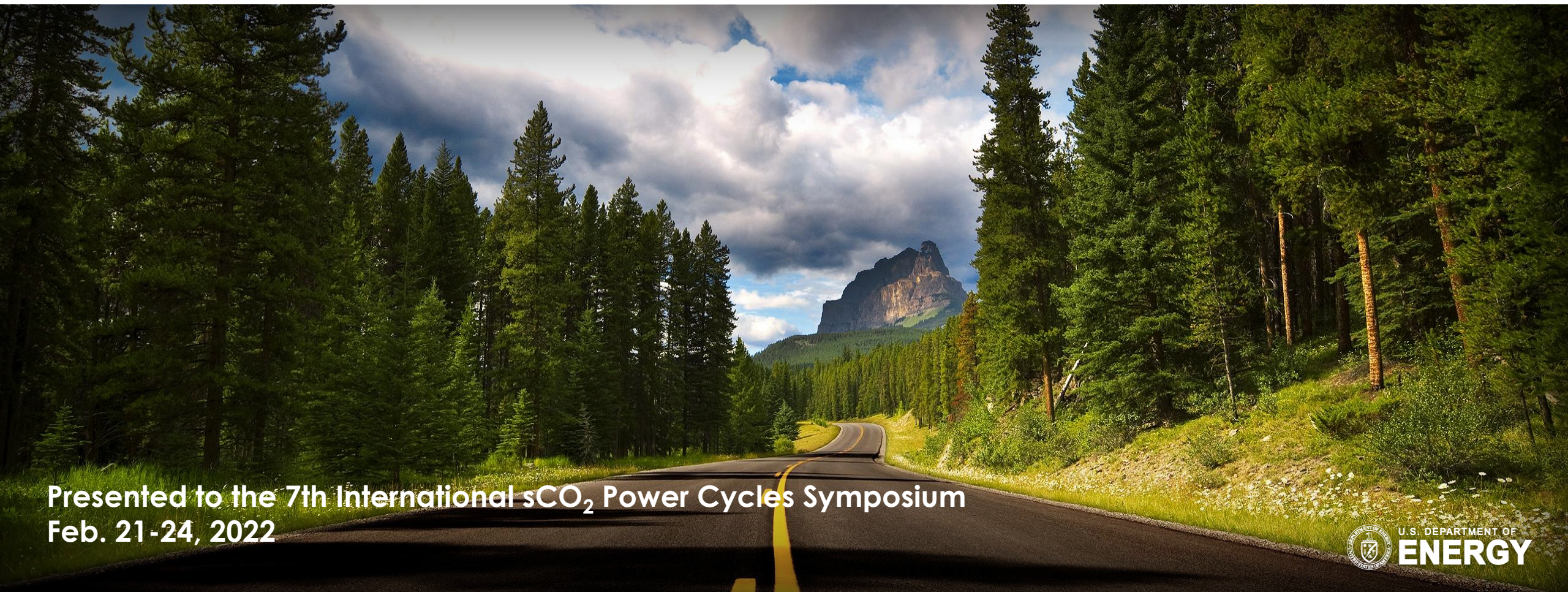


# Mechanical Degradation of Ferritic/Martensitic and Austenitic Steels in CO<sub>2</sub> Environment



Kyle Rozman  
Research Scientist  
Research & Innovation Center



Presented to the 7th International sCO<sub>2</sub> Power Cycles Symposium  
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# Disclaimer



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## Research and Innovation Center

- The Advanced Turbines Program at NETL conducts R&D for directly and indirectly heated supercritical carbon dioxide-based power cycles for fossil fuel applications.
- The focus is on components for indirectly heated fossil fuel power cycles with turbine inlet temperature in the range of 1300 - 1400°F (700 - 760°C) and oxy-fuel combustion for directly heated supercritical CO<sub>2</sub> based power cycles.
- Materials issues involve quantification of creep, fatigue, oxidation and other mechanical and chemical processes in sCO<sub>2</sub> and gaseous CO<sub>2</sub> environments.



<https://netl.doe.gov/onsite-research/materials>

<https://netl.doe.gov/node/7552>

# Introduction

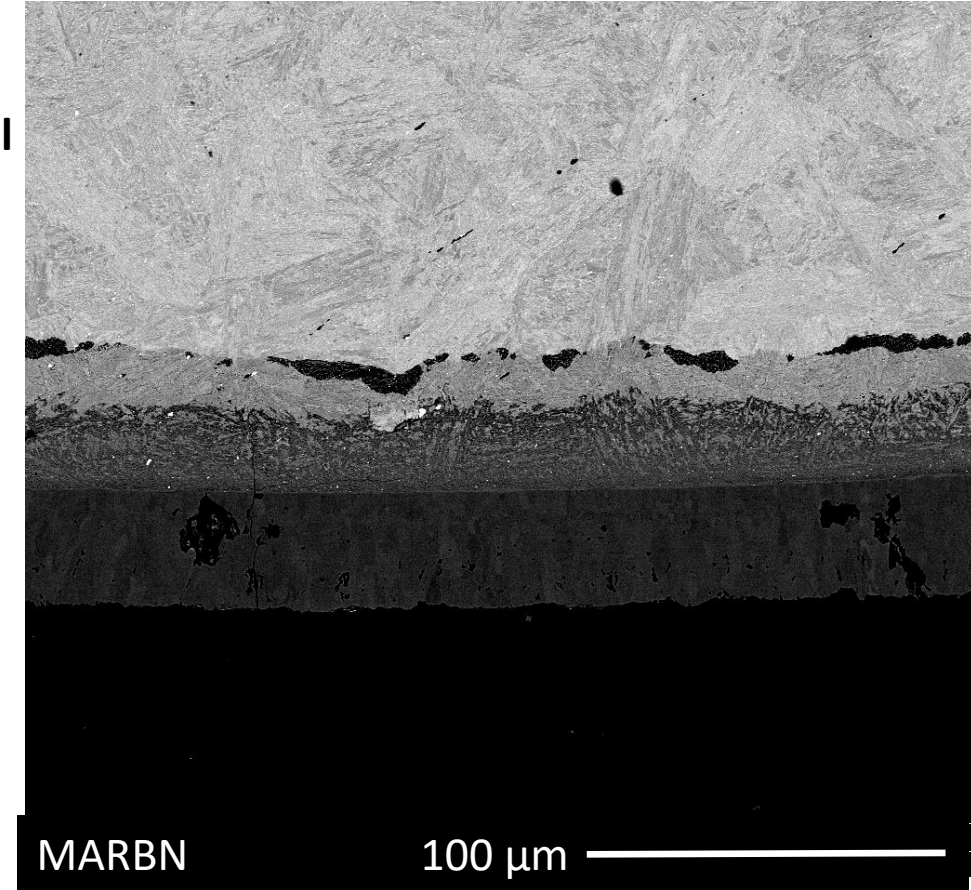
## Oxidation:

- **9% Wt. Cr steels under CO<sub>2</sub>**
  - Form duplex Fe-rich oxide scales following parabolic growth
  - Subject to enhanced carburization
- **Austenitic Stainless (18-25% Wt. Cr.)**
  - Protective Cr-rich scale is known to be interrupted in CO<sub>2</sub>

Base metal

Cr rich

Fe rich



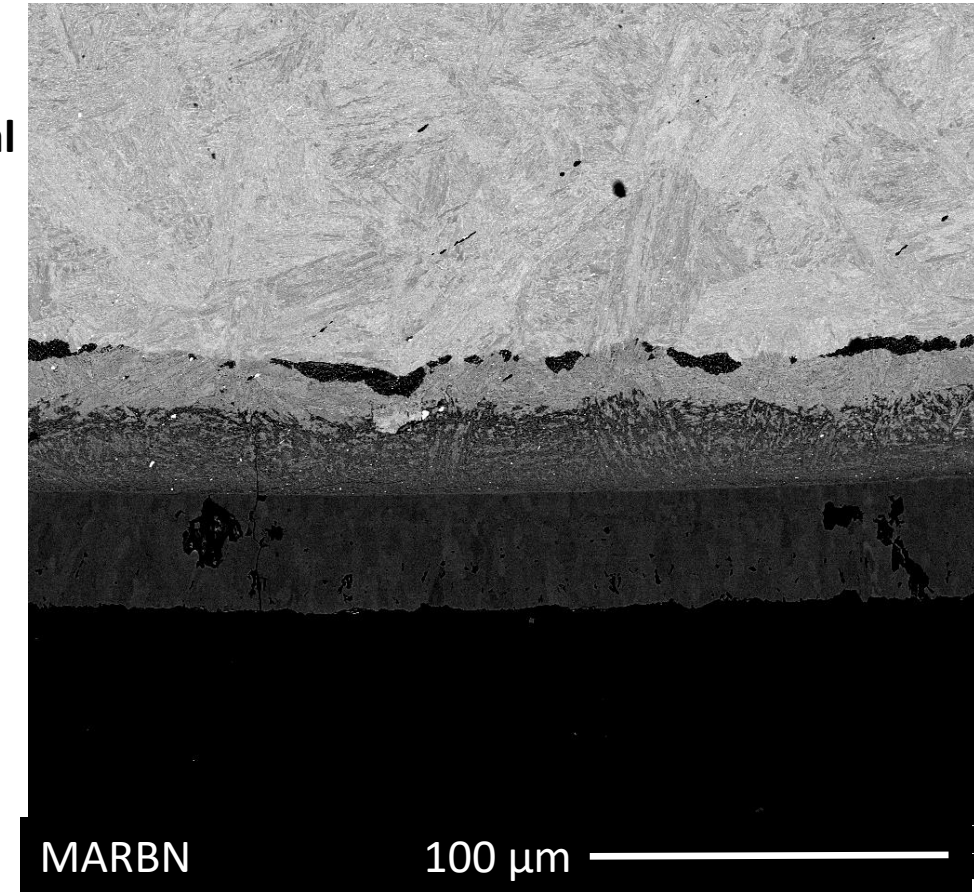
## Mechanical Properties:

- ***Exsitu* tests not showing difference after 500+ hour exposures, except in thin sections or with additions of H<sub>2</sub>O, O<sub>2</sub> gases**
  - Both steels and superalloys
- ***Insitu* testing is more complex**
  - Ethelene cracking experiments show severe carburization
  - Autoclave testing IN600 alloy only showed loss of creep life in sCO<sub>2</sub>

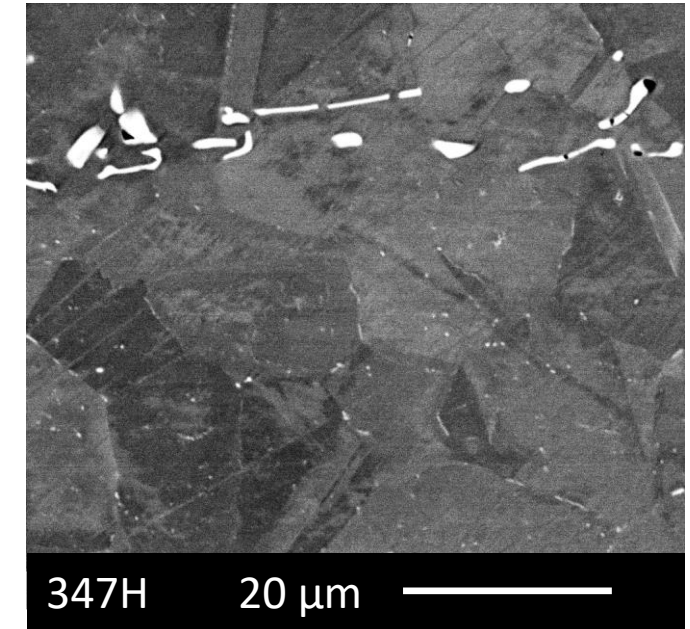
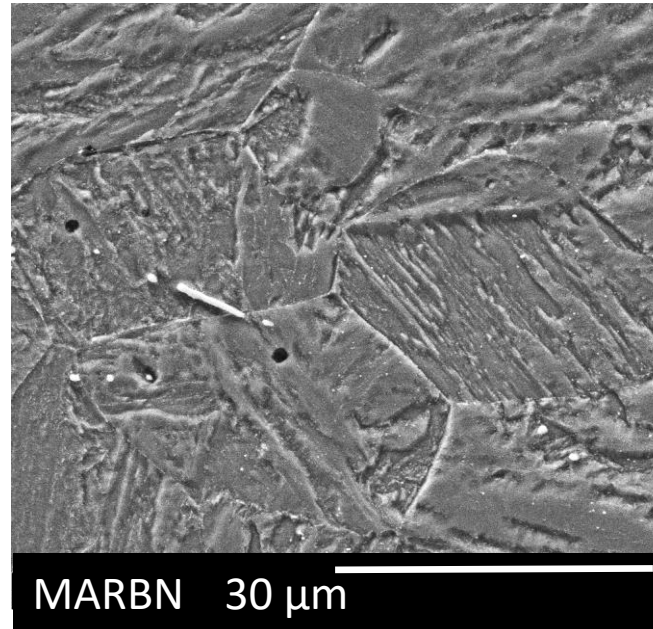
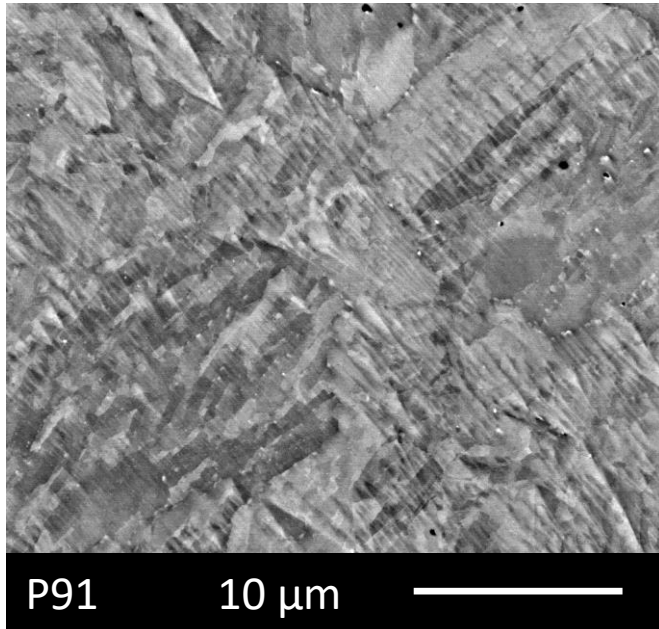
Base metal

