



# Polymer compatibility in super-critical CO<sub>2</sub> environments – behaviors in low temperature and pressure exposures



Presentation to the  
7<sup>th</sup> International Super-critical Carbondioxide Power Cycles Symposium  
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PRESENTED BY

Nalini Menon<sup>1</sup>, April Nissen<sup>1</sup>, Robert Horton<sup>1</sup> Fitzjames Ryan<sup>1</sup>, Mark Anderson<sup>2</sup> Mohamed Elbakhshwan<sup>2</sup>, Nathan Colgan<sup>2</sup>

<sup>1</sup> = Sandia National Laboratories

<sup>2</sup> = University of Wisconsin

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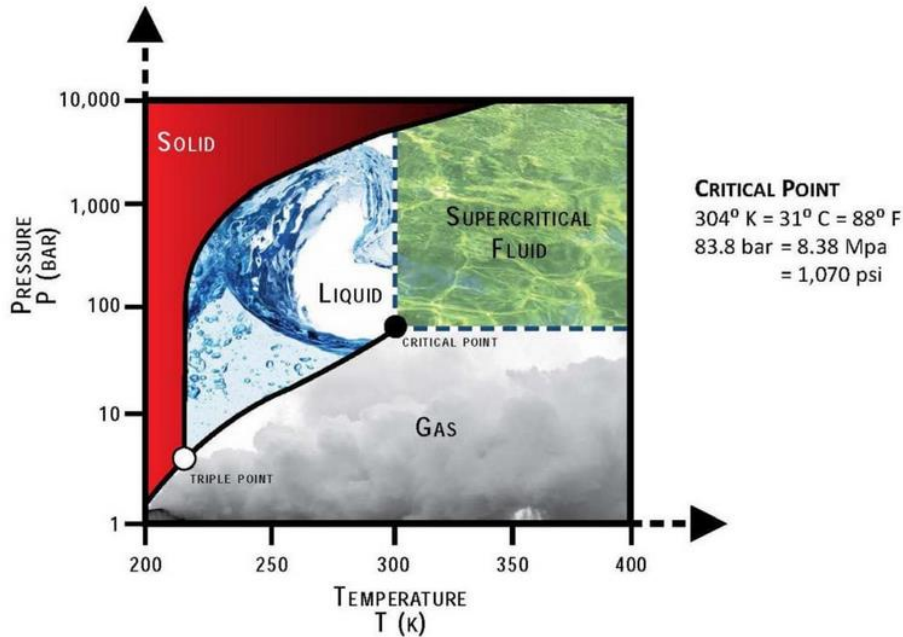
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## Content

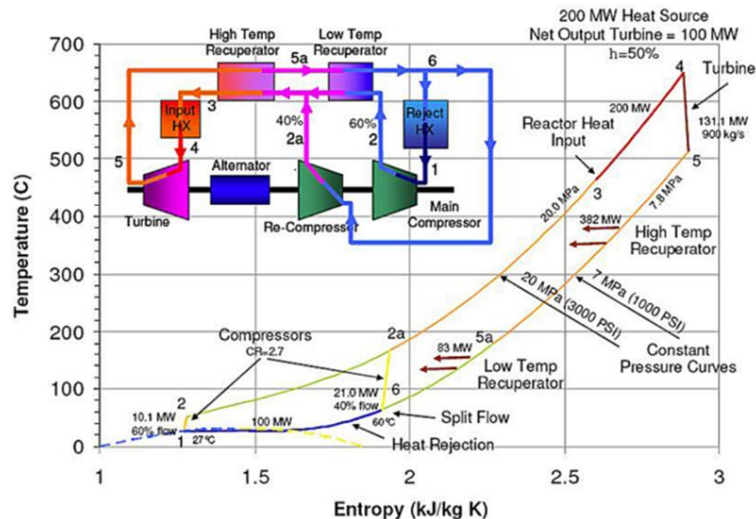
- Why sCO<sub>2</sub> for power generation systems?
- Polymers in sCO<sub>2</sub> power generation
  - Typical service conditions and challenges
  - Current knowledge gaps
- Compatibility of polymers in sCO<sub>2</sub> environments
  - Current work
- Important takeaways from current work
- Future needs

# Supercritical CO<sub>2</sub> for power generation



- Easily achievable low supercritical pressures and temperatures
- Ideal working fluid – nonexplosive, non-flammable, non-toxic and relatively cheap
- High density and volumetric capacity compared to steam
- Smaller components, smaller plant footprint and lower capital costs
- Applicable to many thermal energy sources: fossil fuel combustion, nuclear, solar, geothermal, waste heat recovery
- **Carbon capture and utilization opportunity**

## Supercritical CO<sub>2</sub> Brayton Cycle

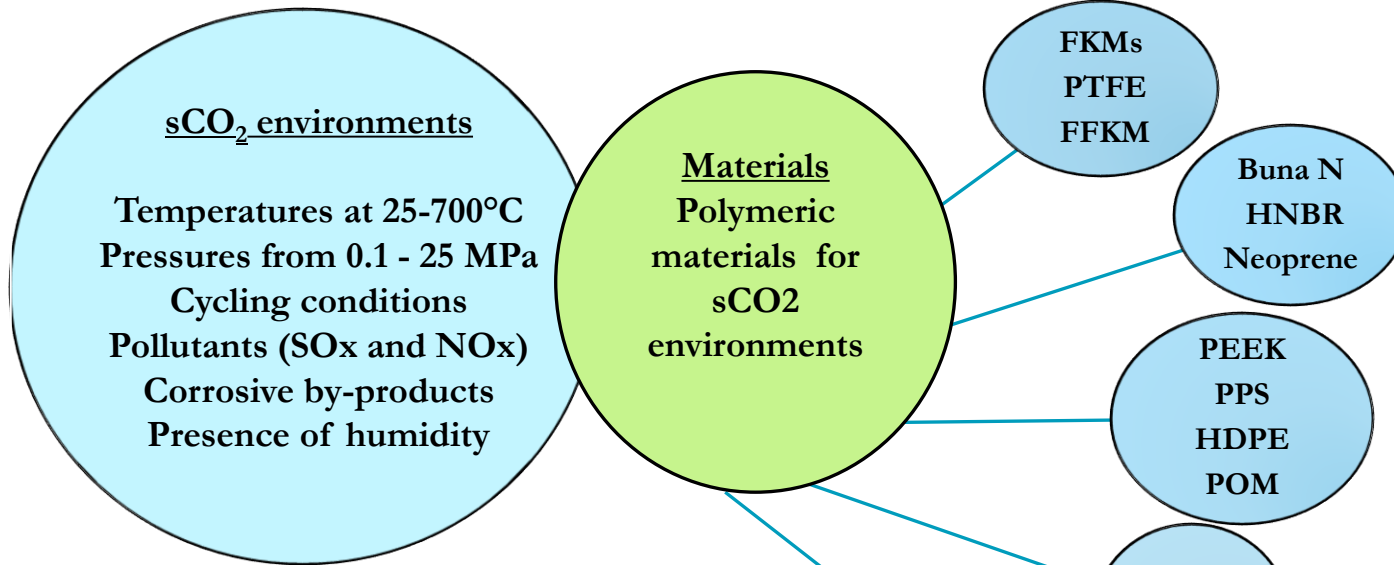


STEP's focus : better materials, designs, components, operation and control systems for commercial acceptance of large scale sCO<sub>2</sub> power cycles

Highly recuperated closed loop Brayton test assembly, Sandia NM

# 4 Polymer compatibility in sCO<sub>2</sub> energy conversion systems

## Environments + materials = Compatibility



**For turbines:**

Inlet total pressure - 21 MPa (3045 psi)  
 Inlet total temperature - 753 K (480°C)  
 Mass flow rate - 1270.5 kg/s  
 Outlet static pressure - 7.35 MPa (1065 psi)

Gas type	Permeation coefficient (Q)	Diffusion coefficient (D)	Solubility coefficient (S)	S/D
N <sub>2</sub>	1	1	1	1
CO <sub>2</sub>	24	1	24	24
CH <sub>4</sub>	3.4	0.7	4.9	7
He	15	60	0.25	0.004
O <sub>2</sub>	3.8	1.7	2.2	1.29

Approximation of permeation, diffusion and solubility coefficients of various gases through common elastomers

