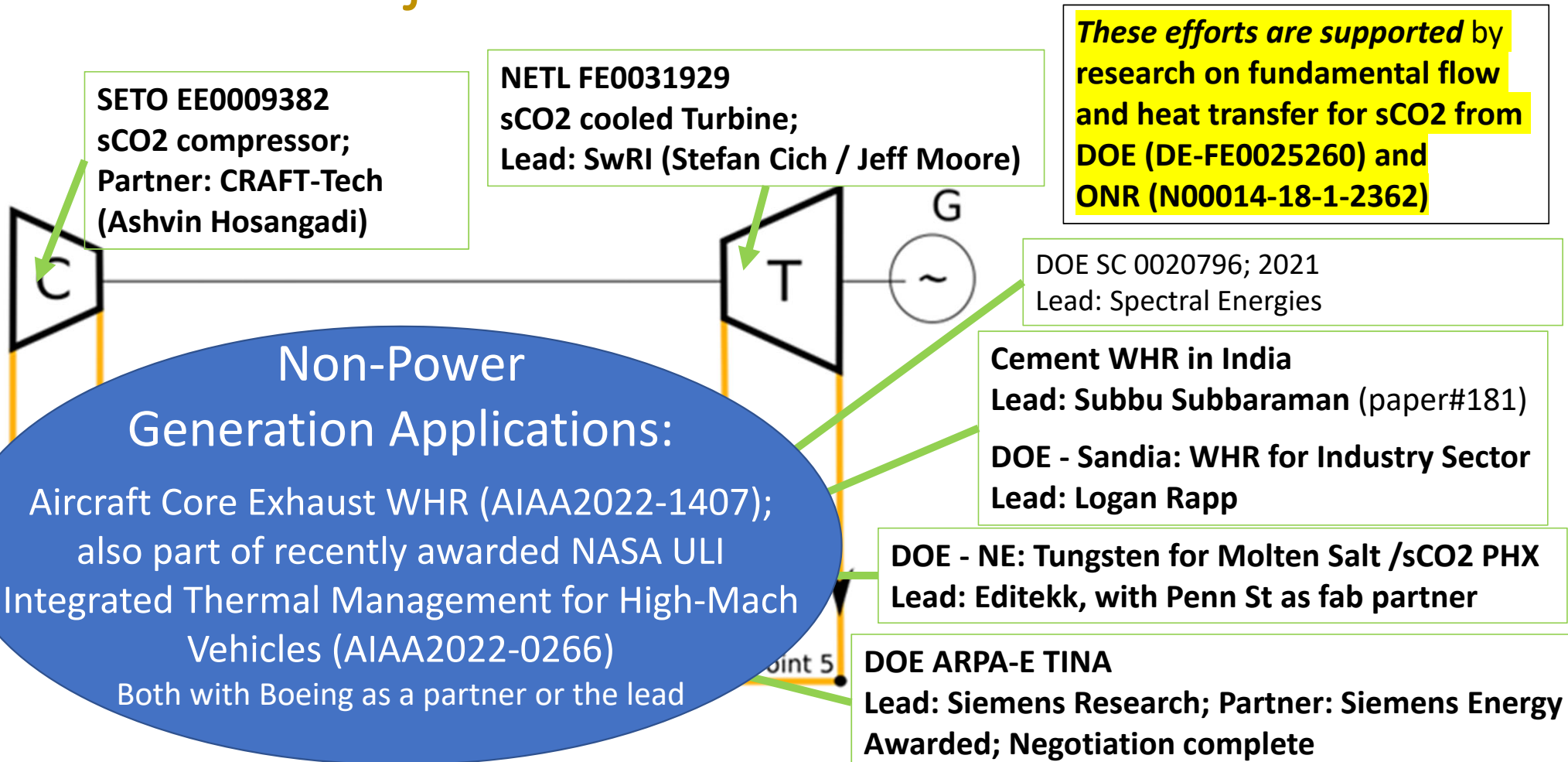
Home Alone:

John Richardson  
Manoj Sargunraj  
Matt Smith

# Various Projects in Non-Combustion Area



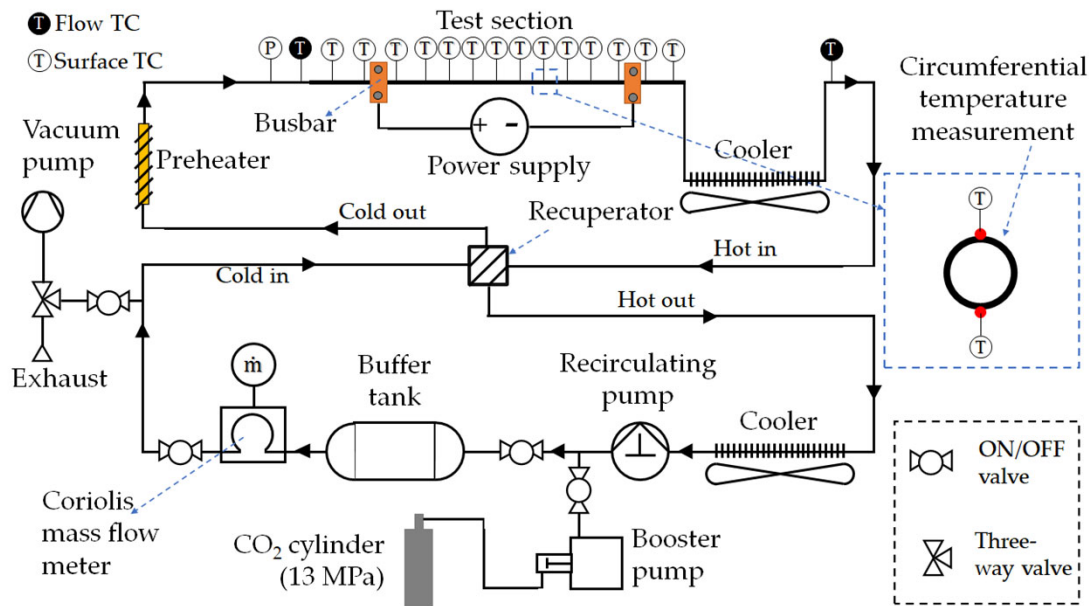
# Various Projects in Non-Combustion Area





# Primary sCO<sub>2</sub> Test Loop

- Stainless steel and Inconel test section; rest of the loop: stainless steel
- Heat addition to test section via Joule heating
- Pressure range = 80-200 bar,
- Mass flow rate range (Sigma pump)
  - 0.66-16.5 L/min OR 0.01-0.25kg/s @910 kg/m<sup>3</sup>
- Temperature up to 700°C for Inconel and 510°C for stainless steel test sections
- Sigma pump (piston driven pump) and recuperator



Schematic of the loop

Heat transfer loop for high pressure, high temperature testing

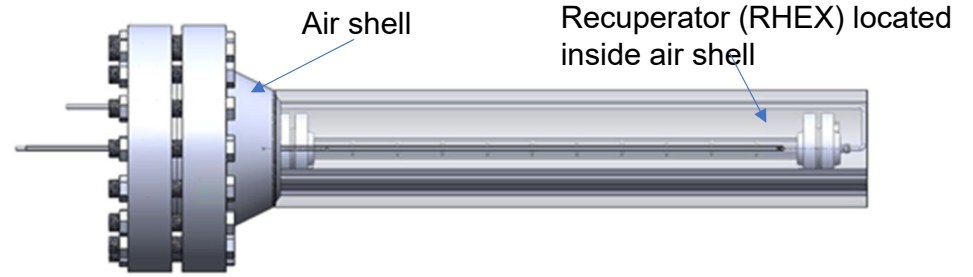


Circulating pump and recuperator in the loop

# Recuperator



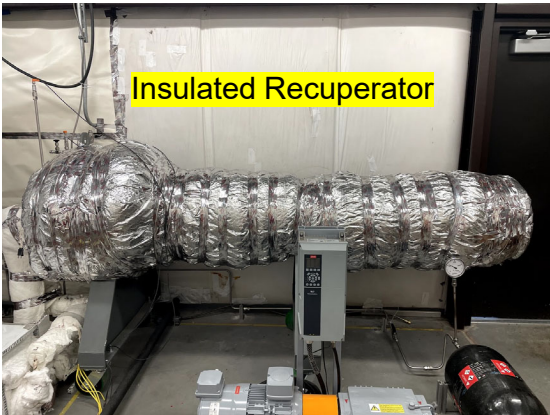
- Hot outlet
- Hot inlet
- Cold inlet
- Cold outlet
- Line for High pressure N2 fill/exhaust to/from "Air Shell"