Cr rich

Fe rich

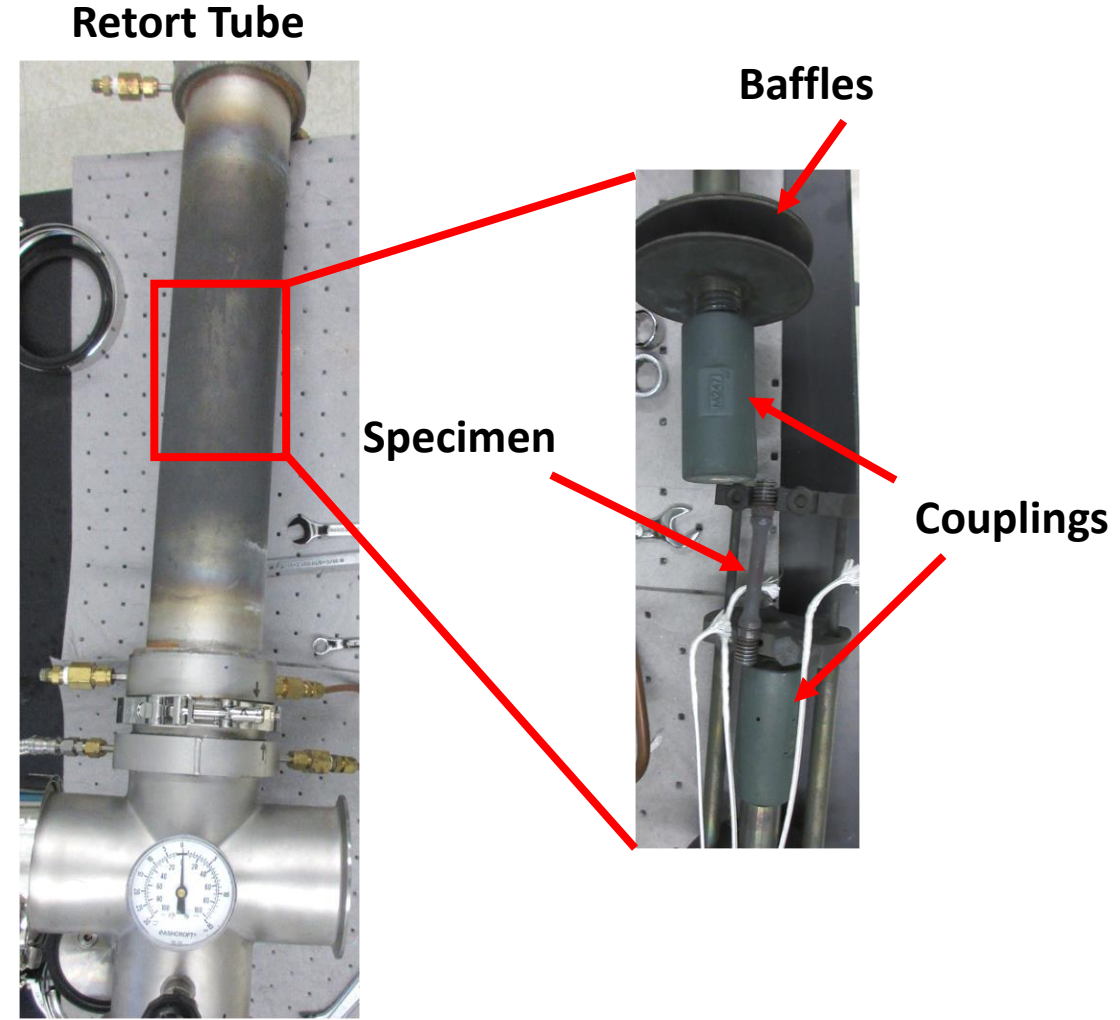


- P91, 9% Cr steel, Martensitic / Ferritic
- MARBN, 9% Cr steel, Martensitic
- 347H, 17.3% Cr stainless steel, Austenitic with Nb-rich carbides



# Methods

- Oxidation experiments performed in tube furnace
  - 2.54, 0.6 and 0.5 mm thick dogbone specimens
  - Surface finish of 600 grit
  - 650°C, CO<sub>2</sub> with 4% H<sub>2</sub>O and 1% O<sub>2</sub> by volume.
  - 10<sup>-6</sup> Torr Vacuum
  - 1000-hour exposure
- Tensile tests
  - 2.54, 0.6 and 0.5 mm thick dogbone specimens pre-exposed as above
  - ASTM E-8 test methodology
  - 3.3\*10<sup>-5</sup> / s strain rate to failure
- Creep testing
  - Cylindrical specimens
  - No pre-exposures
  - Retort tube controls environment at ambient pressures only
  - 207 MPa applied load at 650°C tested to failure





# Pre-Exposure / Oxidation Results

- Tensile specimens were exposed to DF4 environment for 1000 h prior to testing
- P91 showed similar mass gain for both thicknesses
- Spallation led to reduction in mass gain for thin 347H specimen
- Thicker 347H specimen only had ~15% of the mass gain of P91 under the same conditions

Alloy	Specimen Thickness (mm)	Mass gain (mg/cm <sup>2</sup> )
P91	0.50	29.0
P91	2.54	28.0
347H	0.60	-6.0
347H	2.54	4.6