High solubility and easy permeation through polymer



Pressure transducers



Pressure relief valves



Valve seats

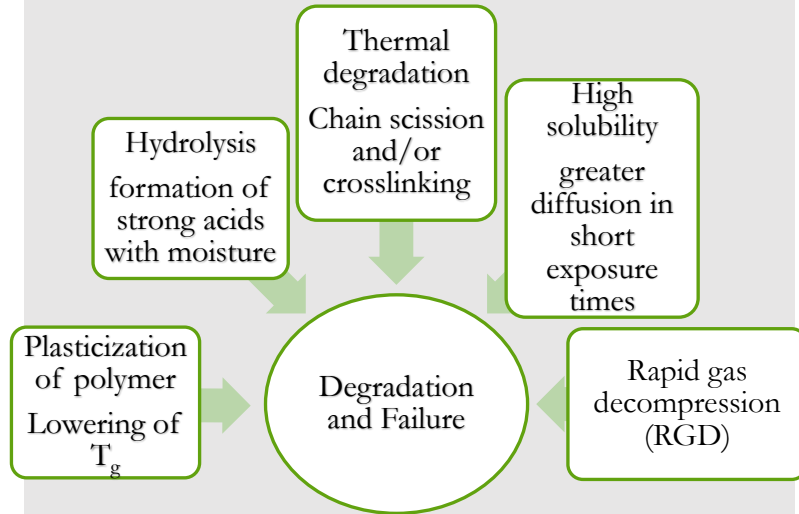


Turbo machinery seals

# Polymer compatibility in sCO<sub>2</sub> – Mechanisms of failure



## Mechanisms of polymer degradation

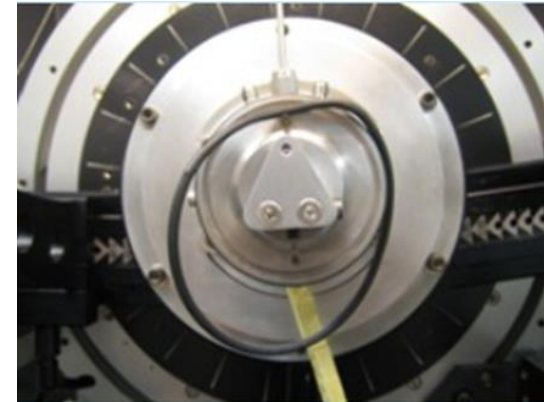


Increased by high pressure (> 10 MPa)  
 Higher CO<sub>2</sub> concentration in gas mixture  
 Higher solubility of CO<sub>2</sub> in elastomer  
 High decompression rate >0.1 MPa/min  
 Elastomer microstructure  
 O-rings with low degree of design-imposed constraint

## Amorphous or semi-crystalline polymer

Degree of crystallinity, substitution on backbone, molecular weight, crosslink density, glass transition temperature T<sub>g</sub>, chain alignment/ packing

Examples of failures in elastomers in sCO<sub>2</sub> service due to explosive decompression



Failure seen with Viton O-ring due to sCO<sub>2</sub> exposure



## 6 Polymer compatibility in sCO<sub>2</sub> – Knowledge gaps

- Data for lower temperature (55-60°C) and pressure (100-1800 psig) exists; R&D required for temperature range (60-150°C) and pressures (4000-6000 psig)
- In-situ monitoring of polymer degradation and failure modes
  - polymer failure initiation and growth during the process instead of a post-mortem approach
  - physical and mechanical property degradation studies supported by chemical characterization
- Test methods and standards development
- Cycling experiments with changes in temperature and sCO<sub>2</sub> pressures
- Solubility and permeation of sCO<sub>2</sub> in polymers and influence of fillers and plasticizers on this phenomenon
- Factors controlling rapid gas decompression – depressurization rates
- Effect of impurities such as H<sub>2</sub>S and chemical aging of polymers
- Research and development for new material resistant to sCO<sub>2</sub> attack

## Polymer compatibility in sCO<sub>2</sub> – Sandia experiments FY2019-21



### Sandia's sCO<sub>2</sub> experimental work focused on establishing

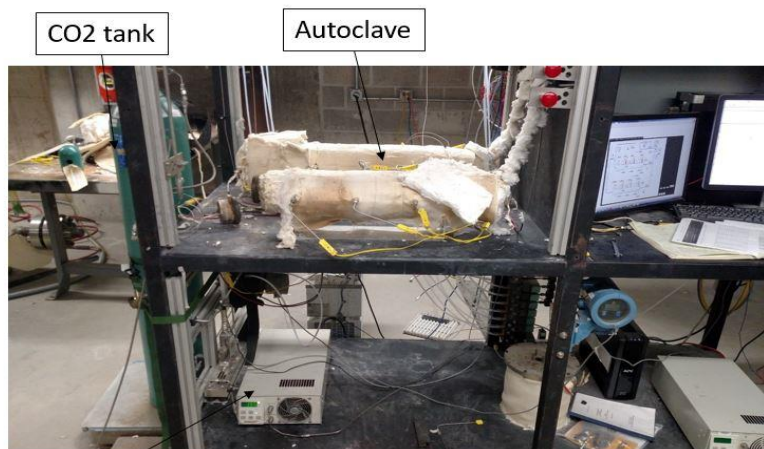
- baseline thermal behaviors of typical polymers at 100°C and 150°C temperatures at 20 MPa sCO<sub>2</sub> pressure in a 1000-hour exposure
- baseline behaviors of typical polymers at 10 and 40 MPa sCO<sub>2</sub> pressures at 100°C temperature in a 1000-hour exposure
- behavior of select polymers in the compressed state mimicking O-rings in sealing applications in sCO<sub>2</sub> in a 1000-hour exposure; some O-rings with a barrier coat were tested for mitigation of sCO<sub>2</sub>
- investigating the effect of thermal cycling (50°-150°-50°C) under steady 20 MPa sCO<sub>2</sub> pressure for 50 and 100 cycles

- Addresses some of the critical knowledge gaps mentioned
- All experiments were possible due to collaboration with University of Wisconsin-Madison
- Sandia's sCO<sub>2</sub> test capability in place by end of FY 2021

# 8 Polymer compatibility in sCO<sub>2</sub> – Sandia experiments FY2019-21



## sCO<sub>2</sub> test equipment and accessories



CO2 tank

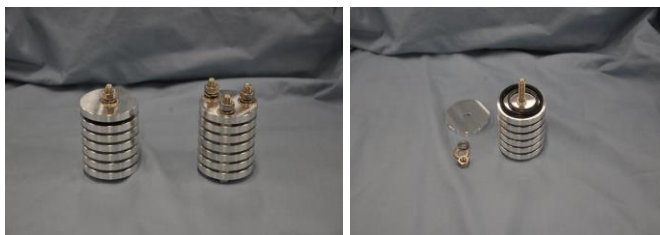
Autoclave

sCO<sub>2</sub> Pump

O-ring sample holder for autoclave



O-ring compression jig used in sCO<sub>2</sub> exposure; 25% deflection shim used