Duct containing insulation for high temp lines

Thermal insulation for high temp lines

Sensors to monitor recuperator performance

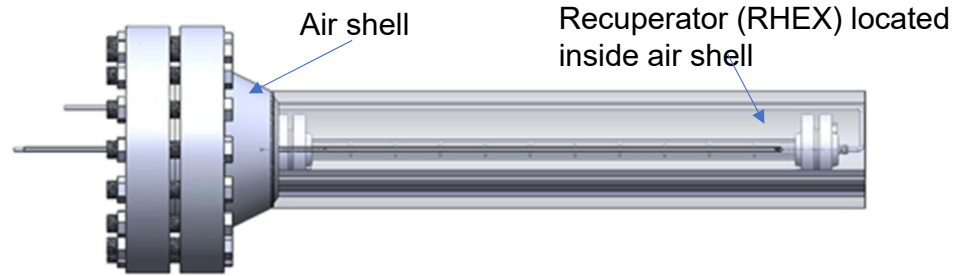




# Recuperator

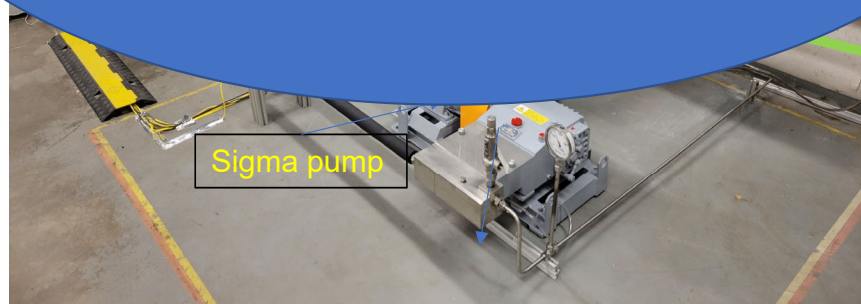
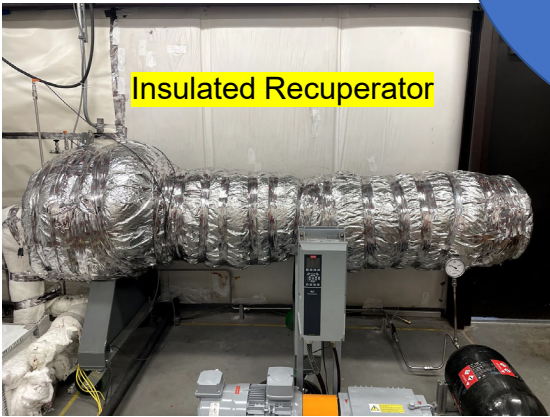
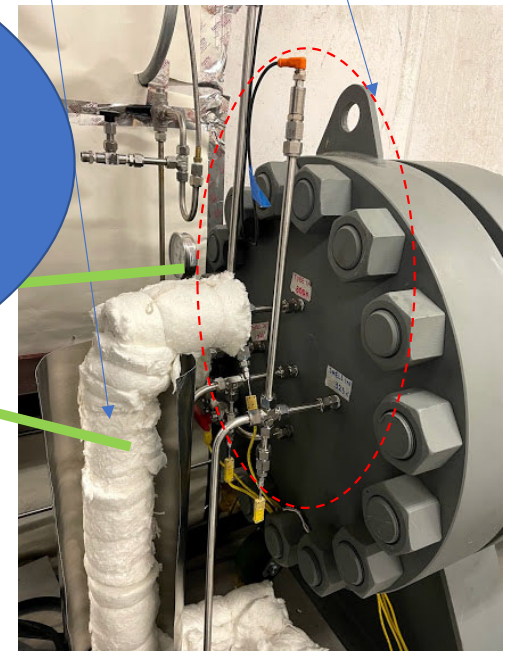


- Hot outlet
- Hot inlet
- Cold inlet
- Cold outlet
- Line for High temp fill/exhaust

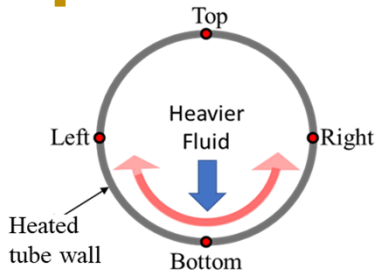


This recuperator will be replaced for testing of ARPA-E TINA Recuperator.

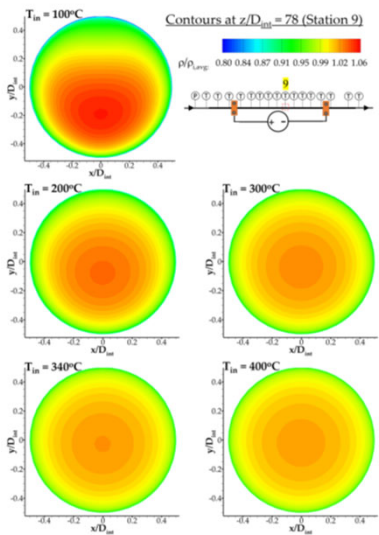
- Duct containing...
- Thermal insulation for high temp lines
- Sensors to monitor recuperator performance



# Impact of Inlet Temperature on buoyancy

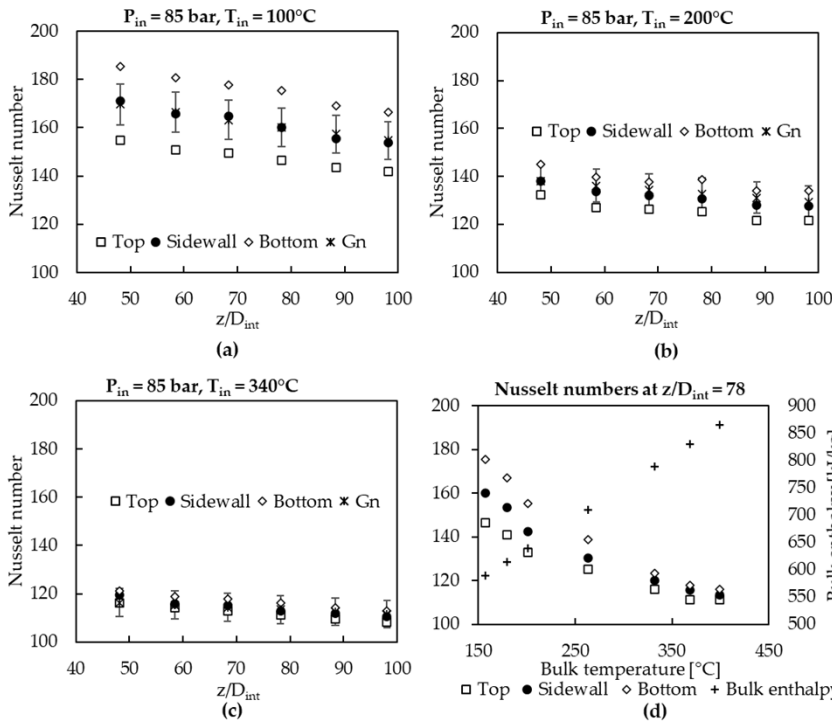


Schematic showing formation of natural convection currents in a cross section of a heated circular tube



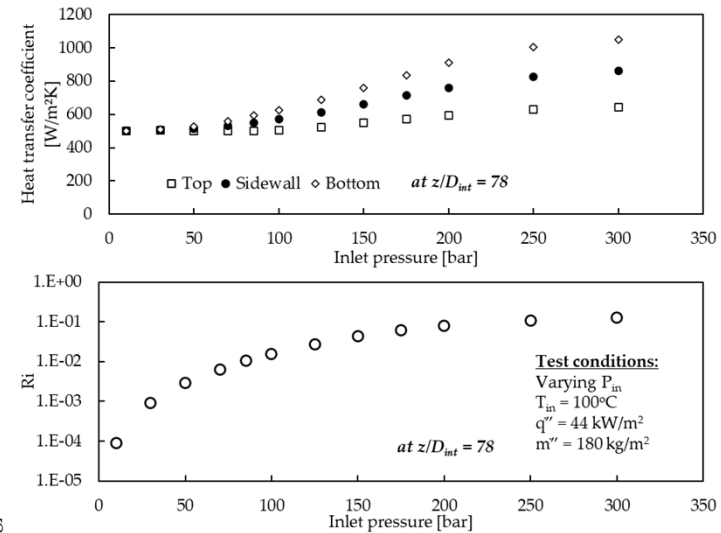
Density contours at varying  $T_{in}$

Experimental results: Varying inlet T cases with constant inlet P, heat flux and mass flux

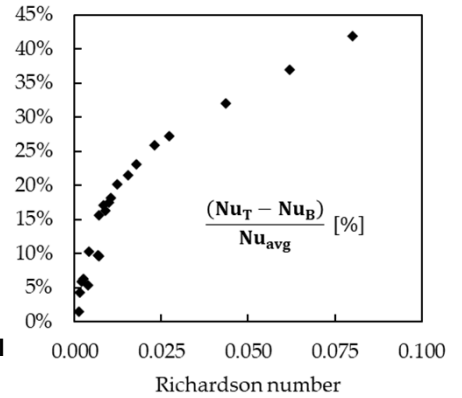


$Nu_T$  = Nusselt number at top wall  
 $Nu_B$  = Nusselt number at bottom wall  
 $Nu_{avg}$  = Average Nusselt number

Varying inlet P cases with constant inlet T, heat flux and mass flux

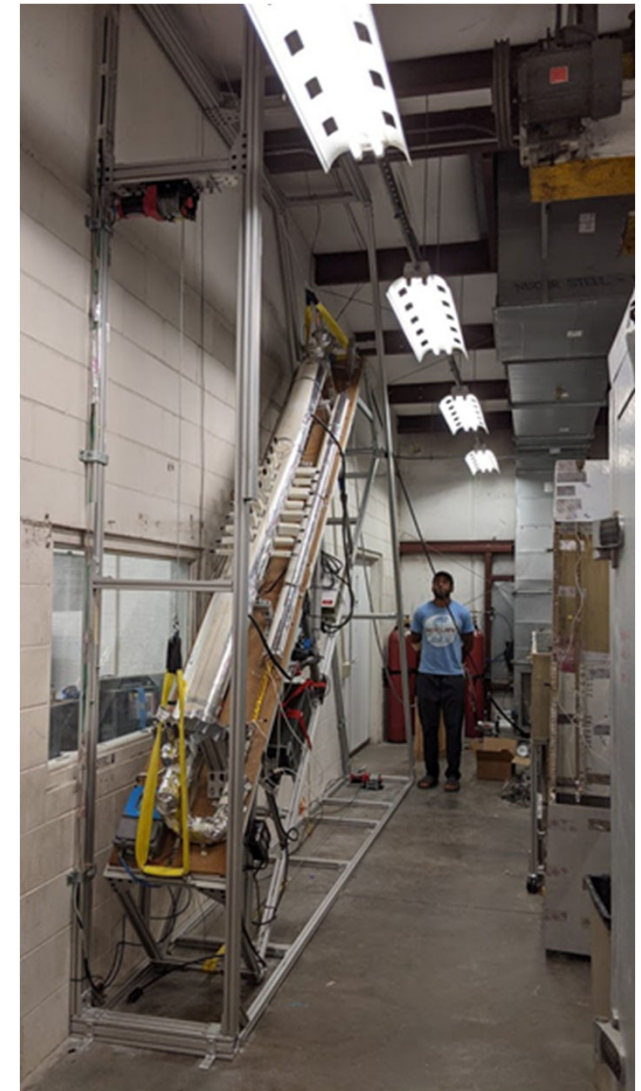
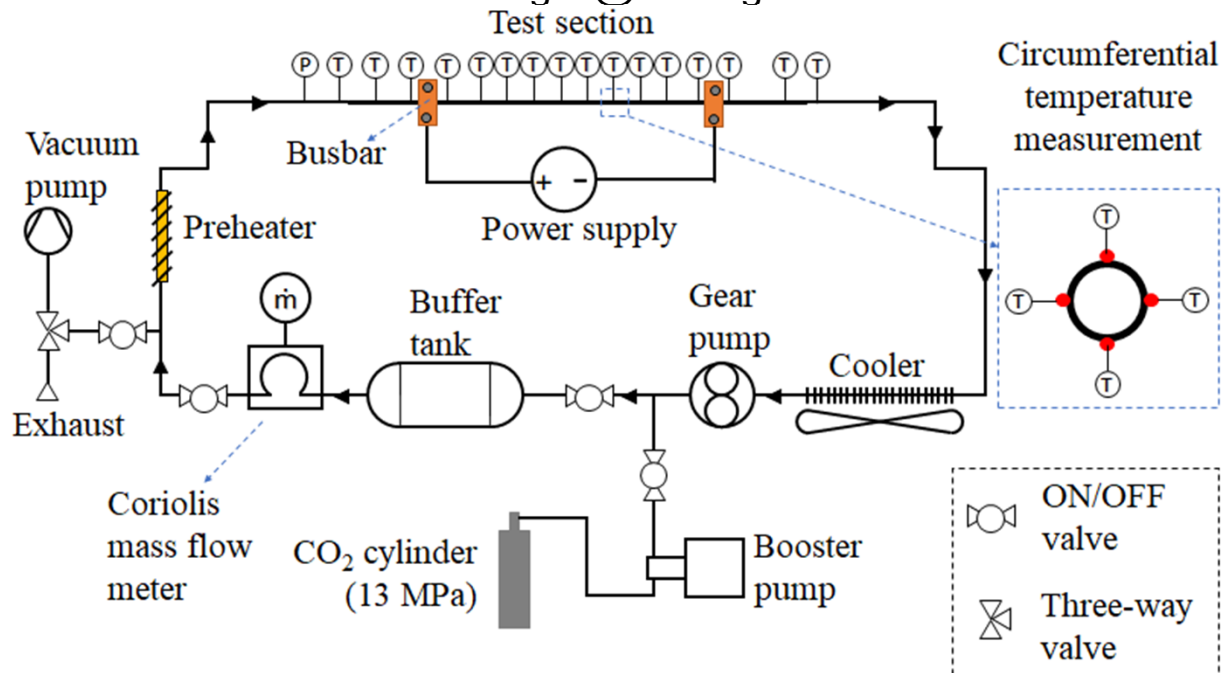


