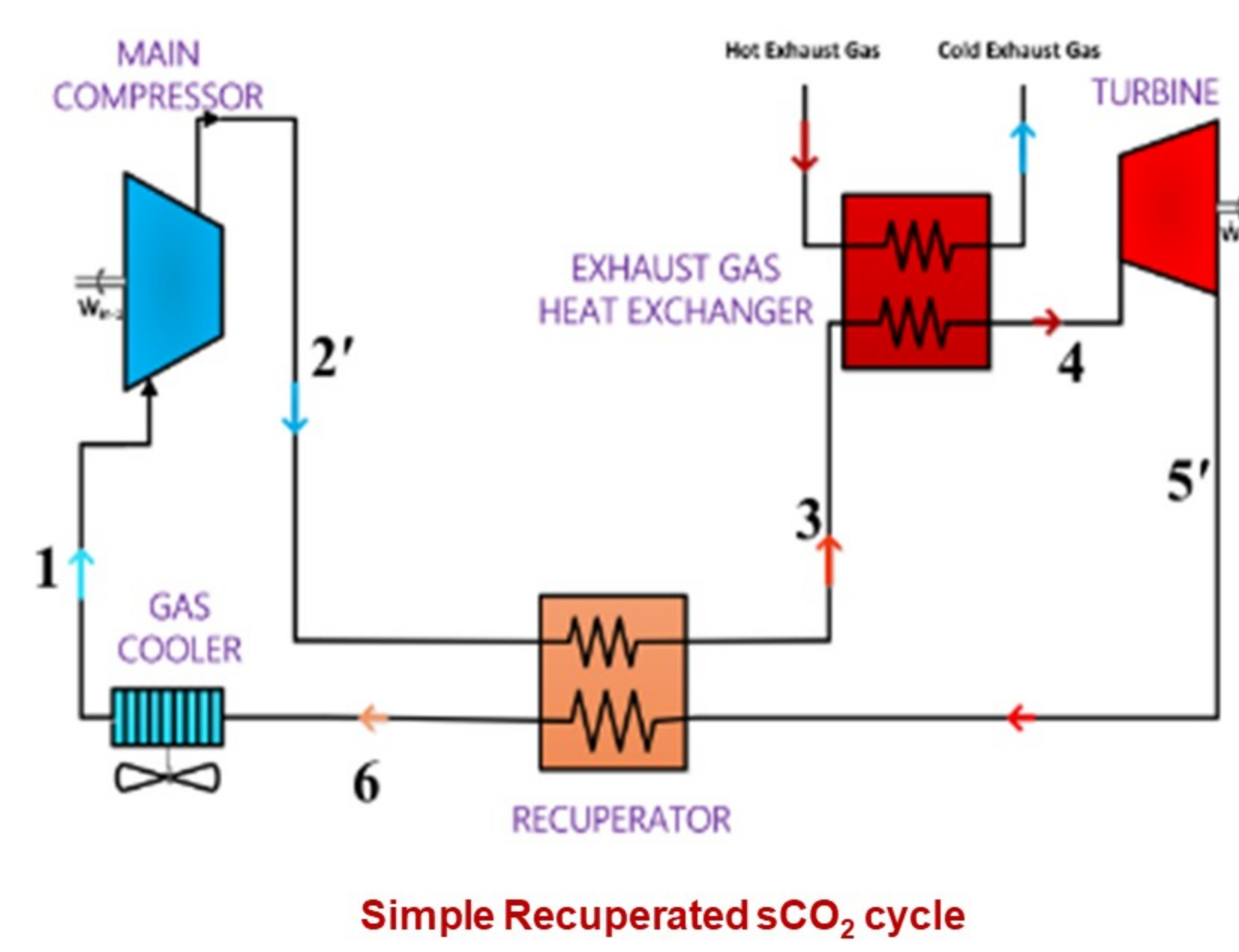


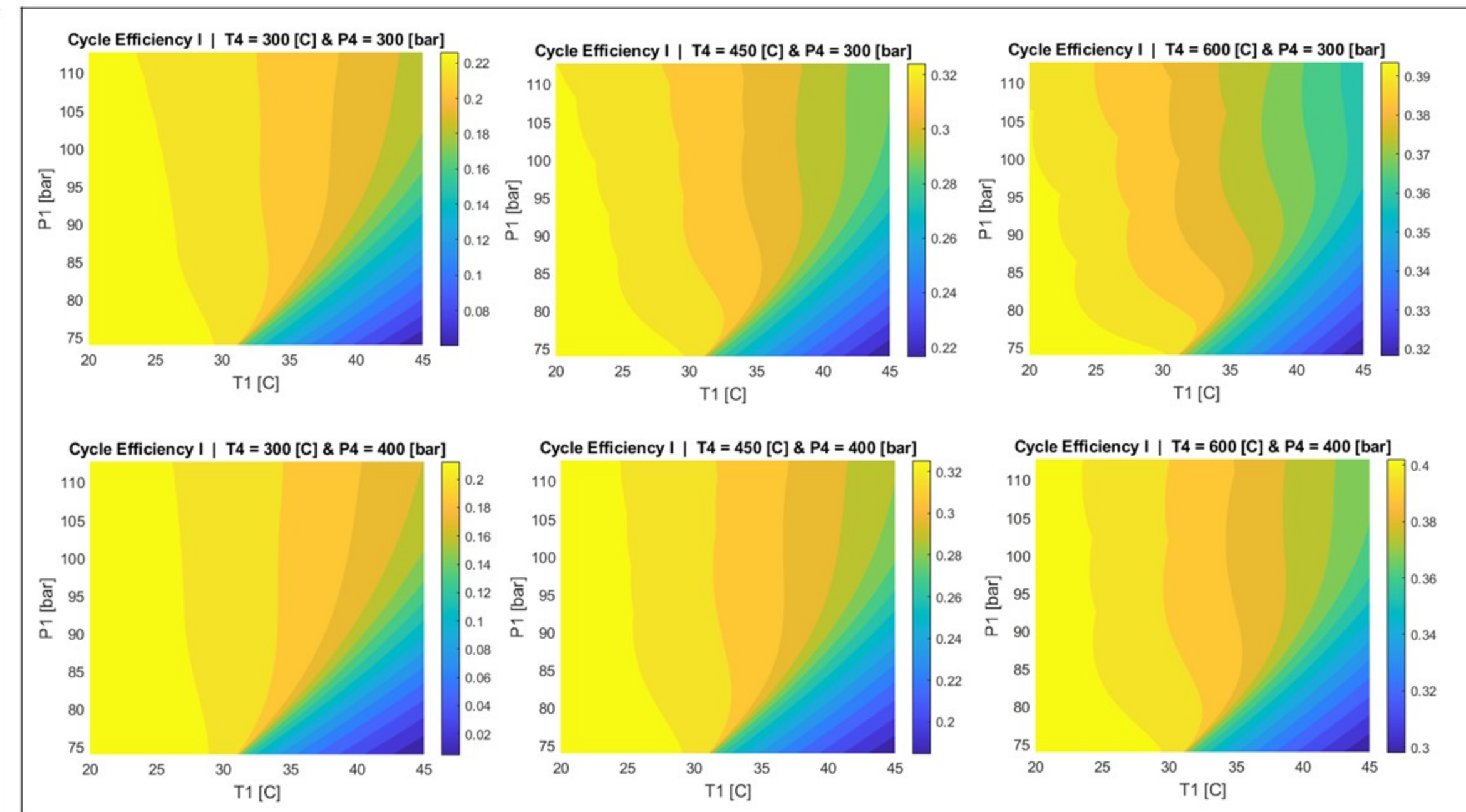