## Ex-situ characterization for sCO<sub>2</sub> effects\*

**Elastomers**  
(FKM, Buna N, HNBR, Neoprene, FF-202, EPDM, EPR)

DMTA for T<sub>g</sub> and Modulus

Specific volume/density changes

Compression Set

ATR-FTIR spectroscopy

**Thermoplastics**  
(HDPE, PTFE, Nylon, PEEK, POM)

DMTA for T<sub>g</sub> and Modulus

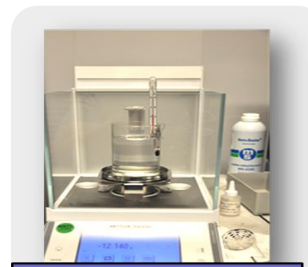
Specific volume/density changes

Tensile Testing

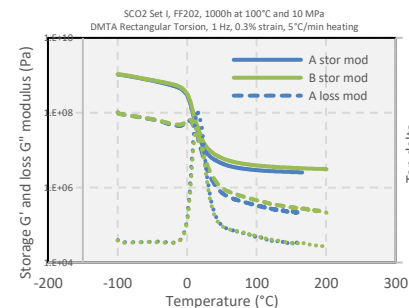
ATR-FTIR spectroscopy



Compression set test



Density measurements set-up



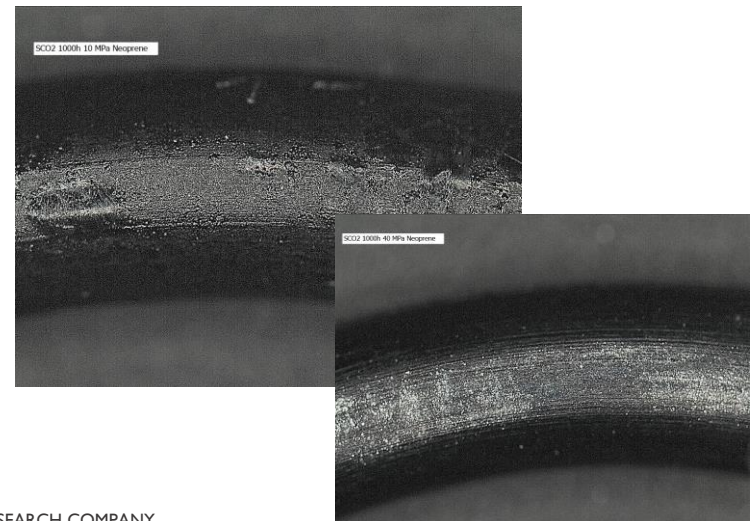
Samples were introduced as whole O-rings to test  
Periodic removal of O-rings at 200 hours, 600 hours and at 1000 hours followed by cutting them to characterization test specimen dimensions



## Results and Discussion – Major takeaways

Based on experiments on 13 polymers including both elastomers and thermoplastics and under conditions of testing shared, the following are high level findings:

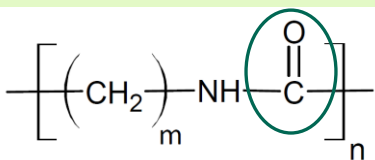
- Thermoplastics showed minimal damage from sCO<sub>2</sub> exposures compared to elastomers
- Elastomer showed internal cracks, surface texturization, structural changes, compression set changes
- Increasing temperatures accelerate damage mechanisms for almost all elastomers
- Increasing pressures in combination with long times of exposure accelerated damage in even robust polymers
- Increasing number of temperature cycles showed varying levels of damage in polymers
- Physical effects seen in the form of cracks inside the polymer and surface texturization
- Chemical effects seen in the form of changes in glass transition temperatures, storage modulus and structural changes in FTIR



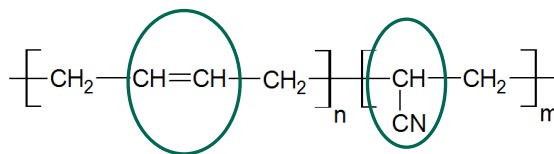


# Results and Discussion – Major takeaways

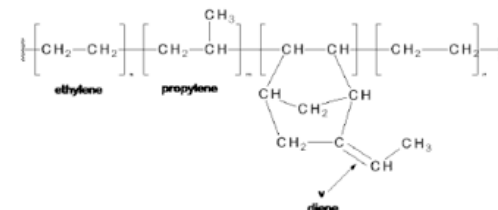
- Polymer backbone and microstructural details showed a great influence on behavior in sCO<sub>2</sub> environments
  - Presence of polar functionality -C=O, -C-Cl, -C-CN or -C=C- (double bonds) on backbone in polymers tested increase propensity for sCO<sub>2</sub> effects – for e.g. higher storage modulus with/without increase in T<sub>g</sub>
  - Large pendant-group atoms (such as fluorine) can provide steric hinderance and decrease sCO<sub>2</sub> diffusion – for e.g. FF-202, FKM and PTFE
  - EPDM and EPR show property changes but less propensity to accelerated sCO<sub>2</sub> attack
  - Hard to separate influential factors in a given polymer type due to lack of information on the COTS materials used
    - influence of molecular weight, degree of crystallinity, crosslink density, fillers and additives, choice of polymer base with custom polymers (supplier-to-supplier differences)



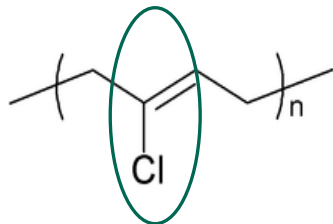
Polyamide  
(Nylon)



Nitrile butadiene rubber (NBR)

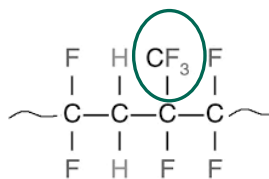


Ethylene propylene diene Monomer  
(EPDM)

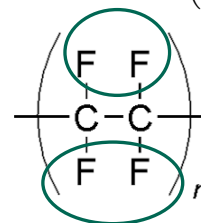


Polychloroprene  
(Neoprene)

FKM

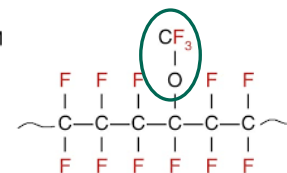


Fluoroelastomers (FKMs)



Polytetrafluoroethylene (PTFE)

FFKM



Perfluoroelastomers  
(FFKMs)



## High level findings- Isothermal isobaric exposures of Elastomers

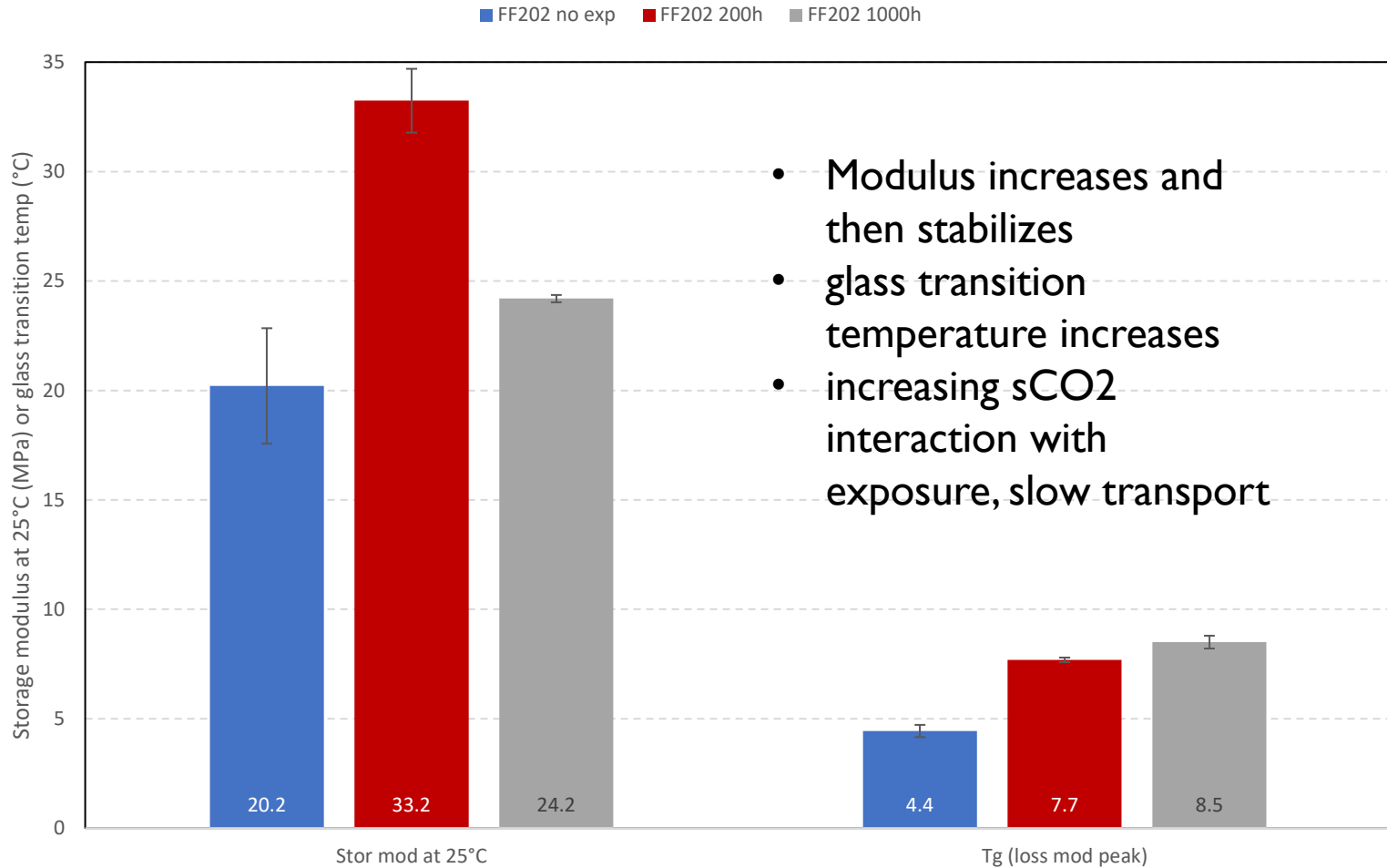
**FFKM, FKM, EPDM, EPR, Buna N,  
HNBR, Neoprene, PUR**