**Test conditions:**  
 Varying  $P_{in}$   
 $T_{in} = 100^\circ\text{C}$   
 $q'' = 44 \text{ kW/m}^2$   
 $m'' = 180 \text{ kg/m}^2$



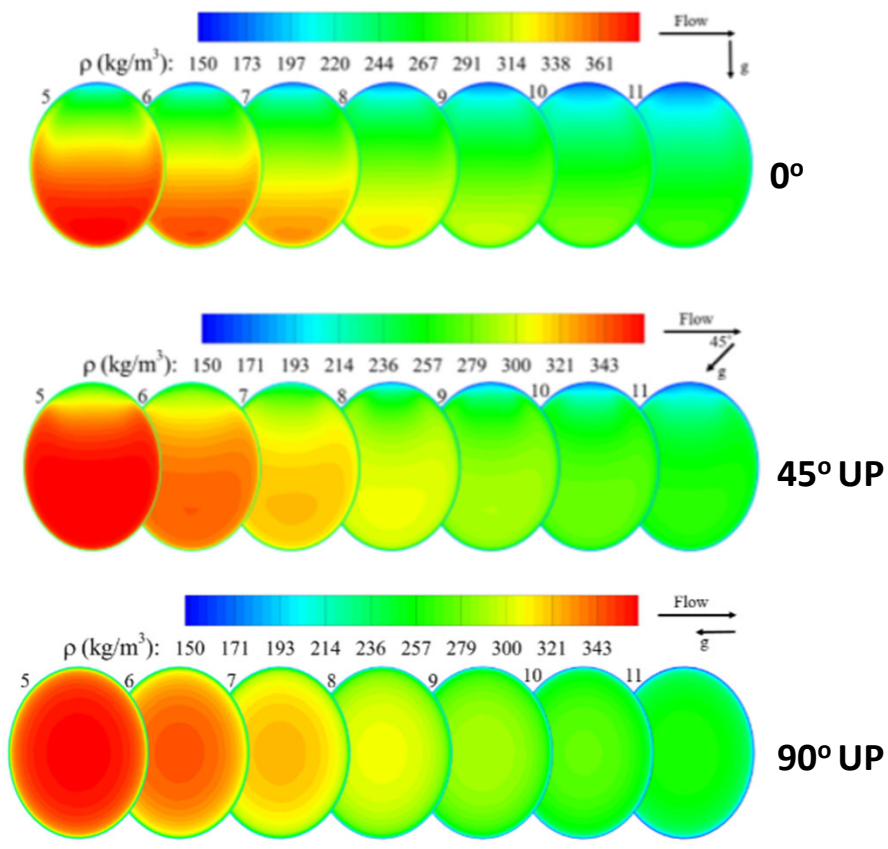
# Inclined, Near-Critical Test Rig

- Capability to test heat transfer in inclined tubes 0-90°
- Pressure up to 100 bar and Inlet temperature range 20-200°C
- Constant heat flux addition to test section via Joule heating
- Micropump pump (gear pump) as recirculating pump
- Flow rate range
  - 3.21 L/min OR 0.05kg/s @ 910 kg/m<sup>3</sup>

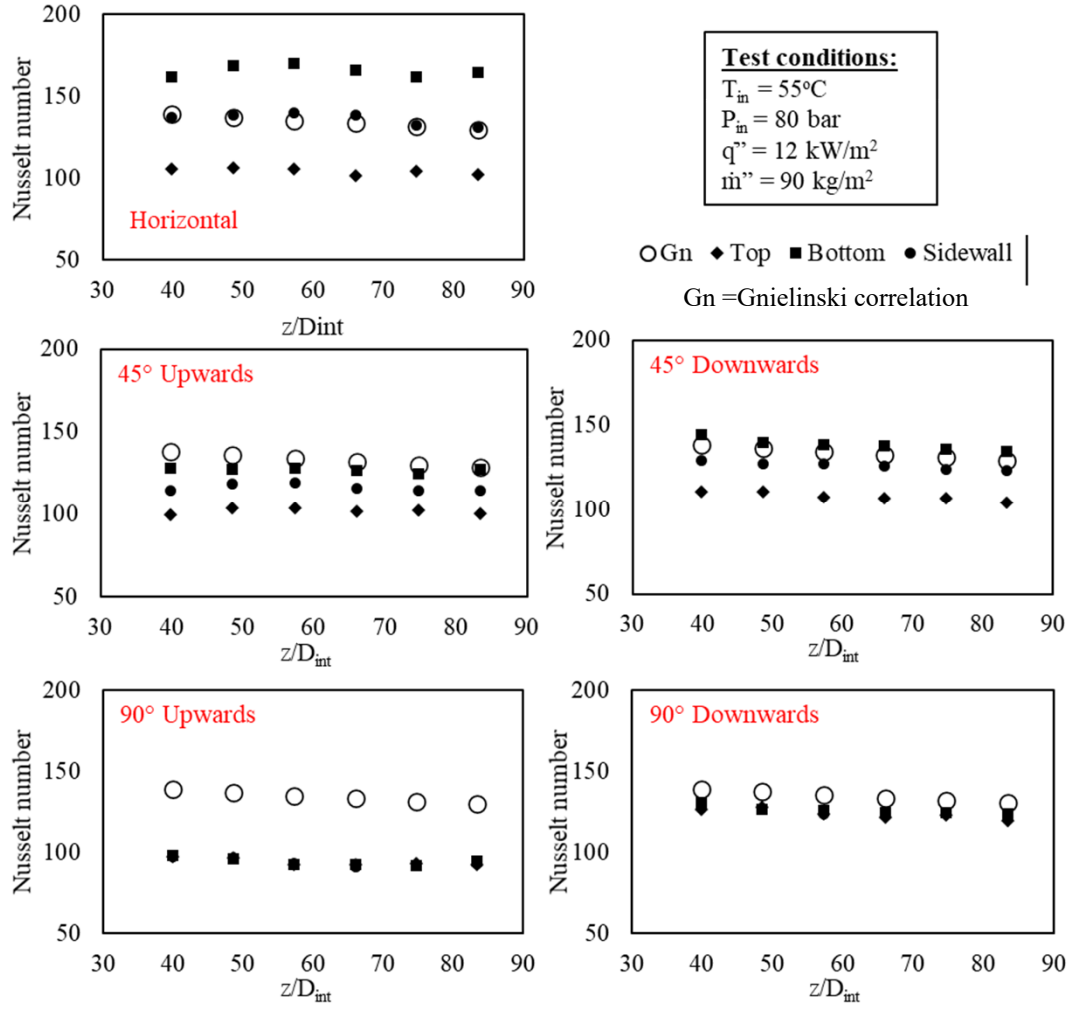




# Impact of inclination on sCO<sub>2</sub> heat transfer



CFD density contours for upward flow 0° to 90°

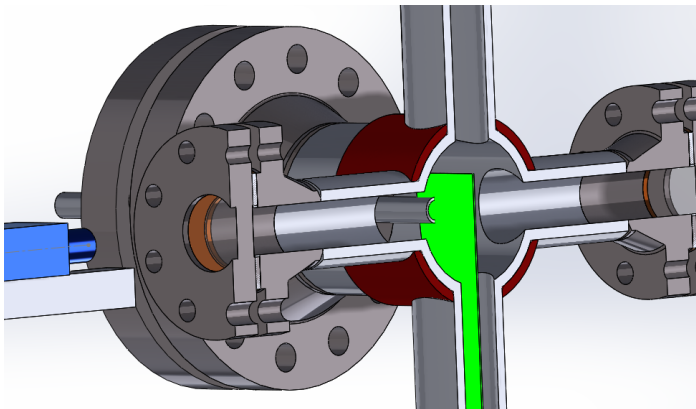
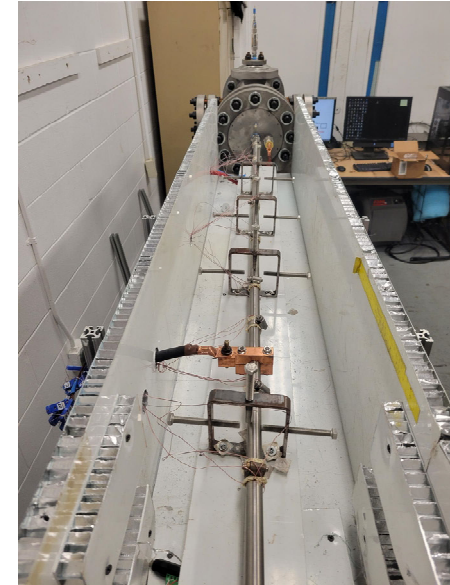
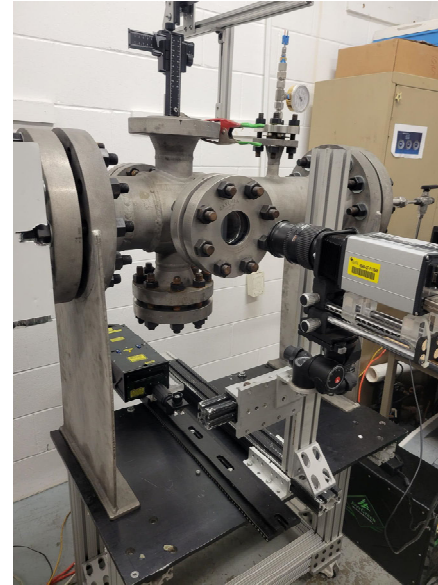