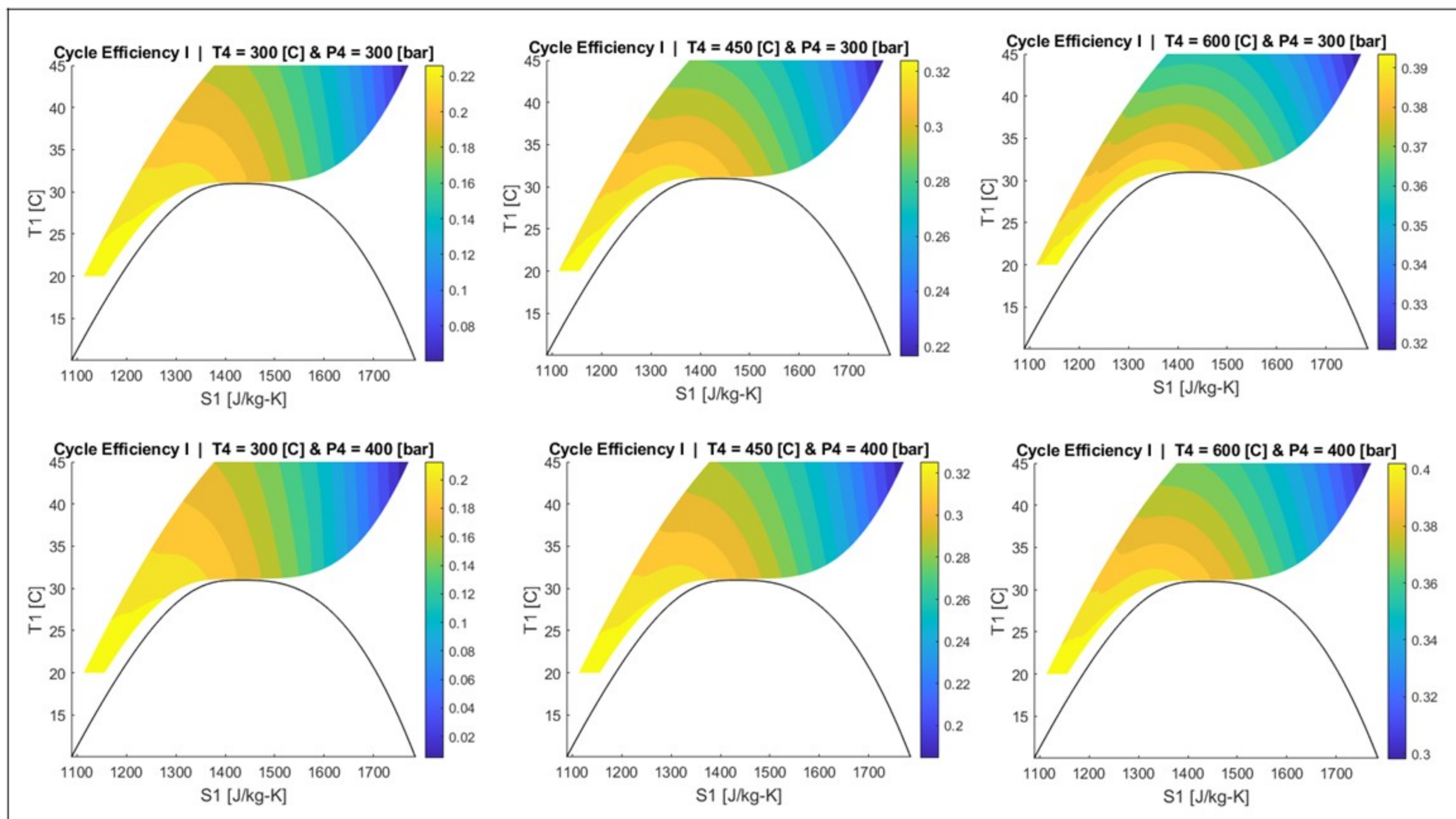
# Test rig design for experimental characterisation of condensation in sCO<sub>2</sub> compressors