# Dynamic Mechanical Thermal Analysis (DMTA) on FFKM FF202

## 150°C exposure @ 20 MPa sCO<sub>2</sub> pressure



FF202 2-161 O-ring, effect of sCO<sub>2</sub> exposure at 150°C  
DMTA Rectangular Torsion, 0.2% strain, 1 Hz, 5°C/min

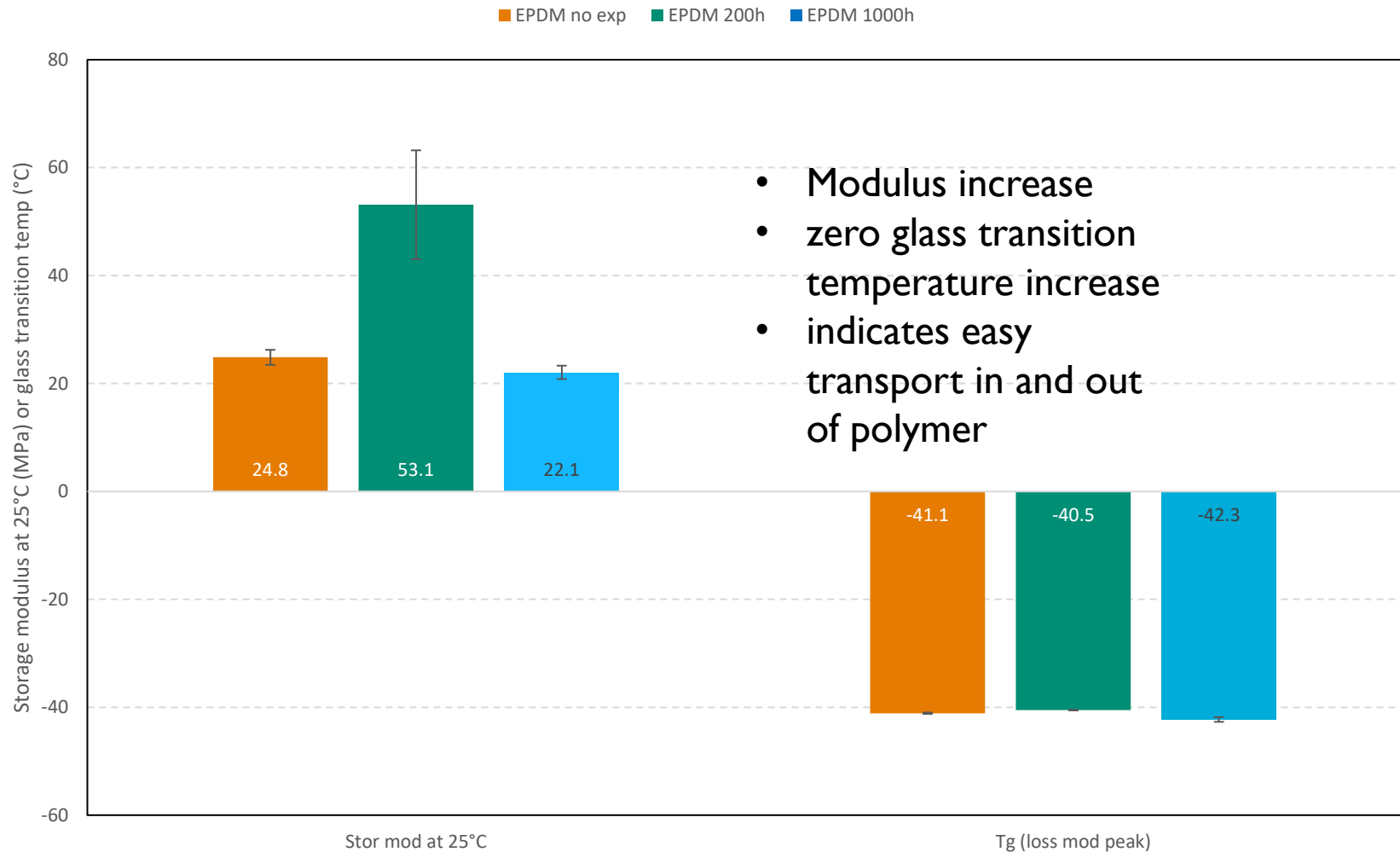


# Dynamic Mechanical Thermal Analysis (DMTA) on EPDM rubber

## 150°C exposure @ 20 MPa sCO<sub>2</sub> pressure



EPDM 2-161 backup ring, effect of sCO<sub>2</sub> exposure at 150°C  
DMTA Rectangular Torsion, 0.3% strain, 1 Hz, 5°C/min