Experimental Nusselt number distribution

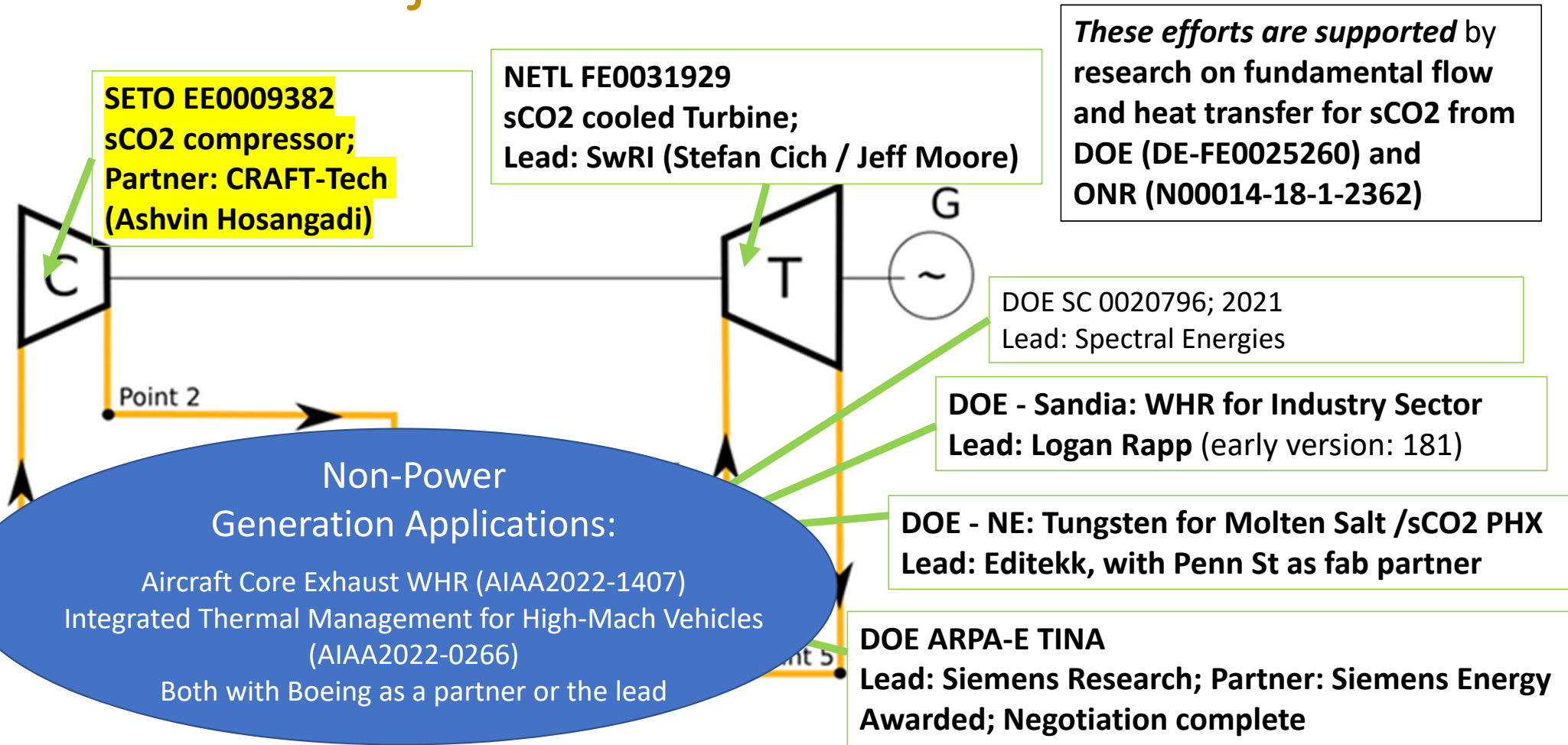


# sCO<sub>2</sub> Optical Diagnostic Testing

- 316 Stainless steel vessel
- Modular Internal setup for testing multiple geometries of interest
- High Pressure gland fittings for internal instrumentation
- Four, 3in fused silica optical windows
- Maximum pressure: 100 bar
- Maximum temperature: 90°C
- Diagnostics; Particle Image Velocimetry(PIV), Background Oriented Schlieren (BOS), Schlieren, Thermographic PIV, Laser Doppler Velocimetry (LDV), IR Thermography (with IR transmissive window)