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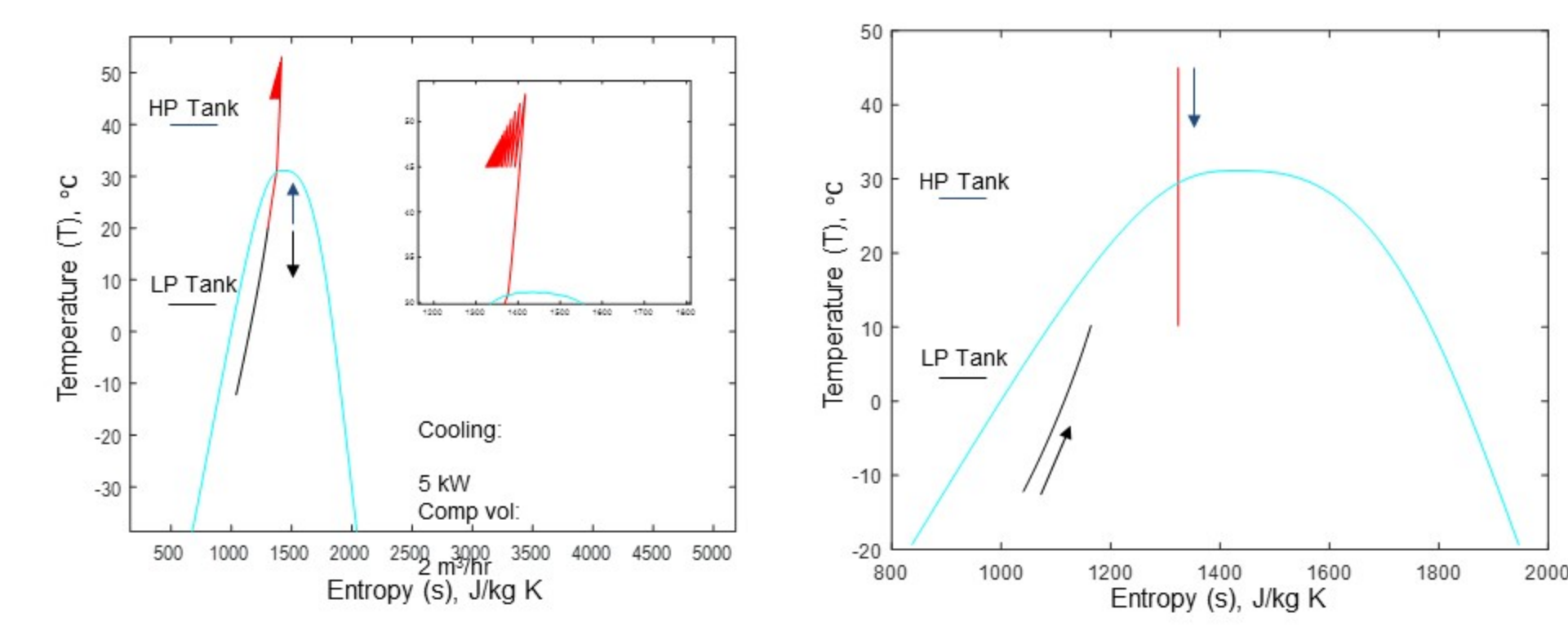
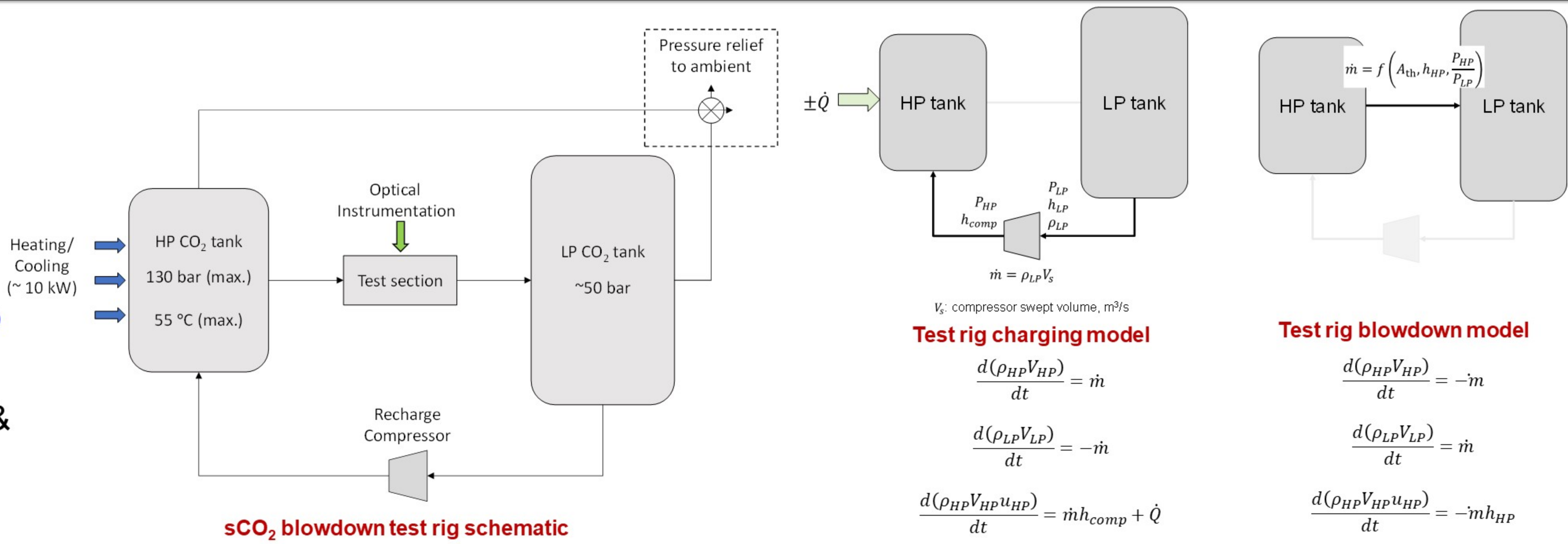
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- Industrial WHR potential
  - ~1000 TWh
  - 30% High Temperature (> 270 °C) waste heat stream
- sCO<sub>2</sub> WHR power range
  - 100 kW to 50 MW
- Simple recuperated cycle
  - Best trade-off between efficiency and cost