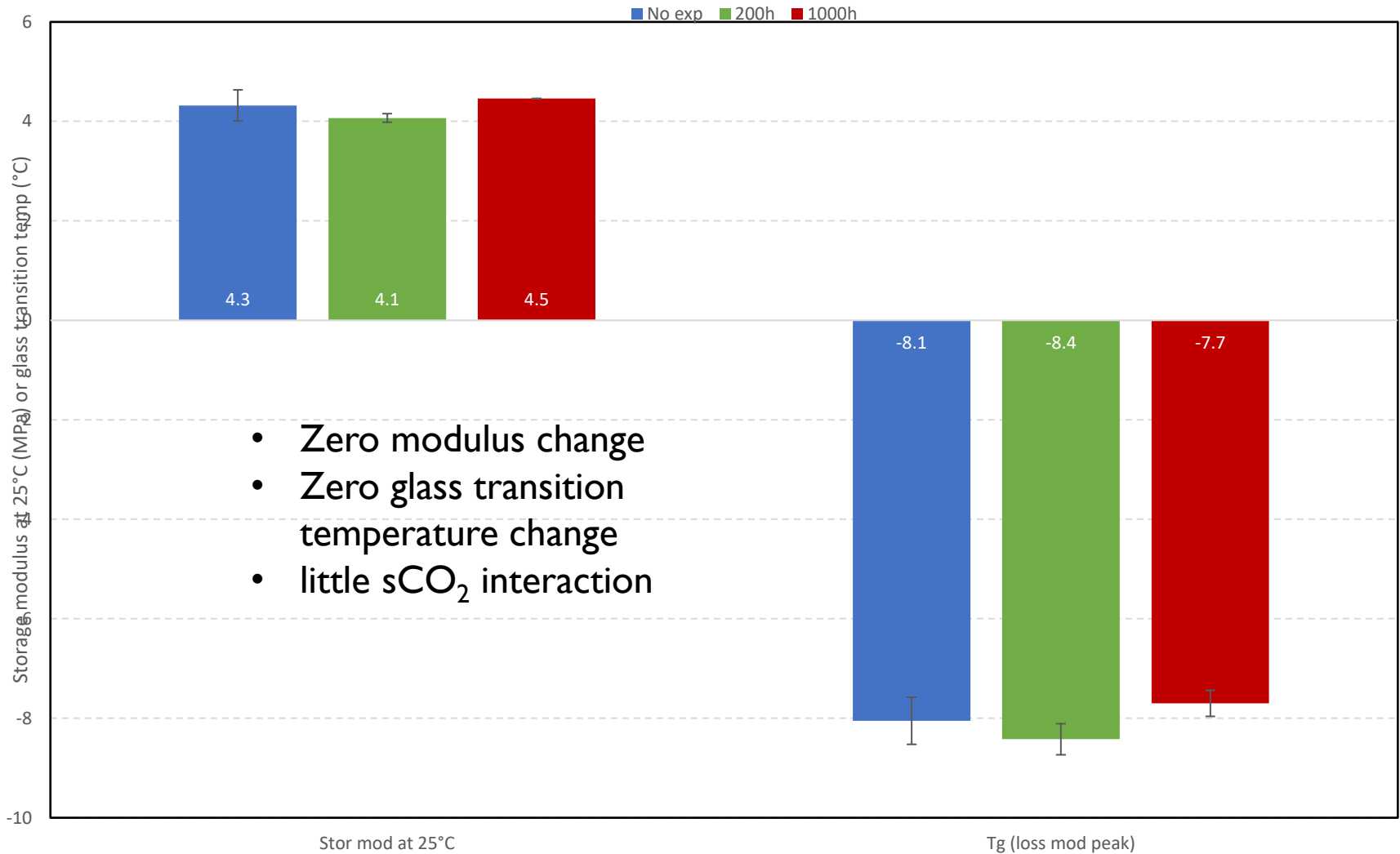


# Dynamic Mechanical Thermal Analysis (DMTA) on FKM Viton

100°C exposure @ 20 MPa sCO<sub>2</sub> pressure



Viton, effect of sCO<sub>2</sub> exposure at 100°C  
DMTA Rectangular Torsion, 0.3% strain, 1 Hz, 5°C/min

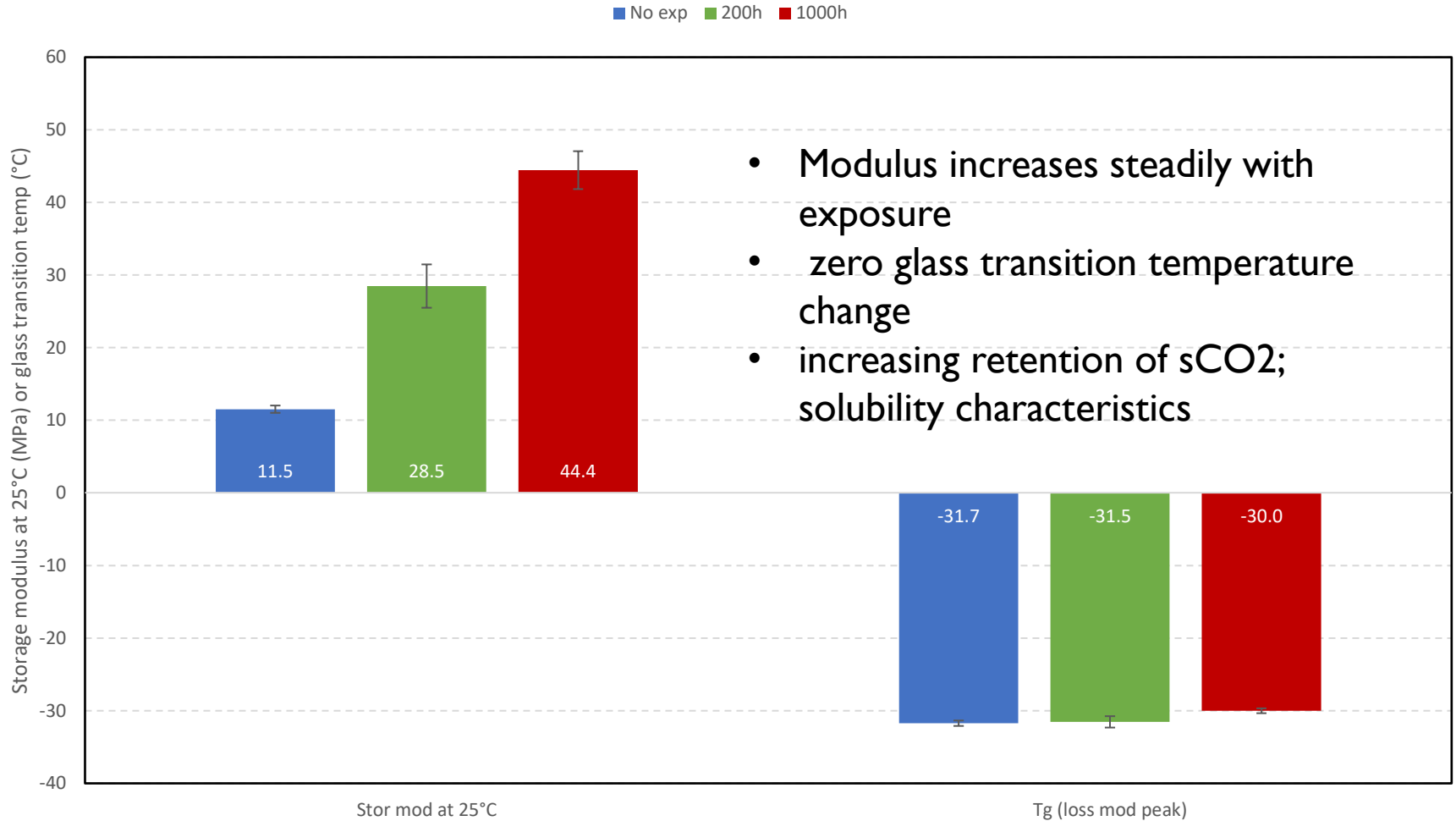


# Dynamic Mechanical Thermal Analysis (DMTA) on Neoprene

100°C exposure @ 20 MPa sCO<sub>2</sub> pressure



Neoprene, effect of sCO<sub>2</sub> exposure at 100°C  
DMTA Rectangular Torsion, 0.1% strain, 1 Hz, 5°C/min