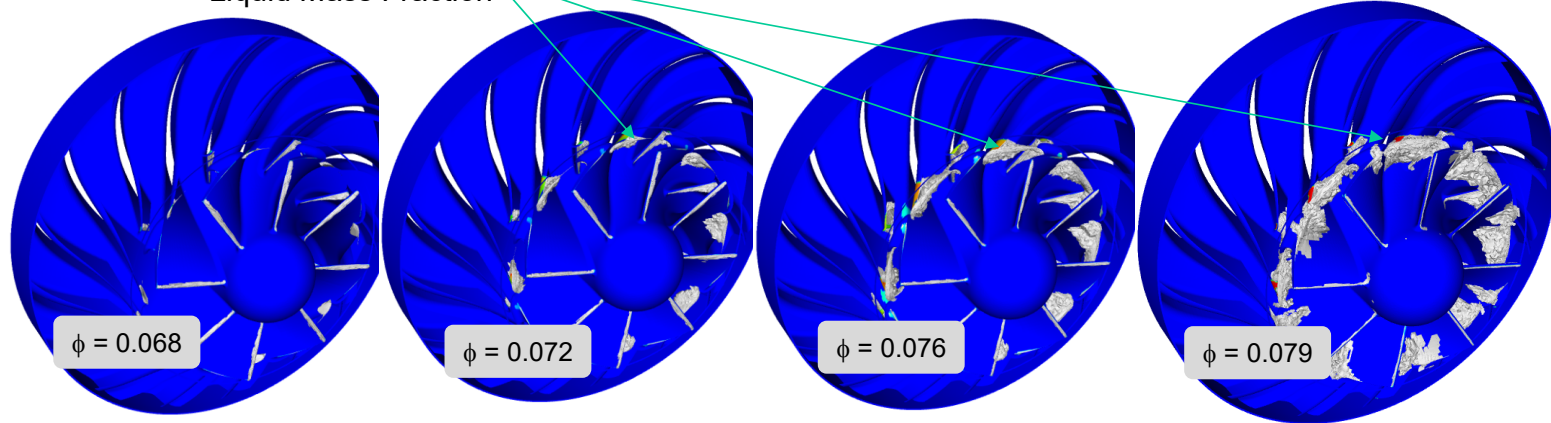


# Various Projects in Non-Combustion Area

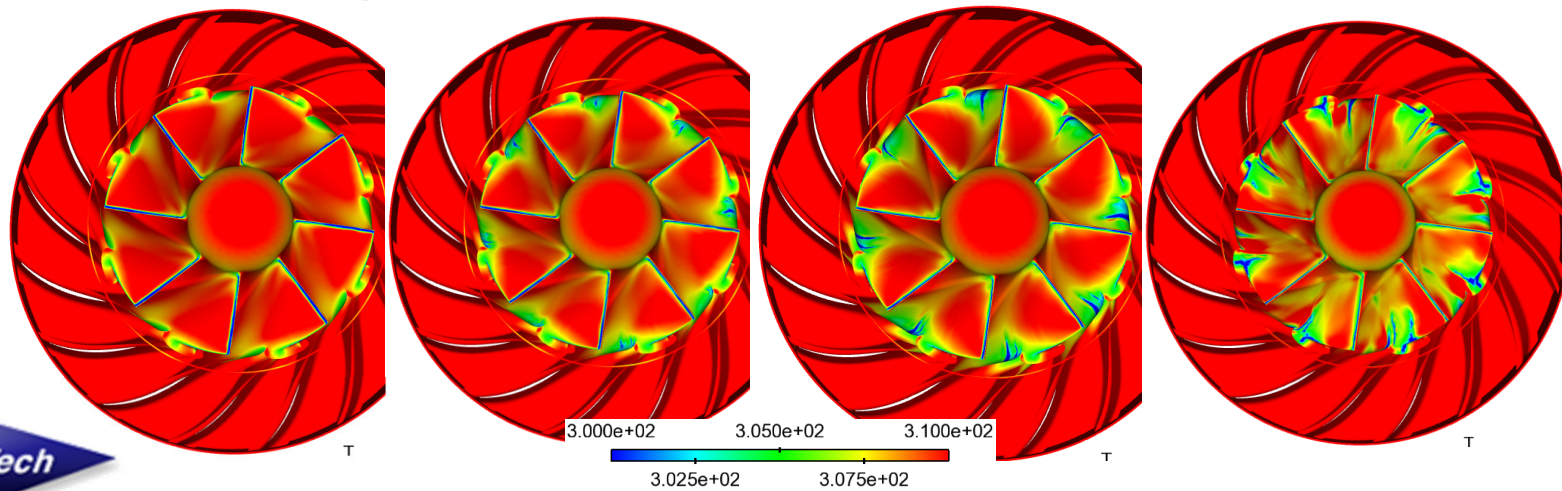


# Subcritical Effects at Shroud Inlet At High Flow Rates

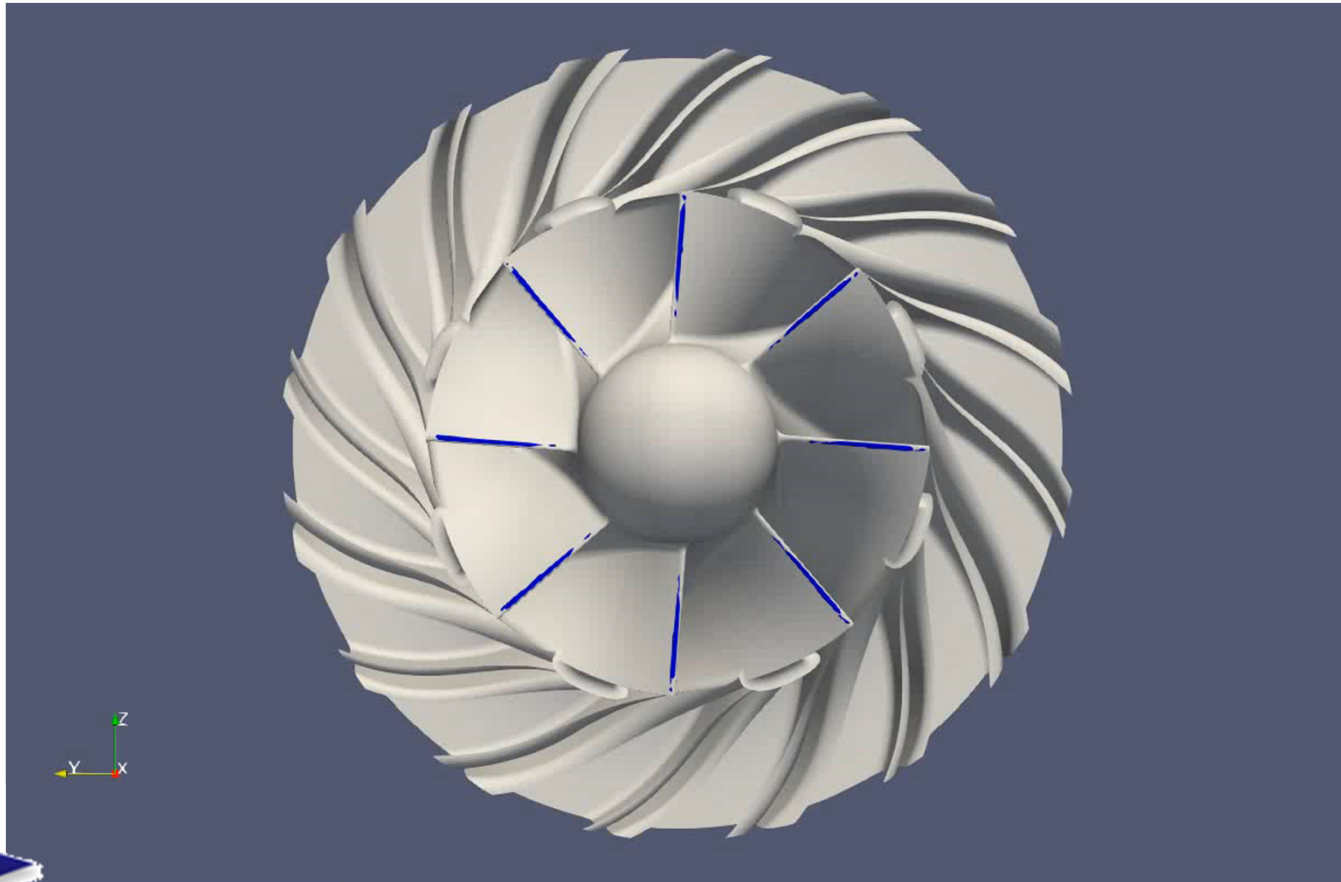
Liquid Mass Fraction



## Subcritical Temperature



# High Flow: Pressure Fluctuation Couples with Phase Change to Generate Surge

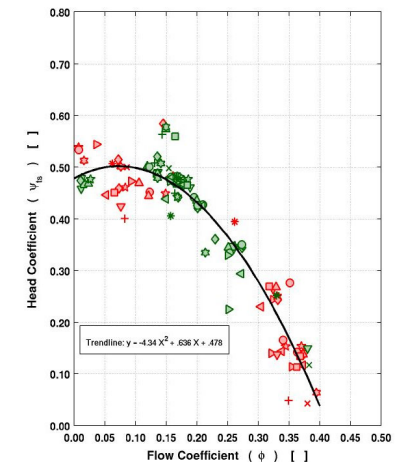
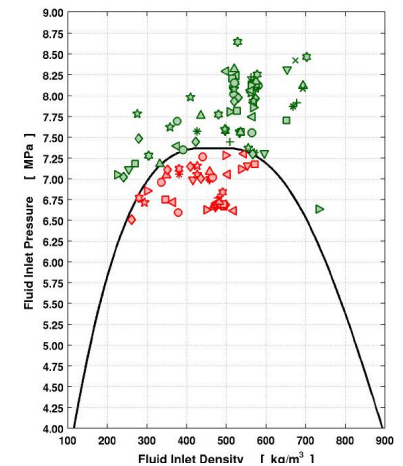




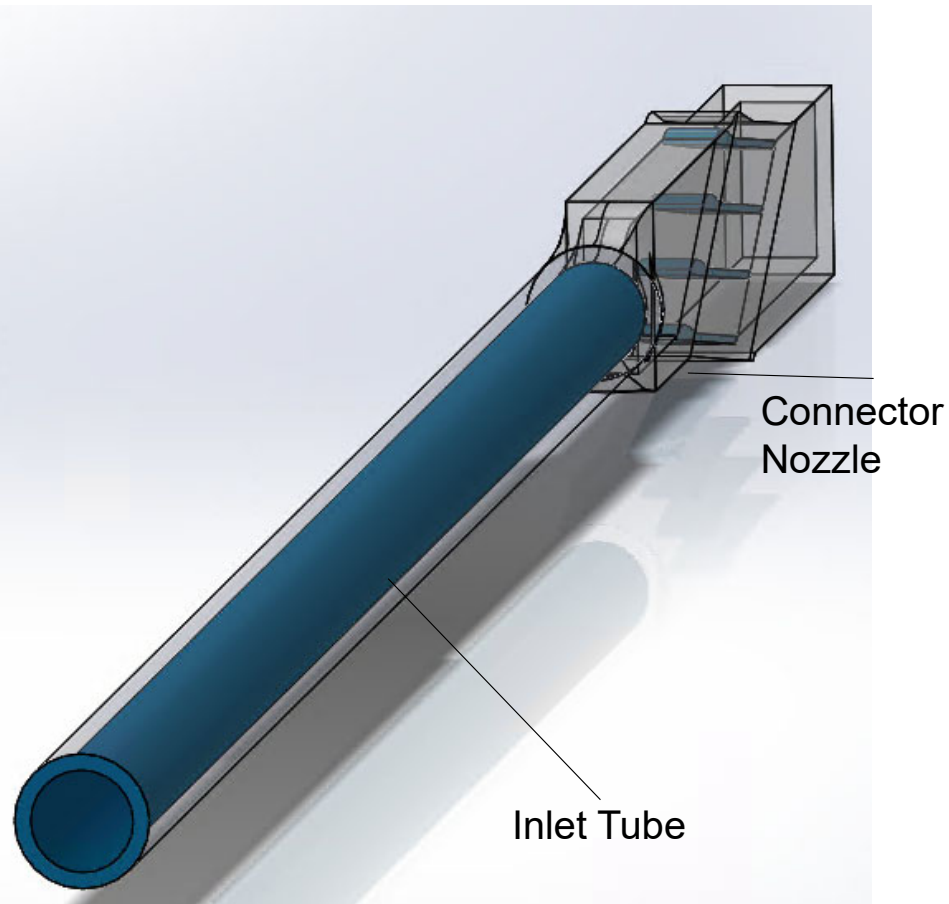
## Comparisons with Sandia: Thoughts and Future Direction

- The Sandia compressor was tested over a broad range of thermodynamic conditions including **at** the critical point as well as subcritical two-phase inlets
- As per results and discussion in Noall and Pasch, the compressor was stable with minimal vibrations, the head coefficient scaled for all conditions.
- While the efficiency values for Sandia compressor may not be reliable the efficiency curves do NOT show a sharp drop-off at high flow rates unlike the Apollo (Hanwha/GE STEP) compressors
  - Tip Speed for Sandia Compressor at 55 K RPM is 110 m/s and Tip Speed for Hanwha Compressor at 27 K RPM is 167 m/s
- It would be worthwhile in a future effort to investigate what the design differences are and if there are lessons to be learned that can further improve the performance of full scale compressors resulting in improved overall system performance

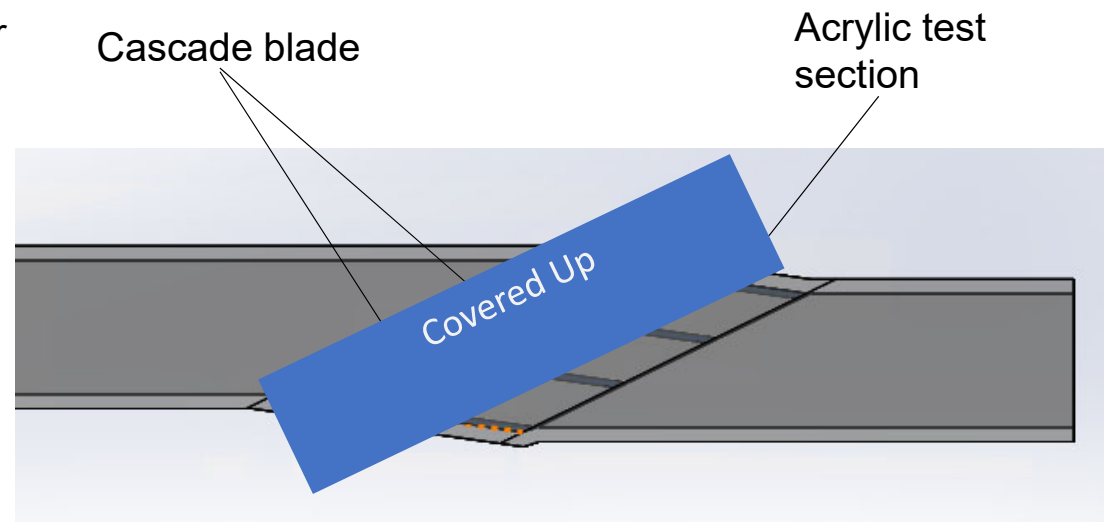
Sandia Test results  
(Noall and Pasch)