- Experimental characterisation to study:
  - Condensation effects @ compressor inlet
  - Validate/update property routine
  - Compare and update numerical 1D and 3D CFD codes
- Assess sCO<sub>2</sub> compressor efficiency & operation



Parameter	HP Tank	LP Tank	Compressor
Total CO <sub>2</sub> charge, kg	100	100	-
Volume, liter	100	185	-
Operating Pressure, bar	130	50	-
Operating Temperature, °C	Min: 32 Max: 55	-20	-
Volumetric flow rate, m <sup>3</sup> /hr	-	-	Min: 1 Max: 4
Cooling capacity with water circuit, kW	10	-	-

Test rig charging model

$$\frac{d(\rho_{HP} V_{HP})}{dt} = \dot{m}$$

$$\frac{d(\rho_{LP} V_{LP})}{dt} = -\dot{m}$$

$$\frac{d(\rho_{HP} V_{HP} u_{HP})}{dt} = \dot{m} h_{comp} + \dot{Q}$$

$$\frac{d(\rho_{LP} V_{LP} u_{LP})}{dt} = -\dot{m} h_{LP}$$

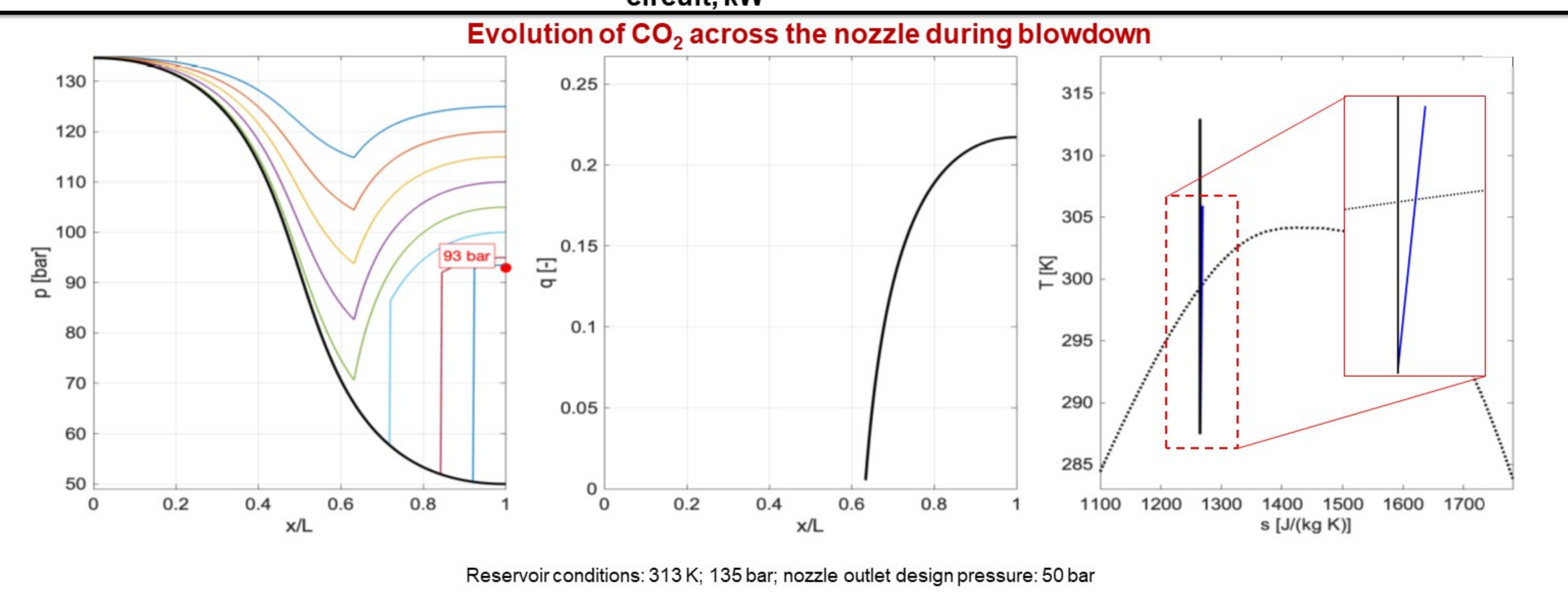