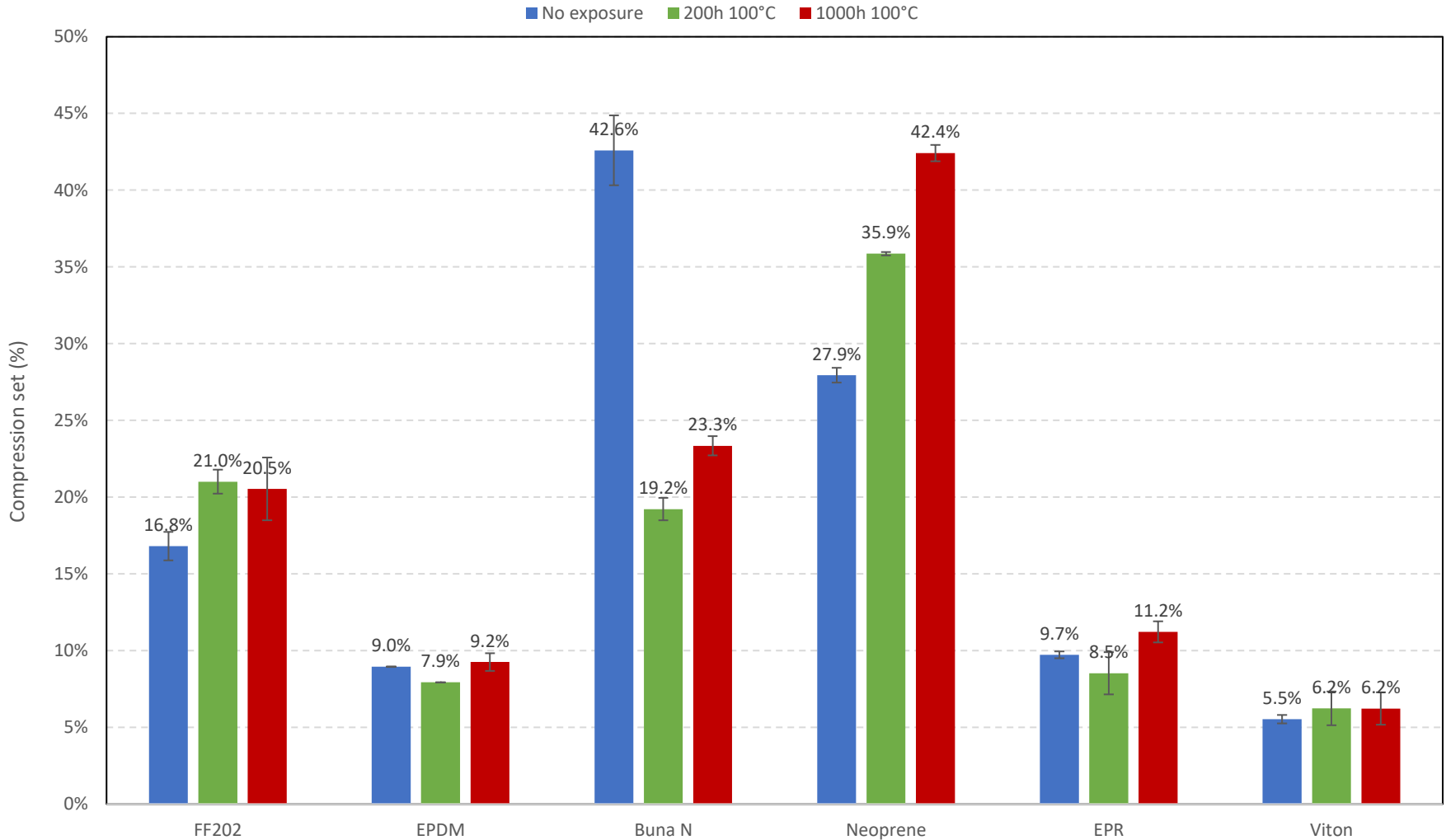


# Compression set (ASTM D395 method B) on different elastomers

## 100°C exposure @ 20 MPa sCO<sub>2</sub>

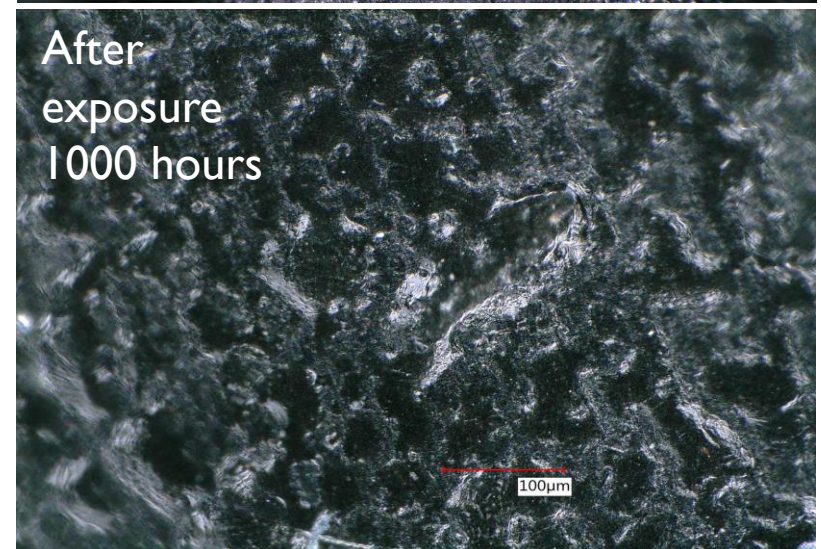
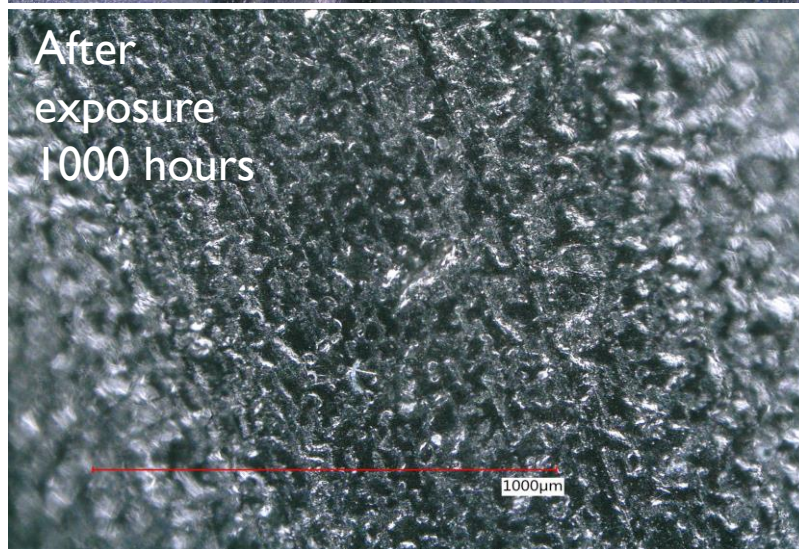
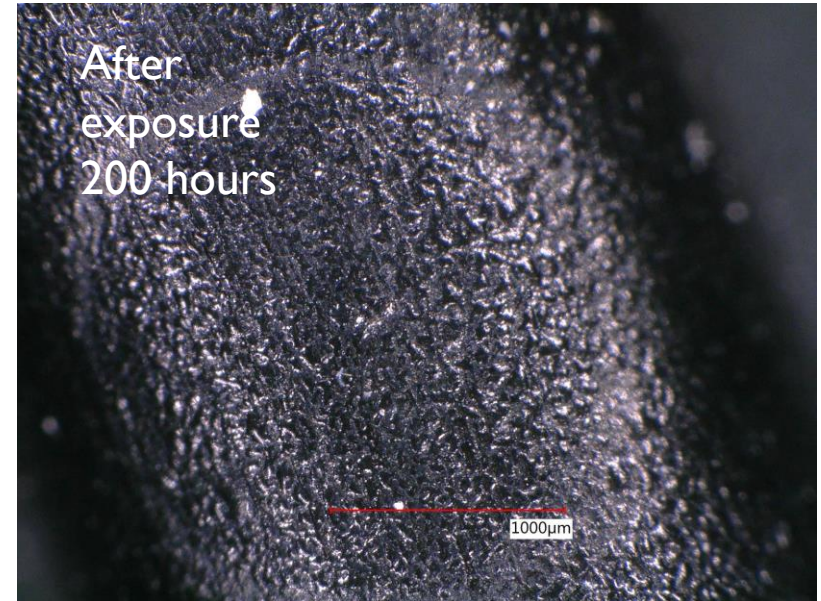
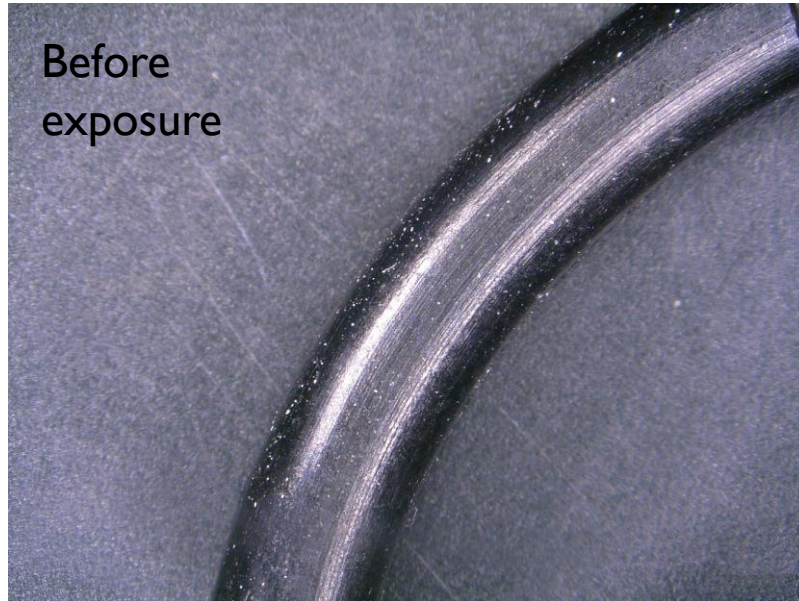


Compression set in materials after exposure to SCO<sub>2</sub> at 100°C  
Compressed to 75% of original height, 22h at 110°C, 30 min recovery, average of 2 specimens





Optical microscopy images on Neoprene  
100°C exposure @ 20 MPa sCO<sub>2</sub> pressure