# sCO<sub>2</sub> Cascade blade Design

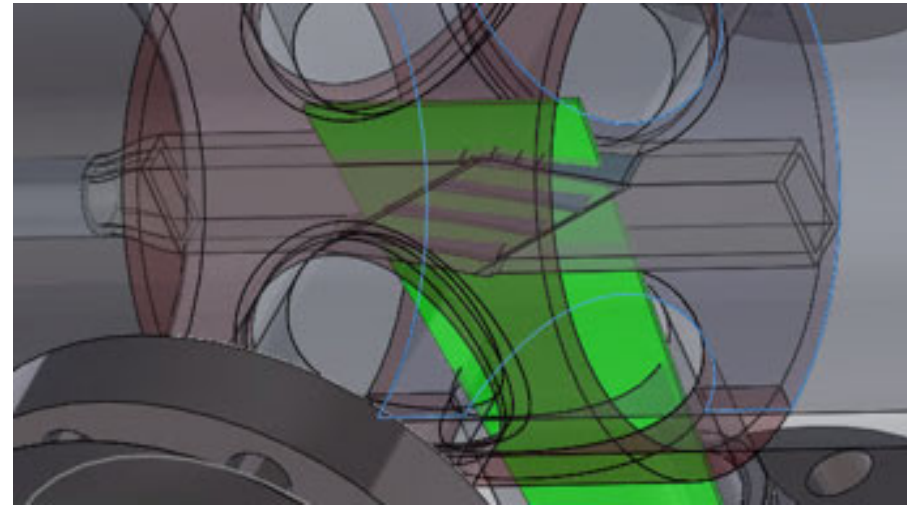
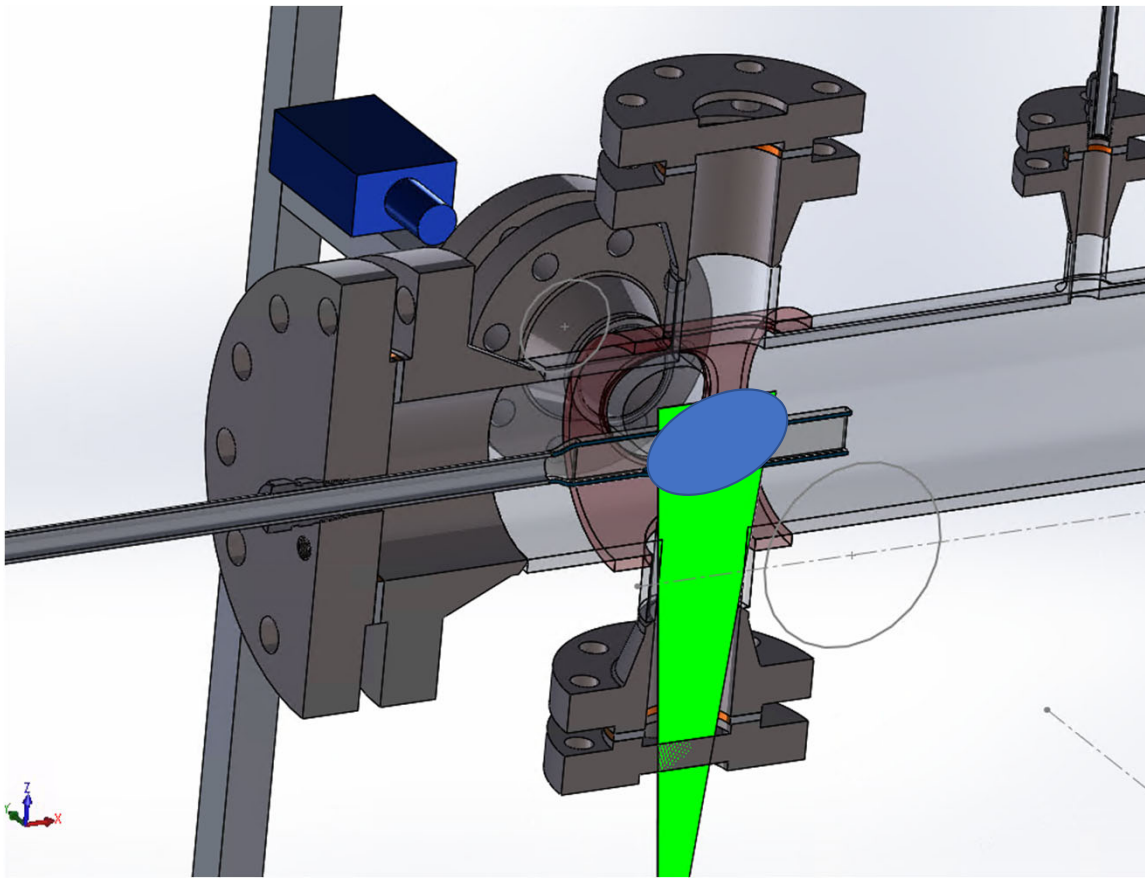


- Inlet Tube with OD of 0.76 inch
  - Seamless stainless steel 316
- Test Section
  - fabricated from acrylic with thickness of 1/8 inch
  - 2 fully immersed cascade blades
  - 2 blades forming the walls
  - Adjustable exit tailboards





# sCO<sub>2</sub> PIV Rig with Linear Compressor Cascade

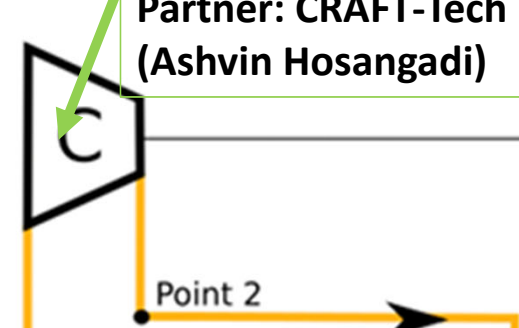


# Various Projects in Non-Combustion Area

SETO EE0009382  
sCO<sub>2</sub> compressor;  
Partner: CRAFT-Tech  
(Ashvin Hosangadi)

NETL FE0031929  
sCO<sub>2</sub> cooled Turbine;  
Lead: SwRI (Stefan Cich / Jeff Moore)

These efforts are supported by research on fundamental flow and heat transfer for sCO<sub>2</sub> from DOE (DE-FE0025260) and ONR (N00014-18-1-2362)



## Key Features in Cooling sCO<sub>2</sub> Turbine:

High external Re, leading high external heat transfer coeff (htc)  
For MAX metal temp control, **high internal htc needed**  
Because of the cycle, higher potential for cooling requiring low heat load parameter (HLP)

## Non-Power Generation Applications:

Aircraft Core Exhaust WHR (AIAA2022-1407)  
Integrated Thermal Management for High-Mach Vehicles (AIAA2022-0266)  
Both with Boeing as a partner or the lead

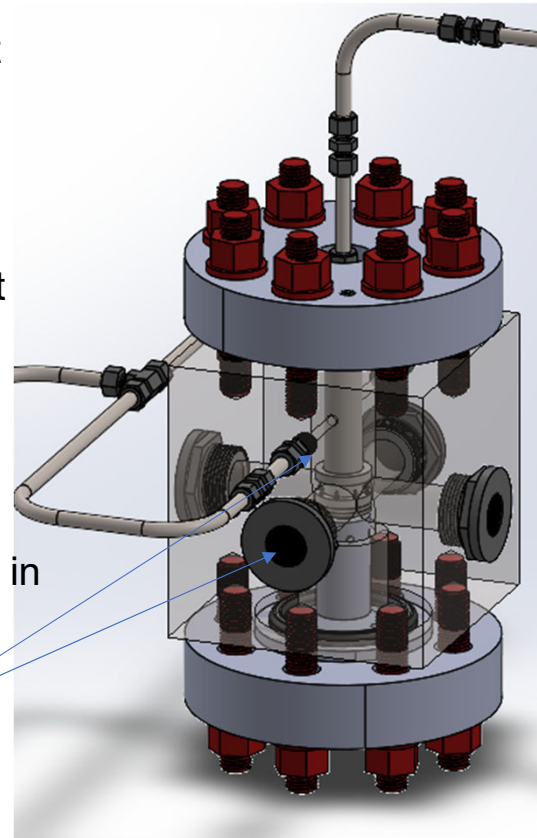
sCO<sub>2</sub> PHX  
Lead: Eutern, with Penn St as fab partner

DOE ARPA-E TINA  
Lead: Siemens Research; Partner: Siemens Energy  
Awarded; Negotiation complete

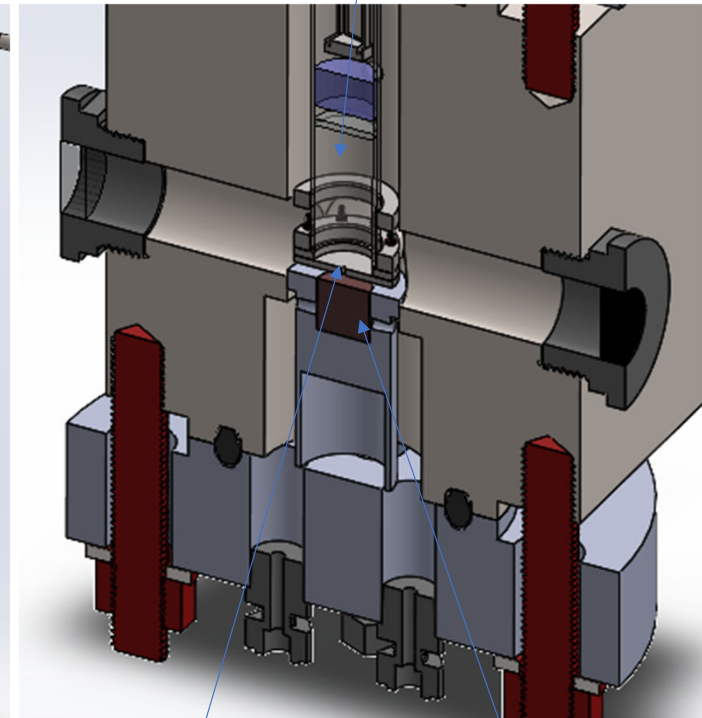
# sCO<sub>2</sub> Impingement heat transfer

- 316 Stainless steel forging with flanges act as pressure vessel
- Maximum operating pressure 200 bar
- Maximum operating temperature 450°C
- Maximum Mass Flow Rate: 0.2 kg/s
- Instrumentation for heat transfer coefficient estimation
- High pressure gland fittings for power transmission and instrumentation
- Variable orifice diameter (> 1mm)
- Variable jet to target spacing
- Copper Impingement target diameter 1.5 in
- Capability for optical diagnostics