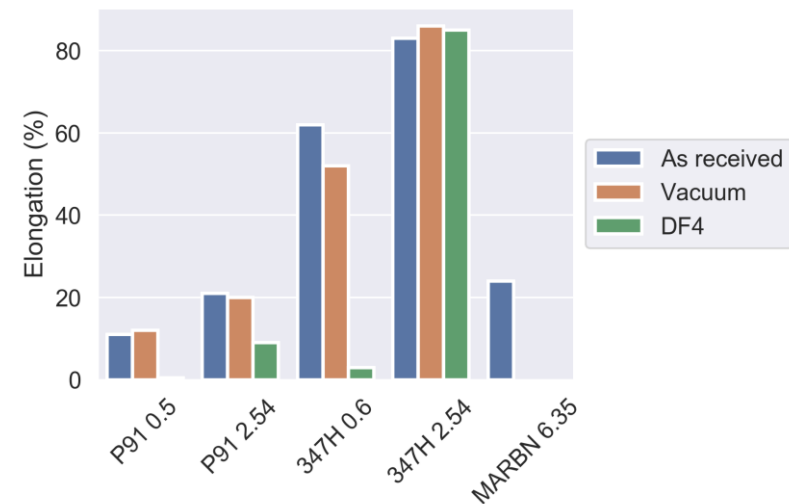
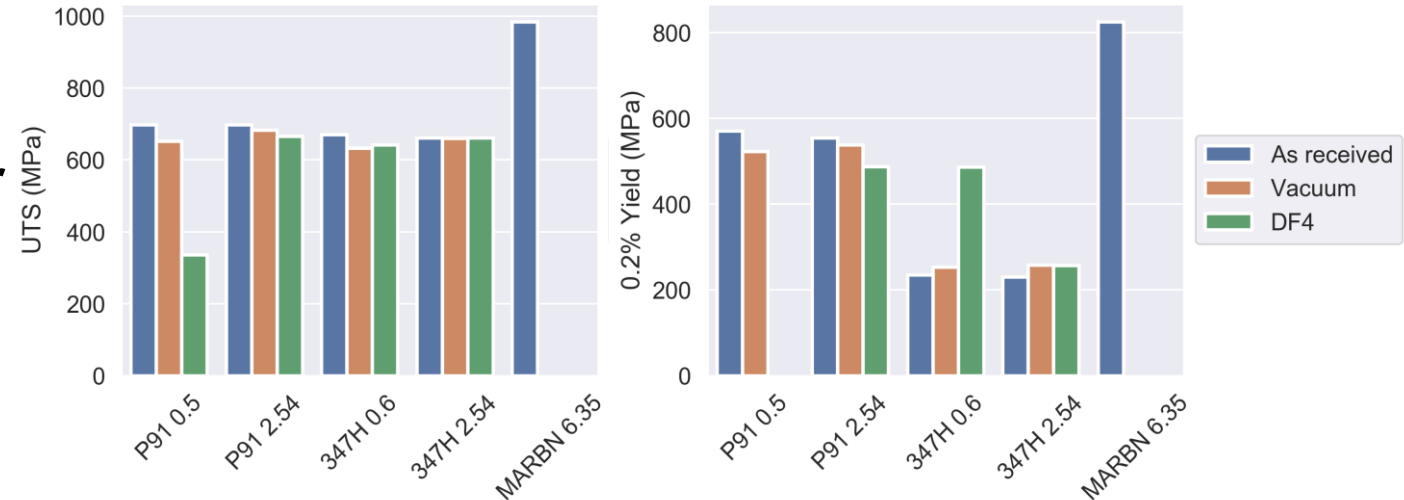
# Tensile Results

## P91 Steel

- No significant changes noted from specimen thickness under vacuum exposures
- Thin specimen failed before yielding
- Thicker specimen's YS and UTS unchanged, but elongation was reduced by 57%

## 347H

- Only notable change from the thin section, which YS doubled and elongation severely reduced

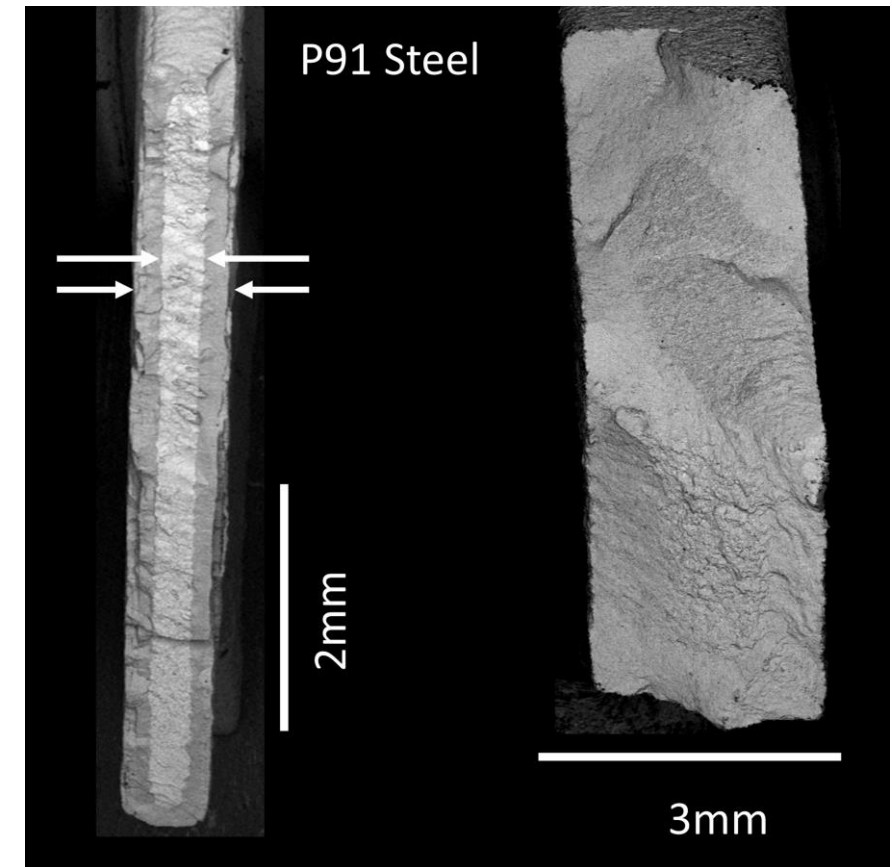


# Tensile Fracture Surfaces – P91

- **Thick specimen showed**
  - ~0.8mm enhanced carburization zone around the perimeter
  - No shear lip formation, suggesting embrittlement
- **Thinner specimen showed**
  - Severe embrittlement
  - Electron backscatter shows oxidation/carburization effected zone penetrating to ~0.2 mm (including oxidation scale)