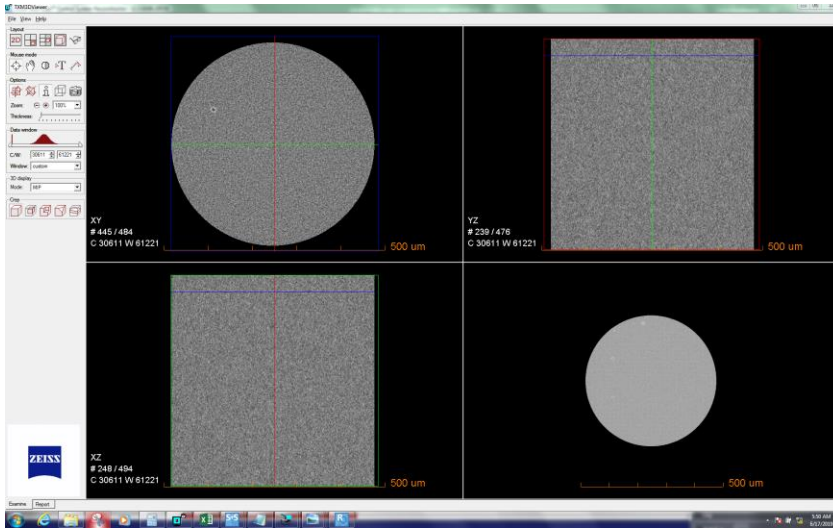


# Micro-Computed tomography images for FFKM FF202 and EPDM rubbers

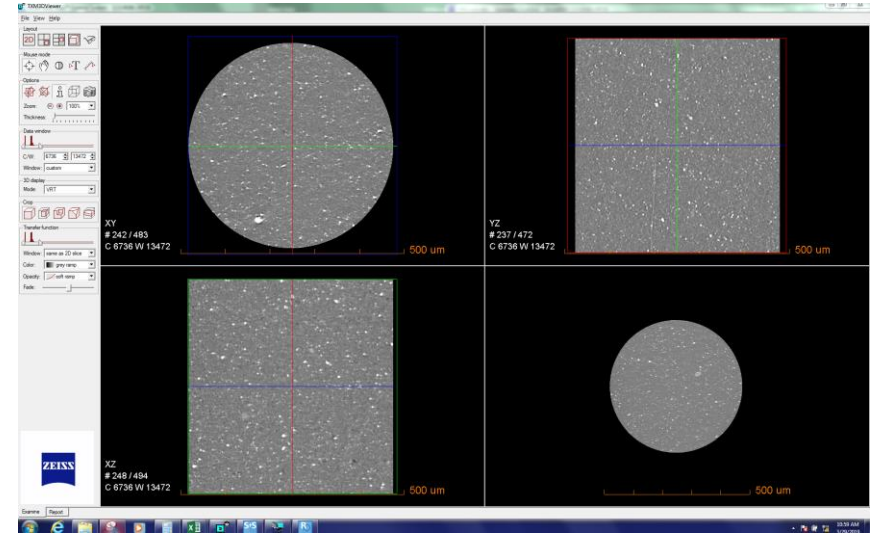
150°C exposure @ 20 MPa sCO<sub>2</sub> pressure



## Unexposed

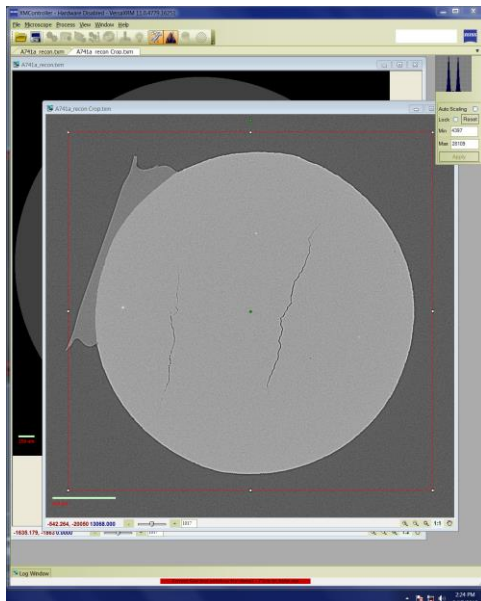


## Unexposed



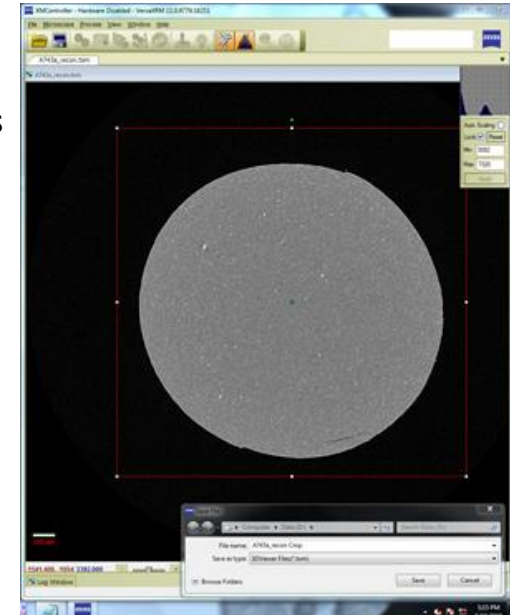
## Exposed

500-1000  
microns length  
cracks in the  
interior



## Exposed

400-475 microns  
length cracks in  
the interior



**In both polymers  
cracks appear as  
early as after 200  
hours of exposure  
at 100°C**

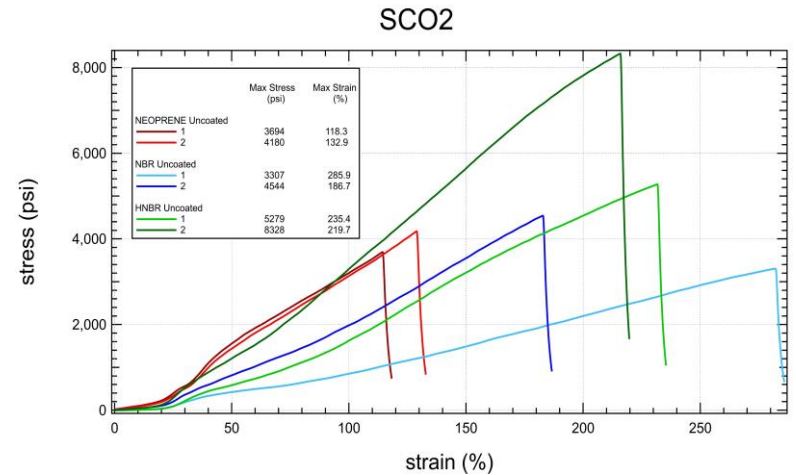
## Polymers held in compression fixture during test (25% deflection) 20 MPa sCO<sub>2</sub> pressure at 100°C



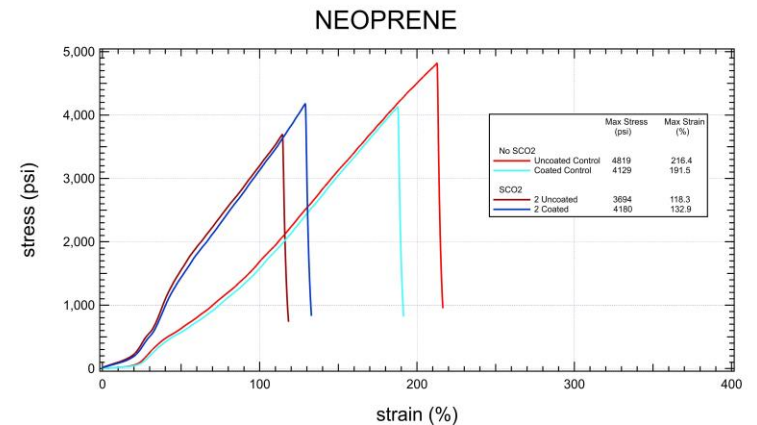
Compression fixtures designed to hold the O-rings inside the sCO<sub>2</sub> autoclave



Picture of whole O-rings after compressed exposure to 20 MPa sCO<sub>2</sub> at 100°C: from left – top row: Viton sample 1, Buna N, EPDM, HNBR; bottom row – Viton sample 2, EPR, Neoprene (uncoated) and Neoprene (coated)