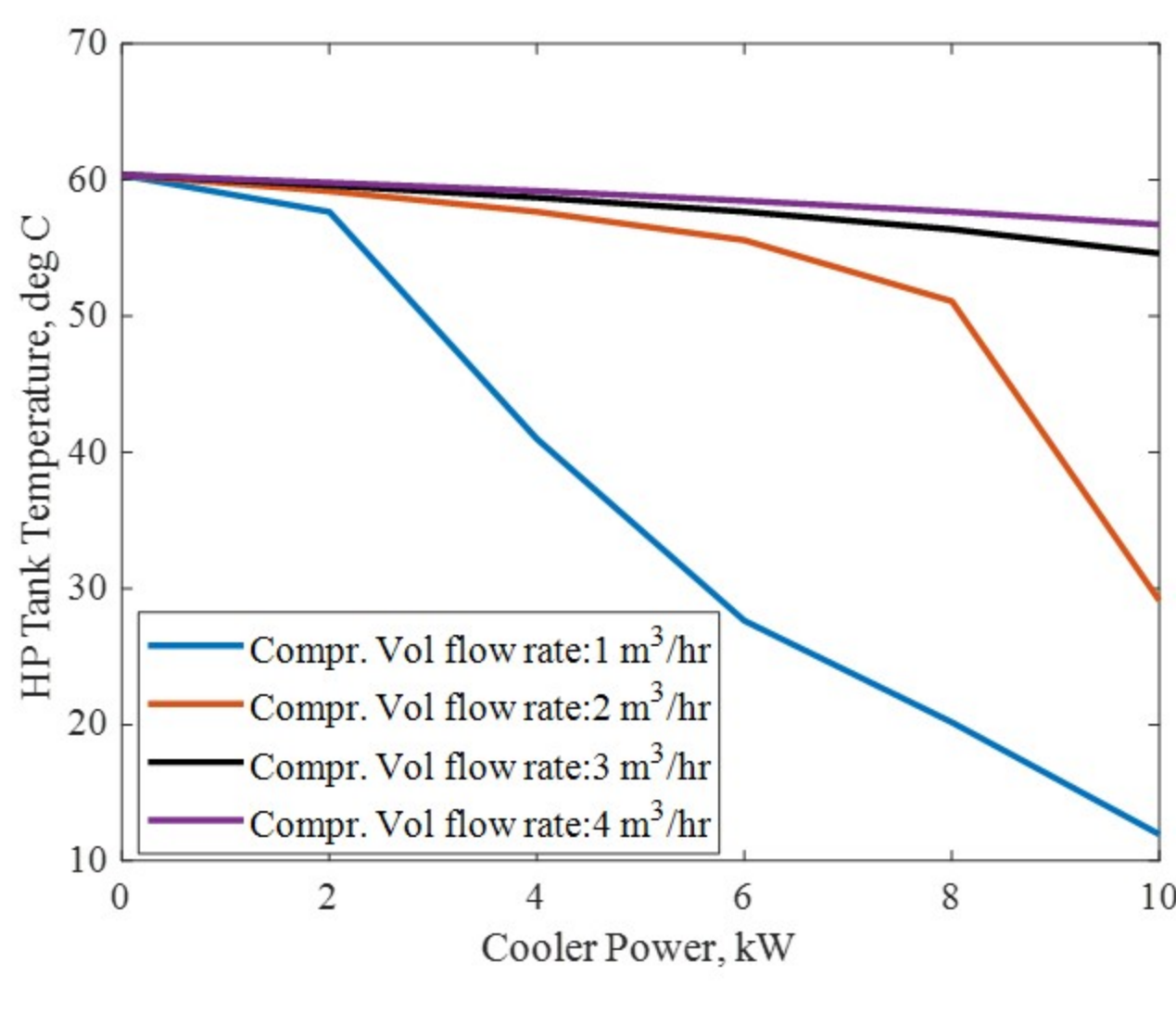
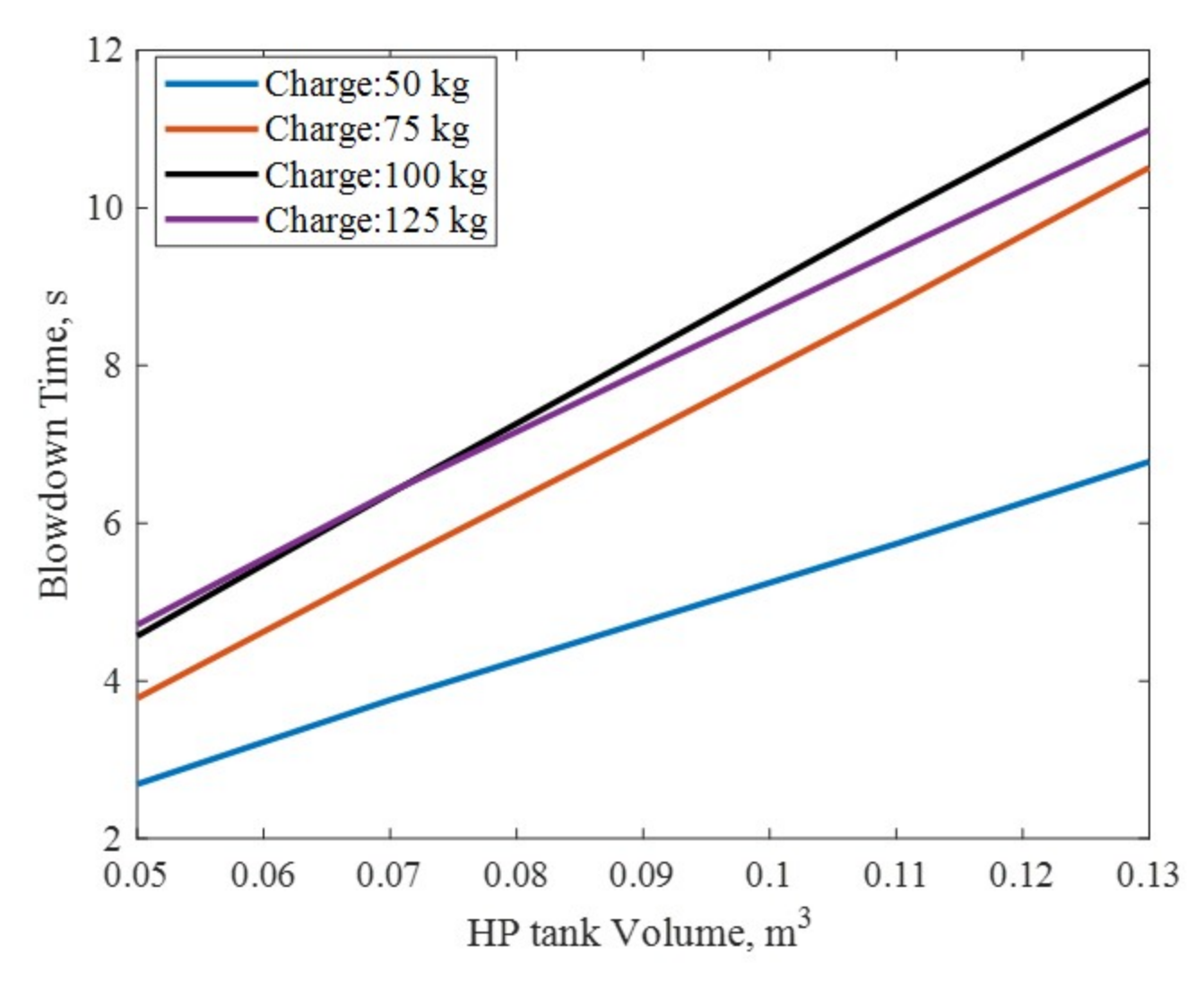
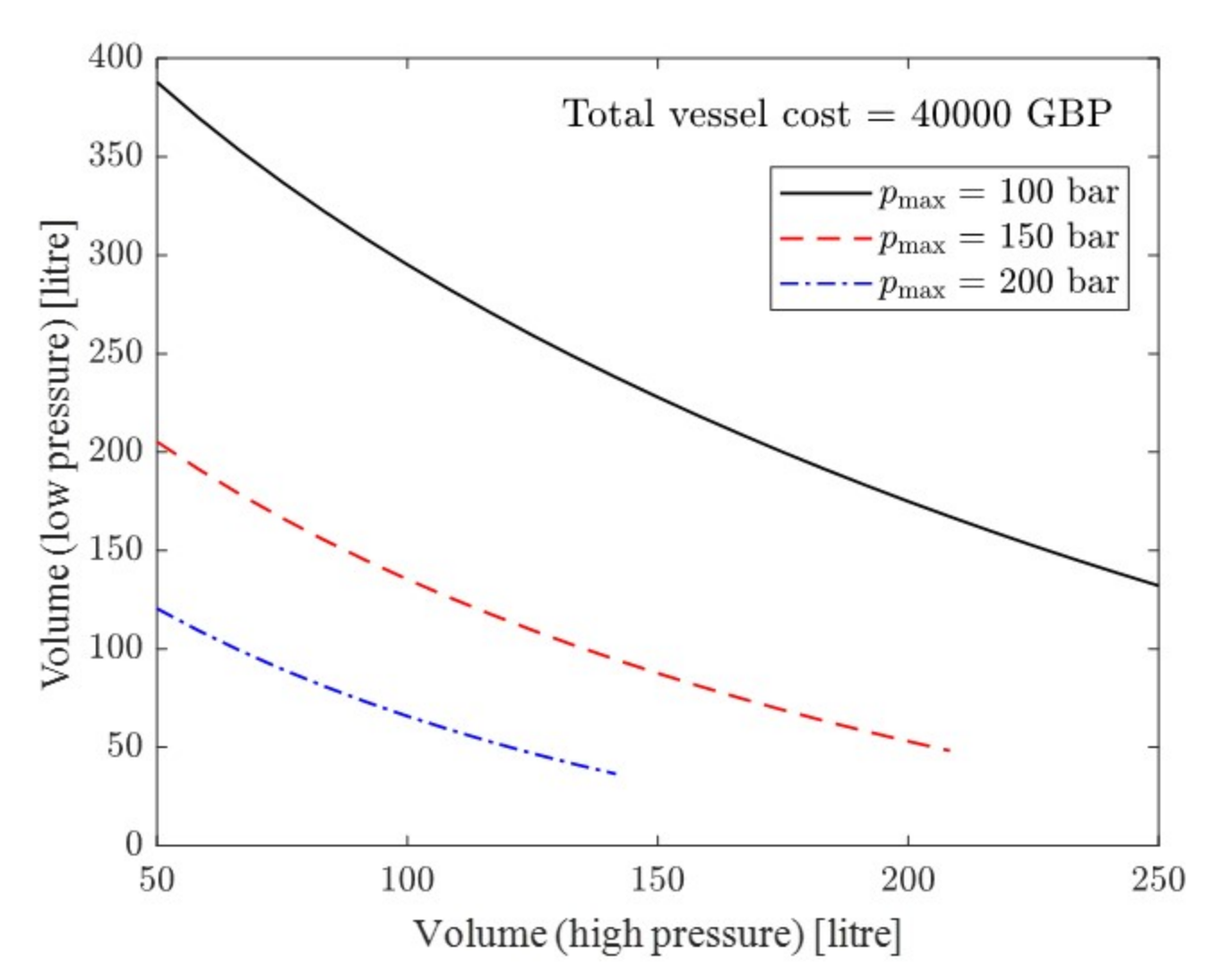
Test rig blowdown model

$$\frac{d(\rho_{HP} V_{HP})}{dt} = -\dot{m}$$

$$\frac{d(\rho_{LP} V_{LP})}{dt} = \dot{m}$$

$$\frac{d(\rho_{HP} V_{HP} u_{HP})}{dt} = -\dot{m} h_{HP}$$

$$\frac{d(\rho_{LP} V_{LP} u_{LP})}{dt} = \dot{m} h_{HP}$$



Left: pressure profile for a fixed reservoir condition and variable outlet pressure:  $p_{out} < 93$  bar normal/oblique shock occurs at the nozzle exit leading to a full expansion within the nozzle, and two-phase conditions expected within the nozzle.  
 Centre: expected vapour qualities in the nozzle. Right: possibility of shocks transitioning from two-phase conditions upstream of the shock, and supercritical conditions downstream of the shock