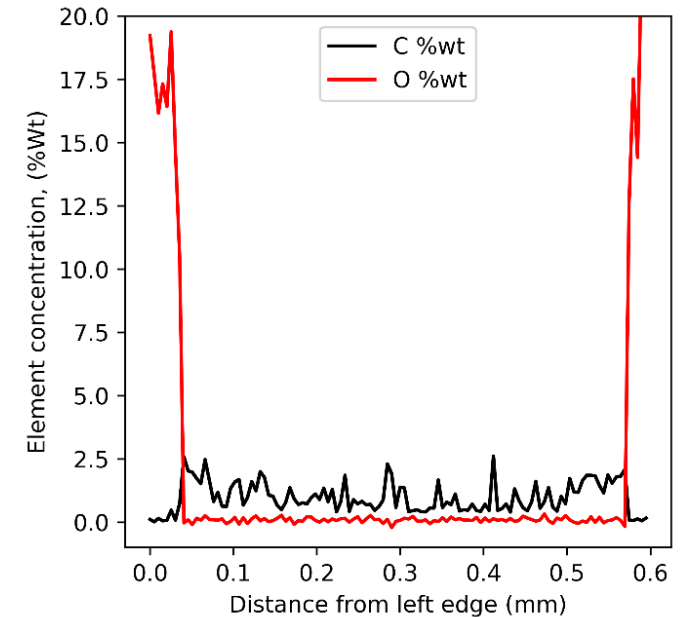
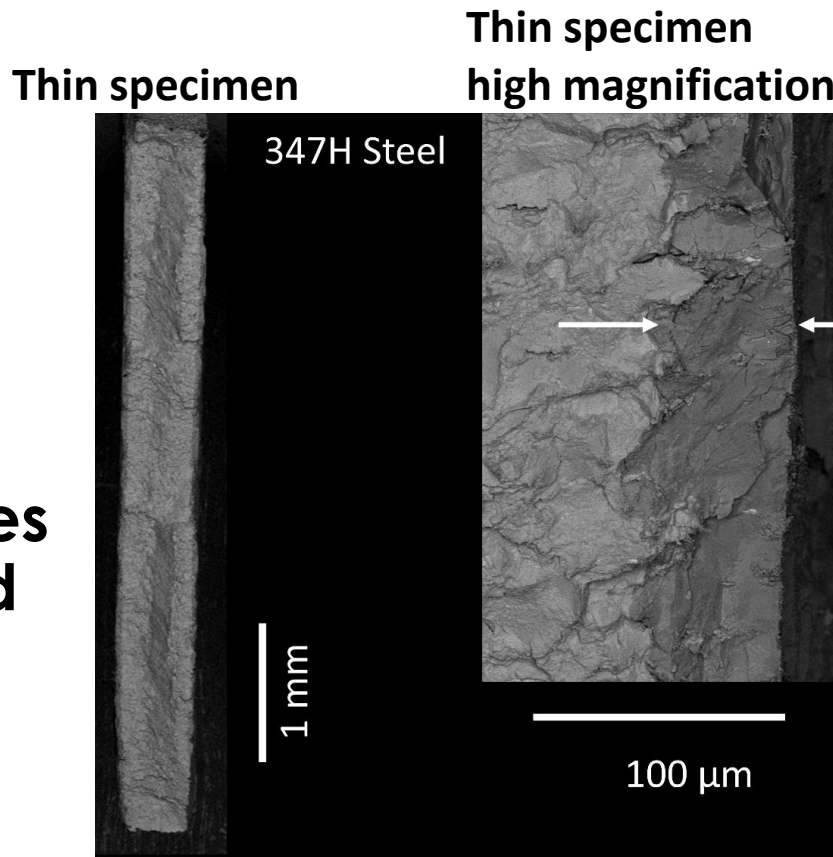
Thin specimen

Thick specimen



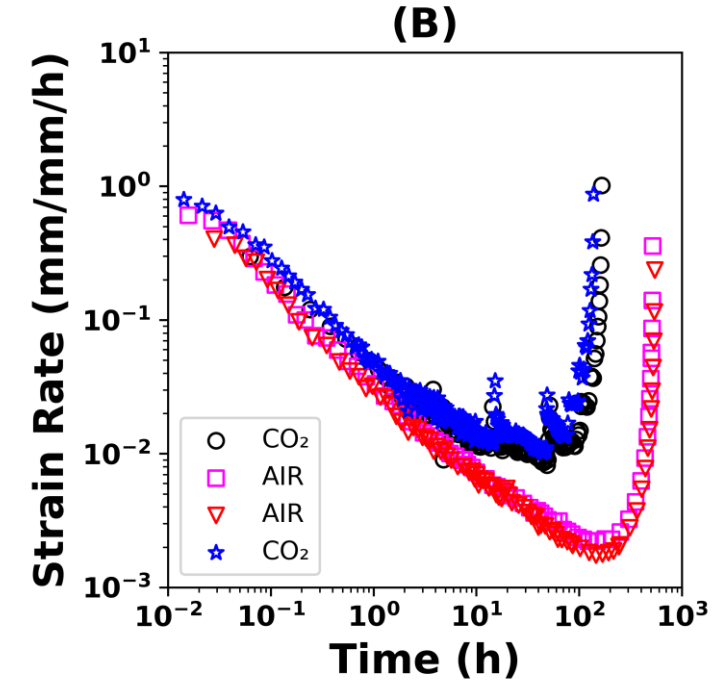
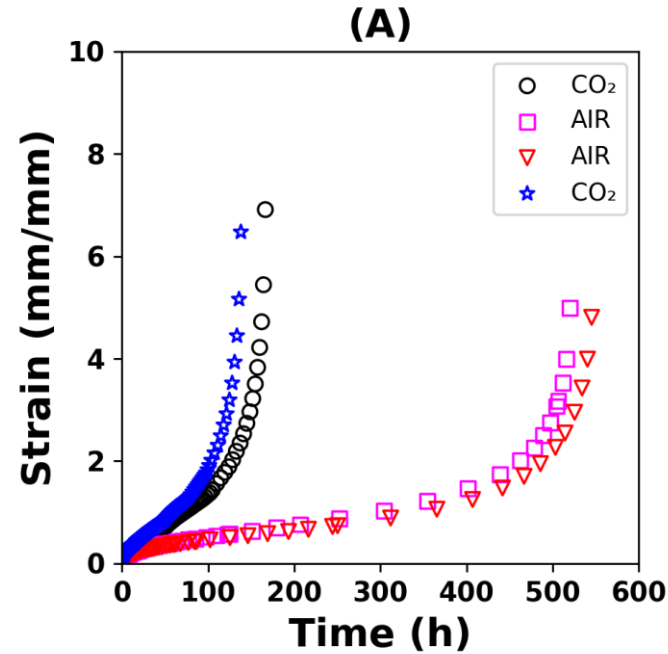
# Tensile Fracture Surfaces – 347H