Optical windows



Jet plenum

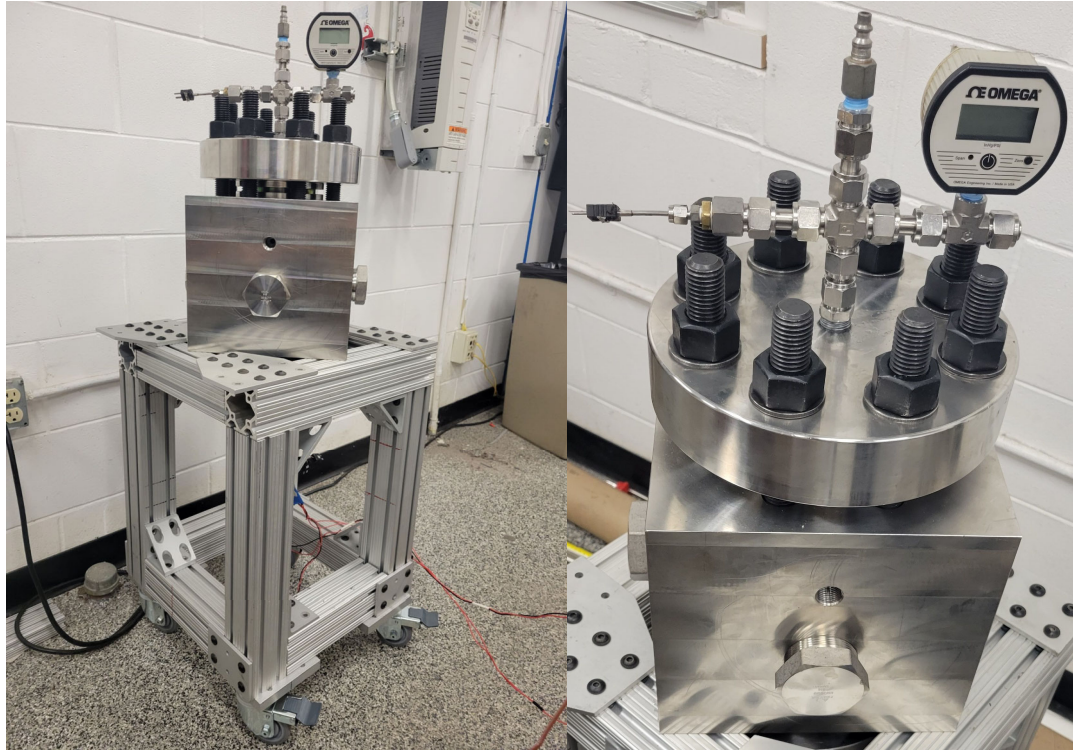


Jet orifice

Copper impingement feature



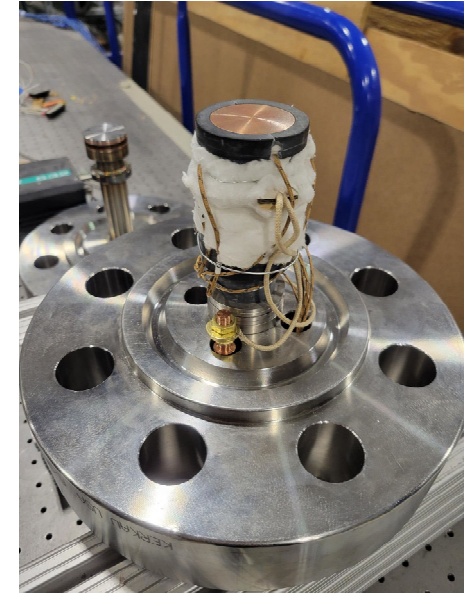
# sCO<sub>2</sub> Impingement heat transfer



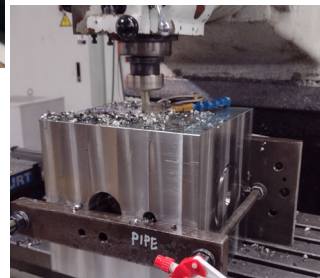
Impingement heat transfer rig (Air validation configuration)



Jet plenum and orifice assembly



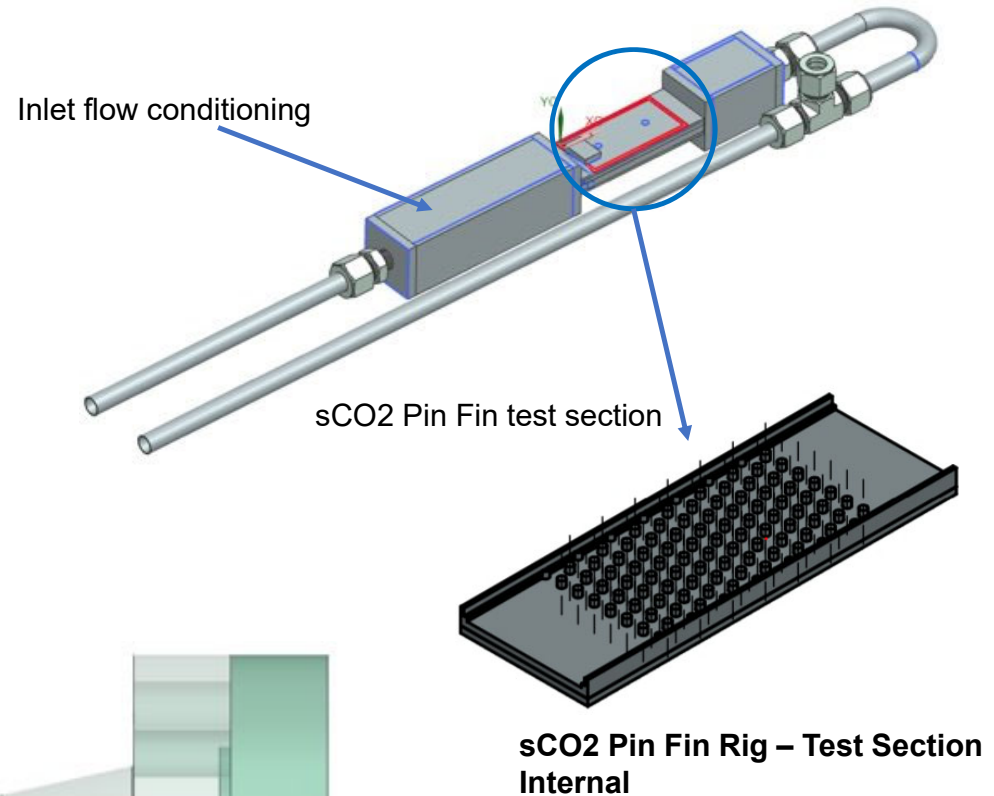
Heat transfer feature assembly with heater and instrumentation



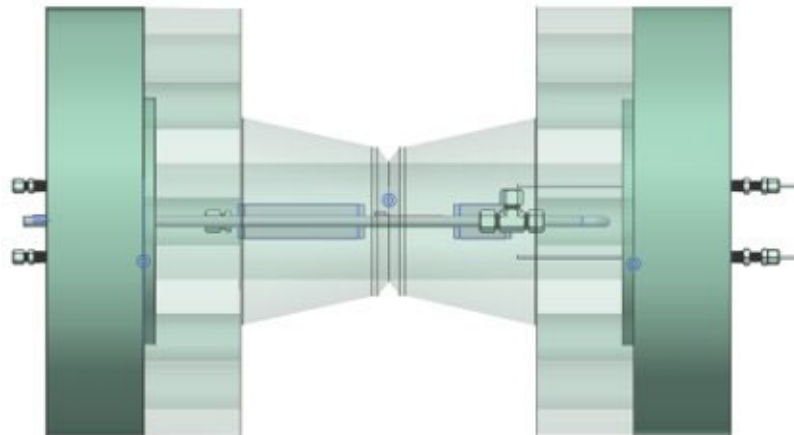
Vessel manufacturing

# sCO<sub>2</sub> Pin Fin heat transfer

- Pin Fin test section, housed within steel pressure vessel
- Maximum operating pressure 200 bar
- Maximum operating temperature 450°C
- Maximum Mass Flow Rate: 0.2 kg/s
- Instrumentation for pin fin array averaged heat transfer coefficient estimation
- High pressure gland fittings for power transmission and instrumentation
- 14 pin rows in test section. Geometry based on Ames pin fin study



Test section pressure vessel

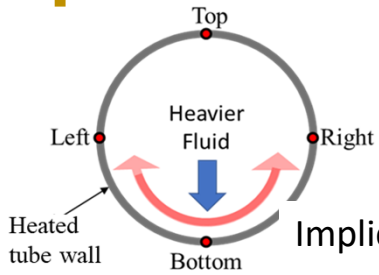


THANK YOU



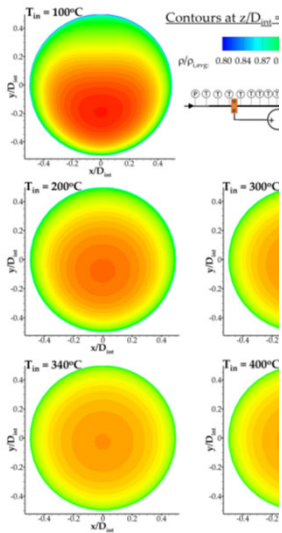
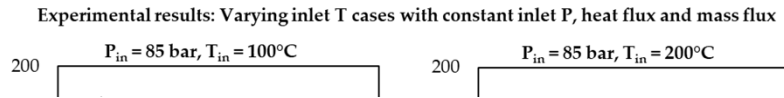
# Back up slide

# Impact of Inlet Temperature on buoyancy

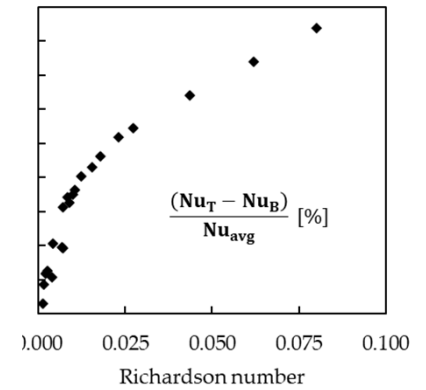
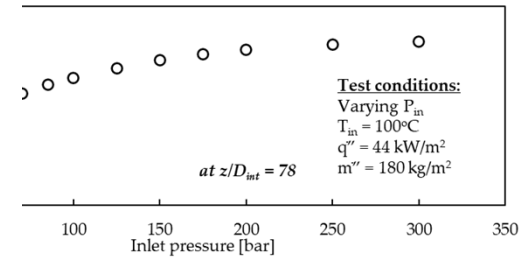
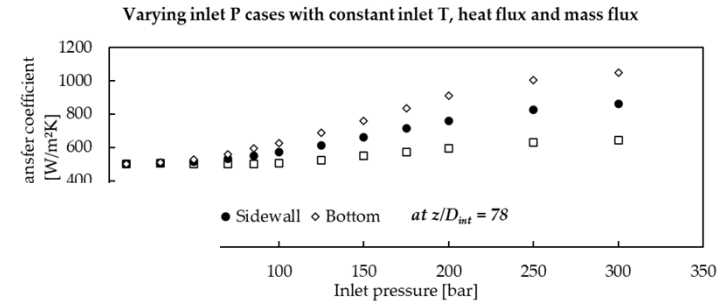