- Only Thin specimen featured
- Specimen failed at 45° incline plane, suggesting shear ductility
- High magnification shows phase contrast ~50 μm deep
- Microprobe analysis verifies this to be oxidation related



# Creep Results

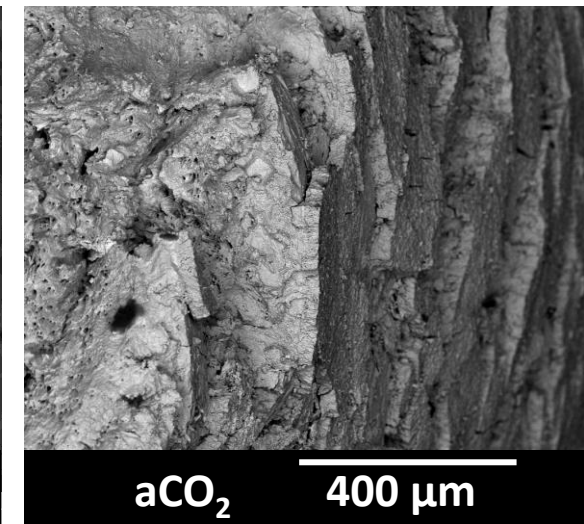
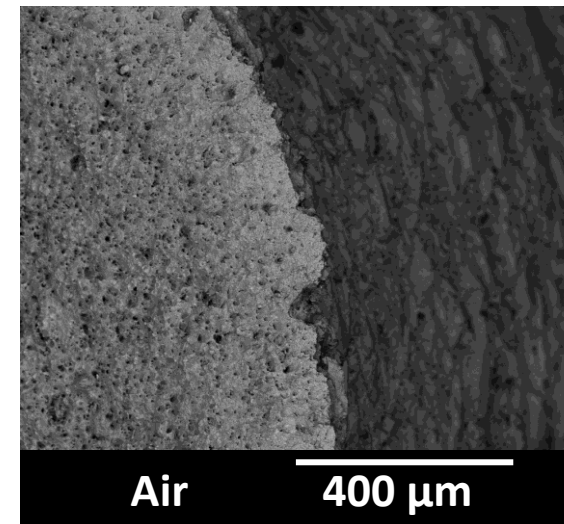
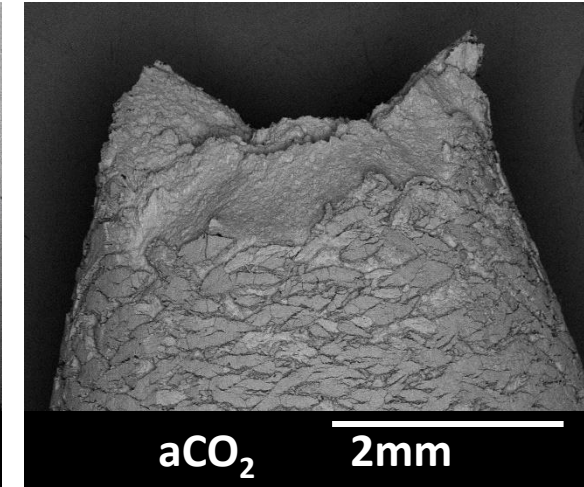
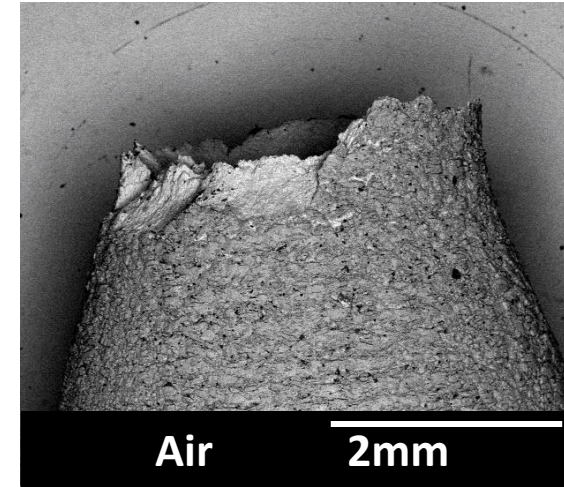
- MARBN and 374H tested to date
- Tests conducted in controlled environment retort tube
  - 100 sccm CO<sub>2</sub>, 650°C, ~207 MPa
- MARBN alloy showed
  - ~3.5X reduction in time to failure
  - ~1 decade faster MCR
- Faster MCR suggest mechanisms change



Alloy Designation	Test Temperature (°C)	Stress Level (MPa)	Time to Failure (h)	Elongation to Failure (%)	Reduction in Area (%)	Minimum Creep Rate (%/h)	Larson Miller Parameter, C=25
MARBN - Air	650	206.84	527	13.2	64.4	2.21·10 <sup>-3</sup>	25586.18
MARBN - Air	650	206.84	545	12.6	69.9	1.74·10 <sup>-3</sup>	25605.15
MARBN - CO <sub>2</sub>	650	206.84	169	16.1	67.3	8.20·10 <sup>-3</sup>	25129.21
MARBN - CO <sub>2</sub>	650	206.84	140	14.7	58.3	1.00·10 <sup>-2</sup>	25054.18

# Fracture Surfaces - MARBN

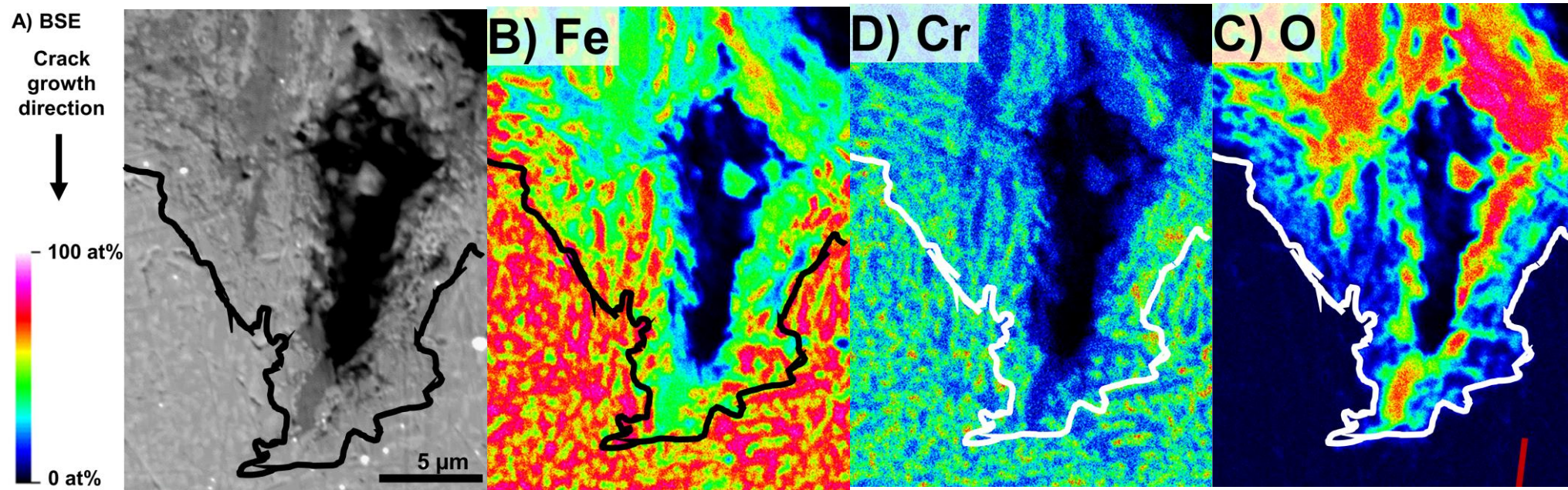
- Left images are from air, right from gaseous CO<sub>2</sub>
- Brittle failure near specimen edge
- Cross sectioned samples
  - Hardness and etching revealed carburized zone penetrated ~200 μm deep



Rozman et al., 2021, Mat Sci Engr A, 826, #141996

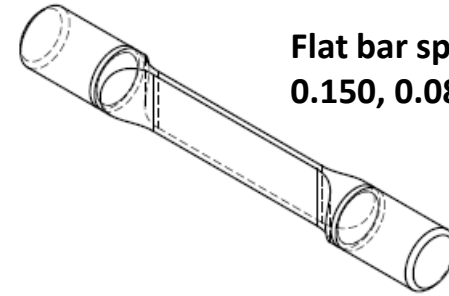
# Cross Sections - MARBN

- Found complex interactions between oxide growth and enhanced carburization
- Carburization tied up Cr
- Less Cr to form protective chromia scale
- Feed back mechanism to enhance environmentally assisted cracking
- As evidenced by microprobe analysis and change in MCR

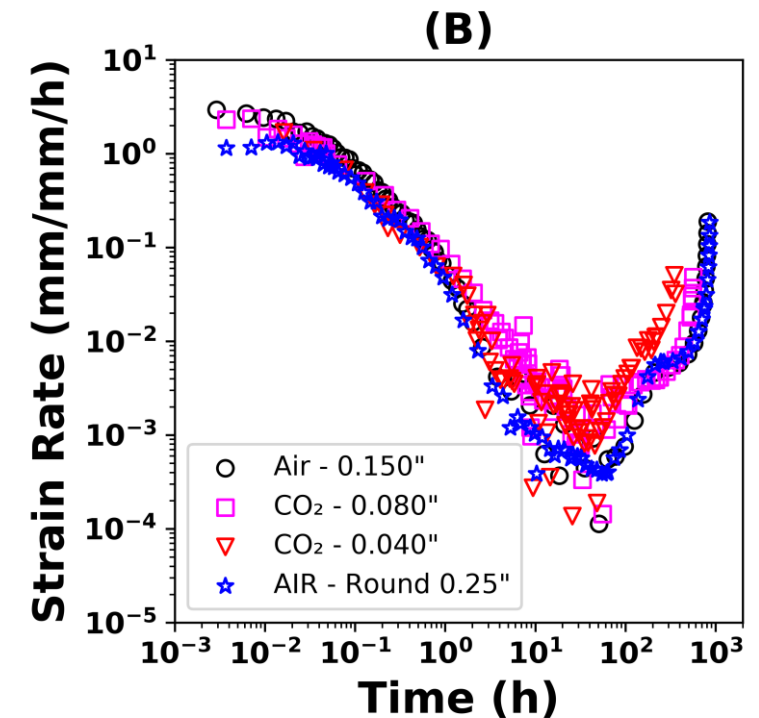
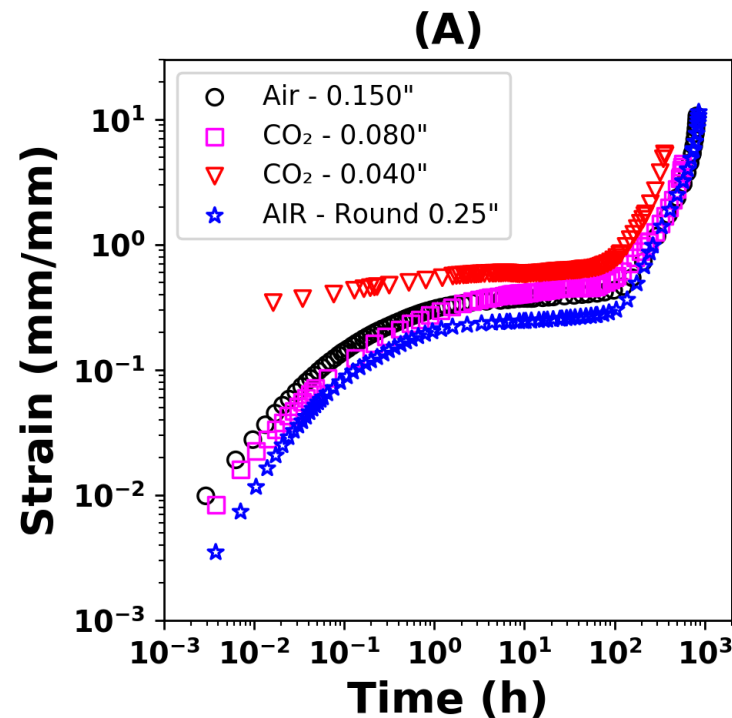


# Creep Results – 347H

- Creep tests on going
  - 650C, 197 MPa
  - Evaluating both effect of thickness and environment
- To date no change NETL has found
  - Reduced creep life
  - Slight increase in MCR
  - Suggests no mechanism change



Flat bar specimen to maximize surface area  
0.150, 0.080, 0.040, 0.020 inch thicknesses