Implications to Cooling and compressor

Schematic showing formation of convection currents in a circular tube heated from the bottom

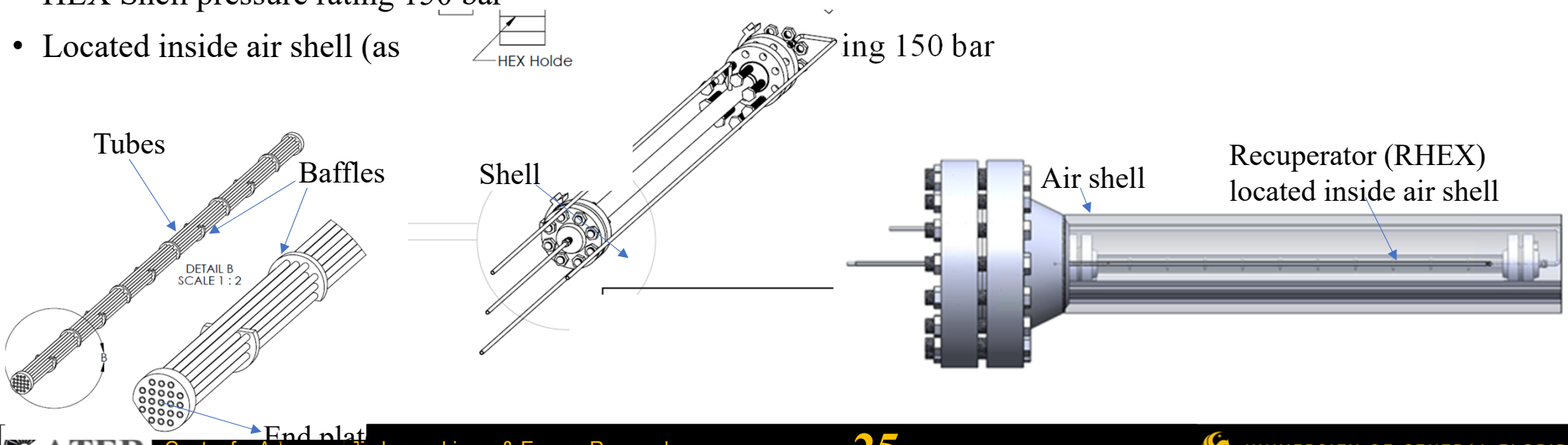


Density contours at various inlet temperatures



# Recuperator

- Recuperator is used to reduce heating and cooling requirements of the loop
- Shell and Tube design with tubes carrying hot CO<sub>2</sub>
- 1D design validated using conjugate heat transfer CFD simulations before fabrication
- Design Effectiveness = 70%
- Tested Effectiveness = 63%
- HEX Shell pressure rating 150 bar
- Located inside air shell (as

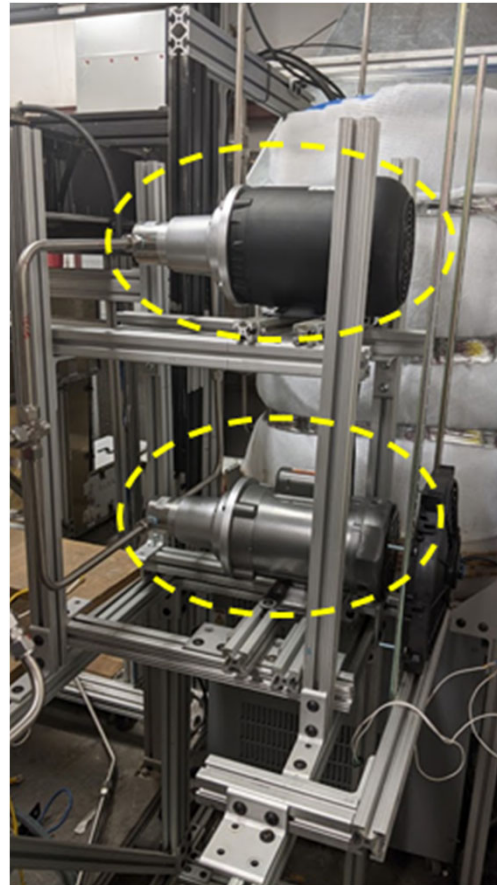


# Pumps in the loops



## Sigma pump plunger pump

- Max inlet temperature = 37°C
- Pressure on suction inlet of the pump
  - Min 80 bar, Max 260 bar
- Pressure on discharge outlet of the pump
  - Min 120 bar, Max 300 bar
- Max differential pressure = 40 bar
- Mass flow rate range
  - 0.66-16.5 L/min *OR* 0.01-0.25kg/s @910 kg/m<sup>3</sup>



## Micropump gear pump

- Max inlet temperature = 150°C
- Maximum system pressure = 103 bar
- Max differential pressure = 8.7 bar
- Mass flow rate range
  - 3.21 L/min *OR* 0.05kg/s @910 kg/m<sup>3</sup>

# Coolers in the loop

- *Each heat exchanger is custom-designed and in-house fabricated*
- Air cooler to cool CO<sub>2</sub> from higher temperatures to 50-80°C
- Water cooler to cool CO<sub>2</sub> to 25-30°C (required at inlet of recirculating pump)

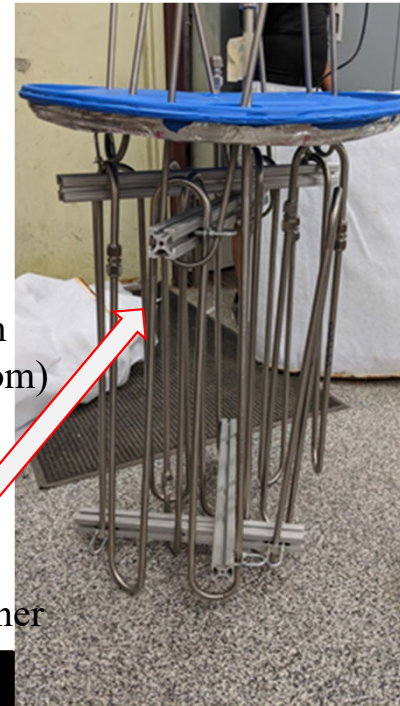
## Air cooler

- Finned tube bank over the fan (left bottom)
- Canopy+duct for fan exhaust out of the room
- Dielectric union is connected between air cooler and water cooler
- Flow TC between air and water cooler to monitor temperature going into water cooler below ~90°C

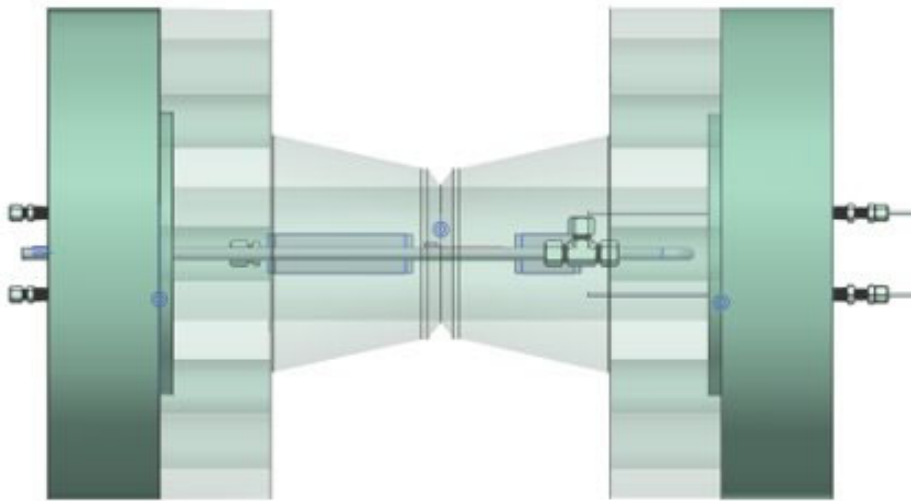


## Water cooler

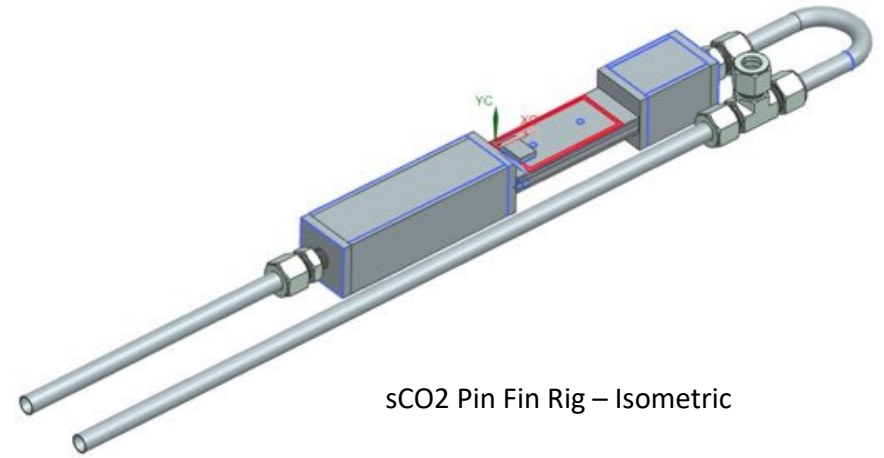
- Tube bank for CO<sub>2</sub>
- Insulated water drum with distilled water (right bottom)
- 2 re-circulating pumps inside for increased convection
  - Bottom to top and Tangential to inner



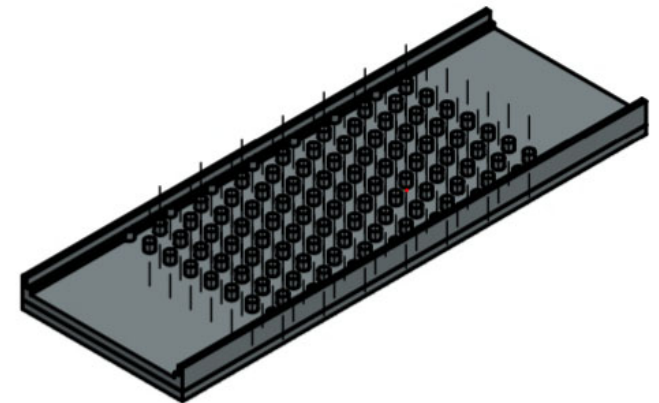
# Pin Fin Rig – Part Allocation



Rig Design for Experimental Processes



sCO<sub>2</sub> Pin Fin Rig – Isometric



sCO<sub>2</sub> Pin Fin Rig – Test Section Internal