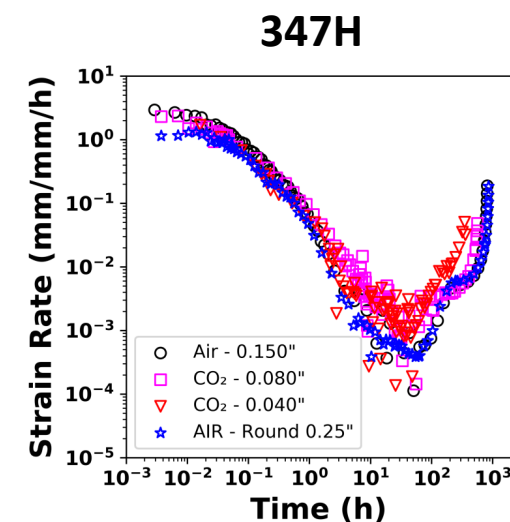
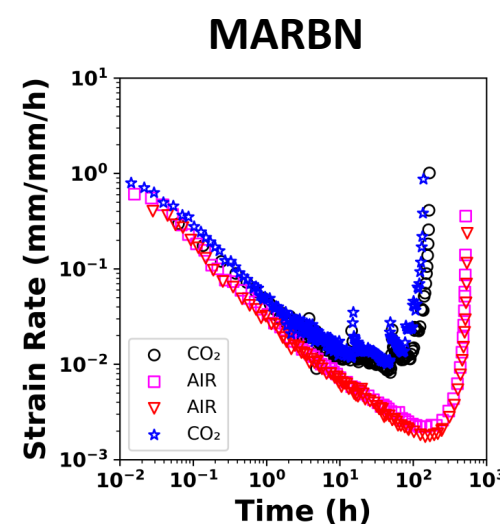
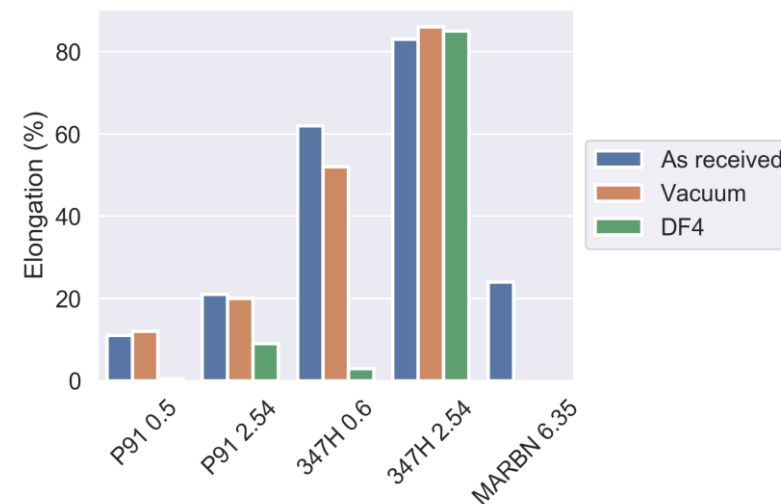




# Conclusions

## 9%Wt Cr steels

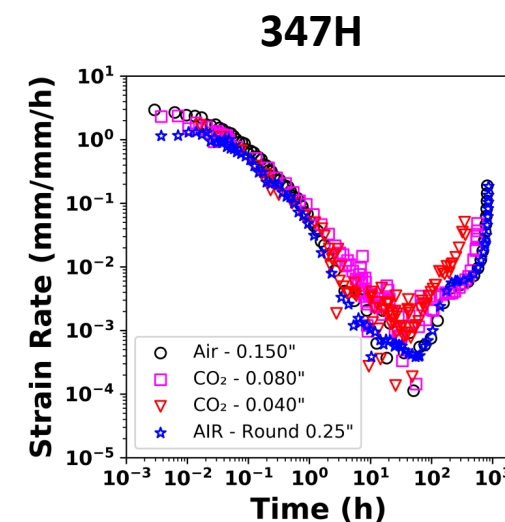
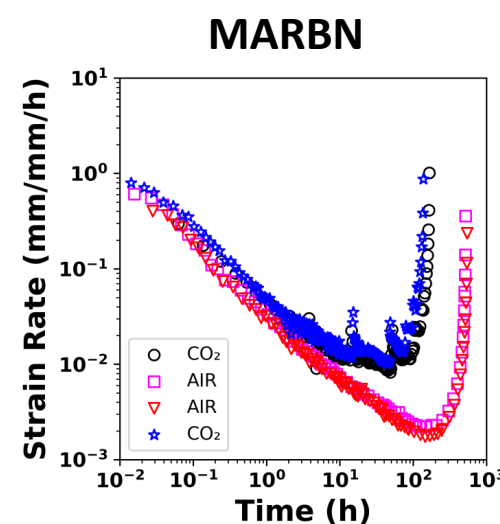
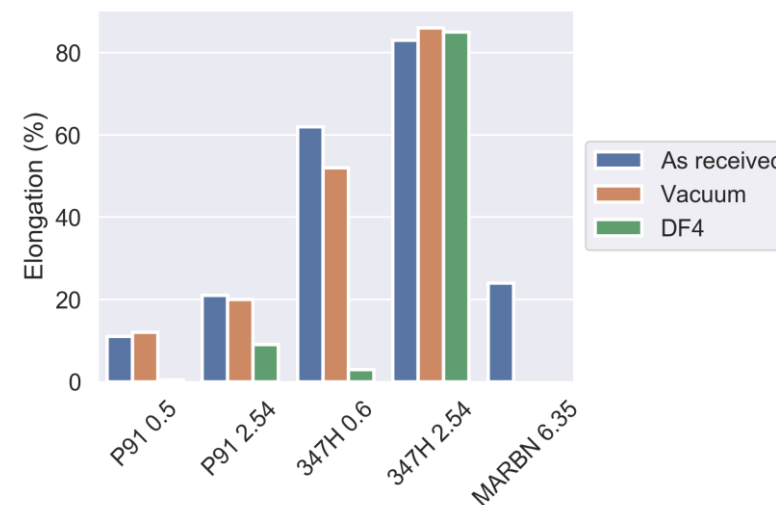
- Carburization strongly effects mechanical properties
- Strategies to mitigate carburization are necessary if used in sCO<sub>2</sub> applications
- Thin sections subject to severe degradation
- Creep lifetimes reduced ~3.5X



# Conclusions

## Austenitic steels – 17%Wt Cr

- Generally better resistance to environmental effects in sCO<sub>2</sub>
- Thin sections showed brittle behavior (reduction in ductility and increase in yield stress)
- Creep experiments are on going
- Preliminary results show reduction in lifetimes but no change in MCR
- Suggests they may be resistant to environmentally assisted cracking



# Thank You

Questions?



## ACKNOWLEDGEMENTS

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# RESOURCES

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