Elastomer-sCO<sub>2</sub> effects impact mechanical properties



SCO<sub>2</sub>-exposed Neoprene fails at lower % strain over unexposed



## High level findings- Effect of changing pressures under isothermal conditions for Elastomers

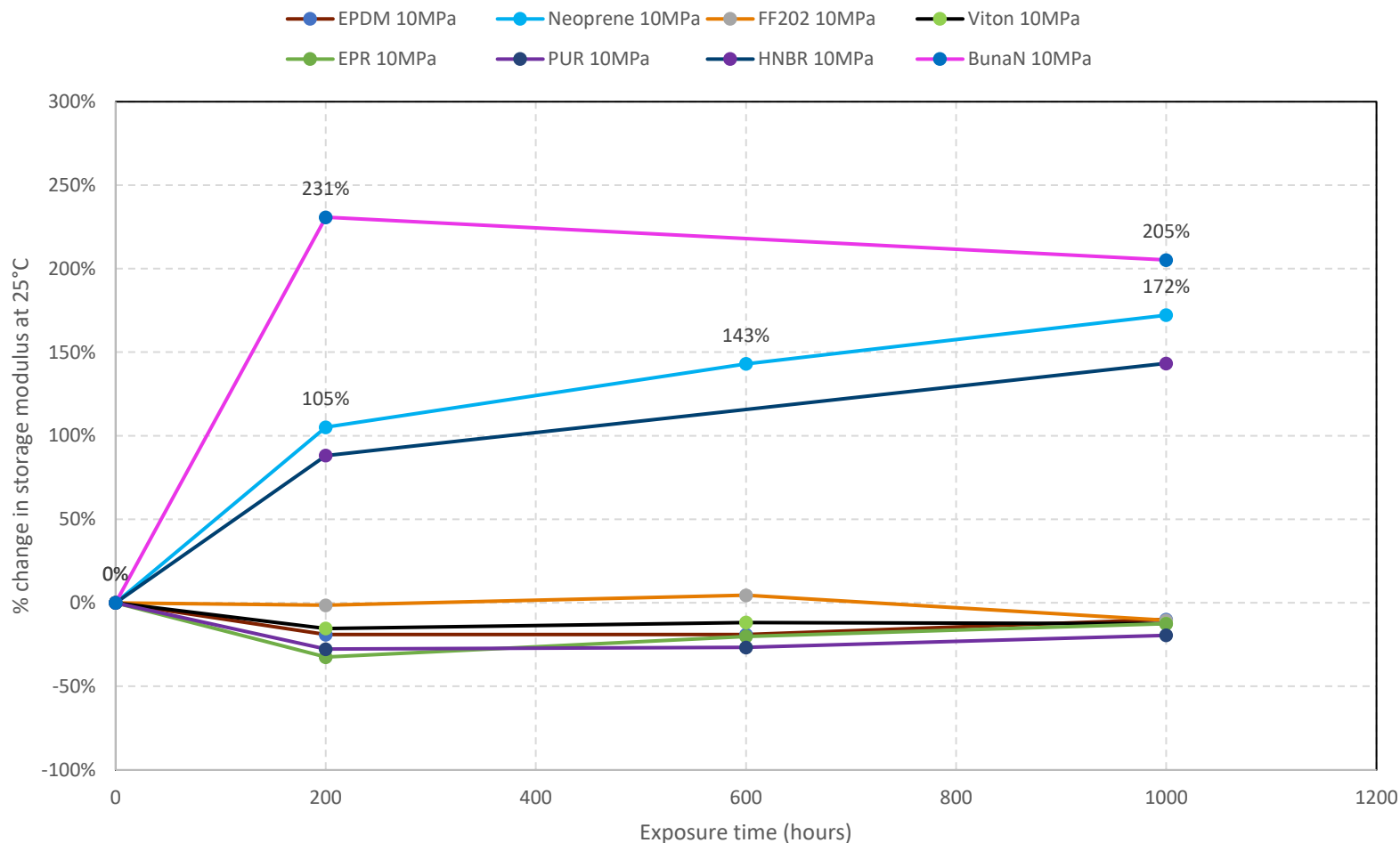
**FFKM, FKM, EPDM, EPR, Buna N,  
HNBR, Neoprene, PUR**

# Dynamic Mechanical Thermal Analysis (DMTA) on different elastomers

## Exposure to 10 MPa sCO<sub>2</sub> at 100°C temperature



Effect of SCO<sub>2</sub> exposure at 100°C, 0-1000h at 10MPa, change in storage modulus  
DMTA Rectangular Torsion, 1 Hz, 0.3% strain, 5°C/min heating

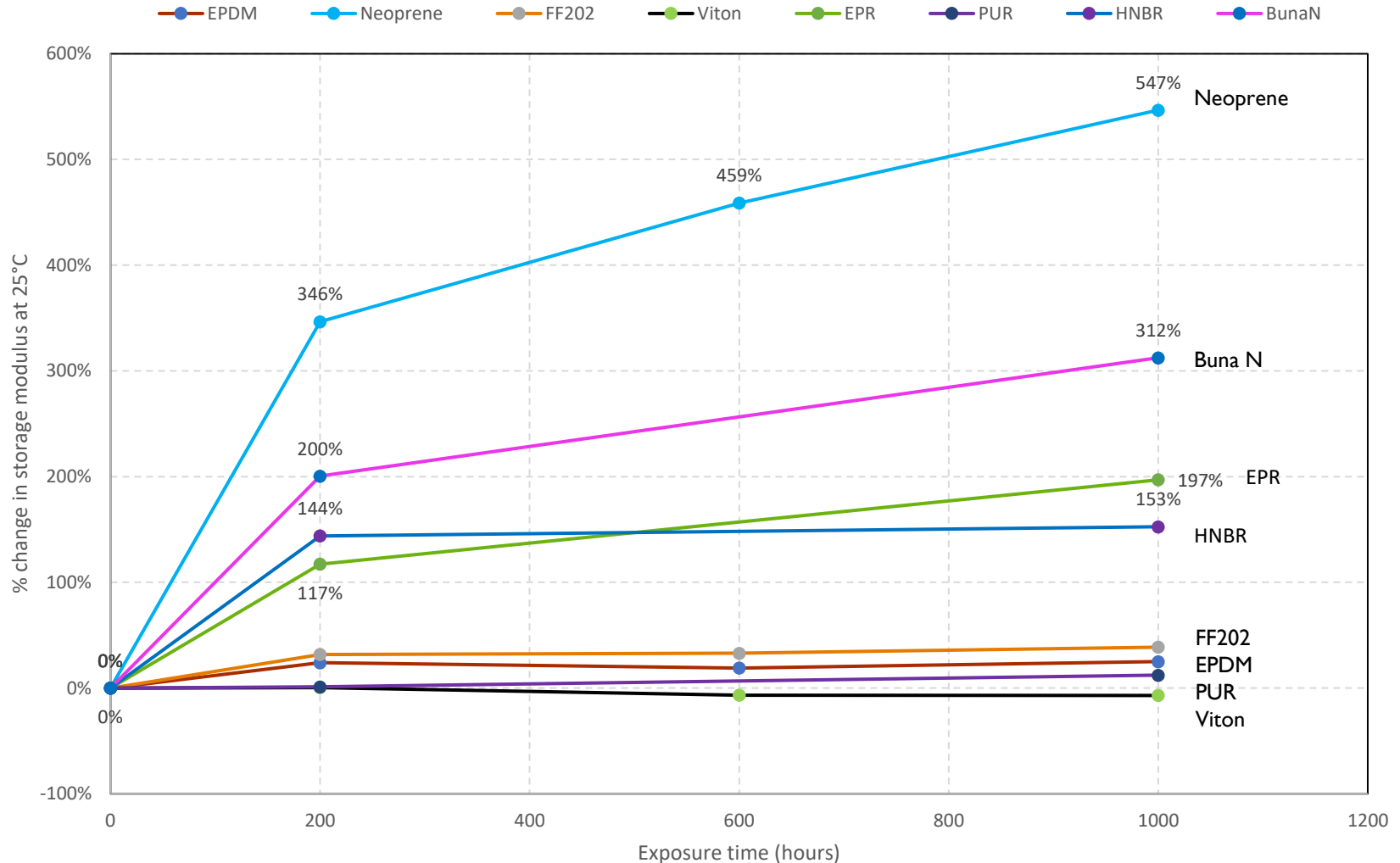


# Dynamic Mechanical Thermal Analysis (DMTA) on different elastomers

## Exposure to 40 MPa sCO<sub>2</sub> at 100°C temperature



Effect of SCO<sub>2</sub> exposure at 100°C, 0-1000h at 40MPa, change in storage modulus  
DMTA Rectangular Torsion, 1 Hz, 0.3% strain, 5°C/min heating

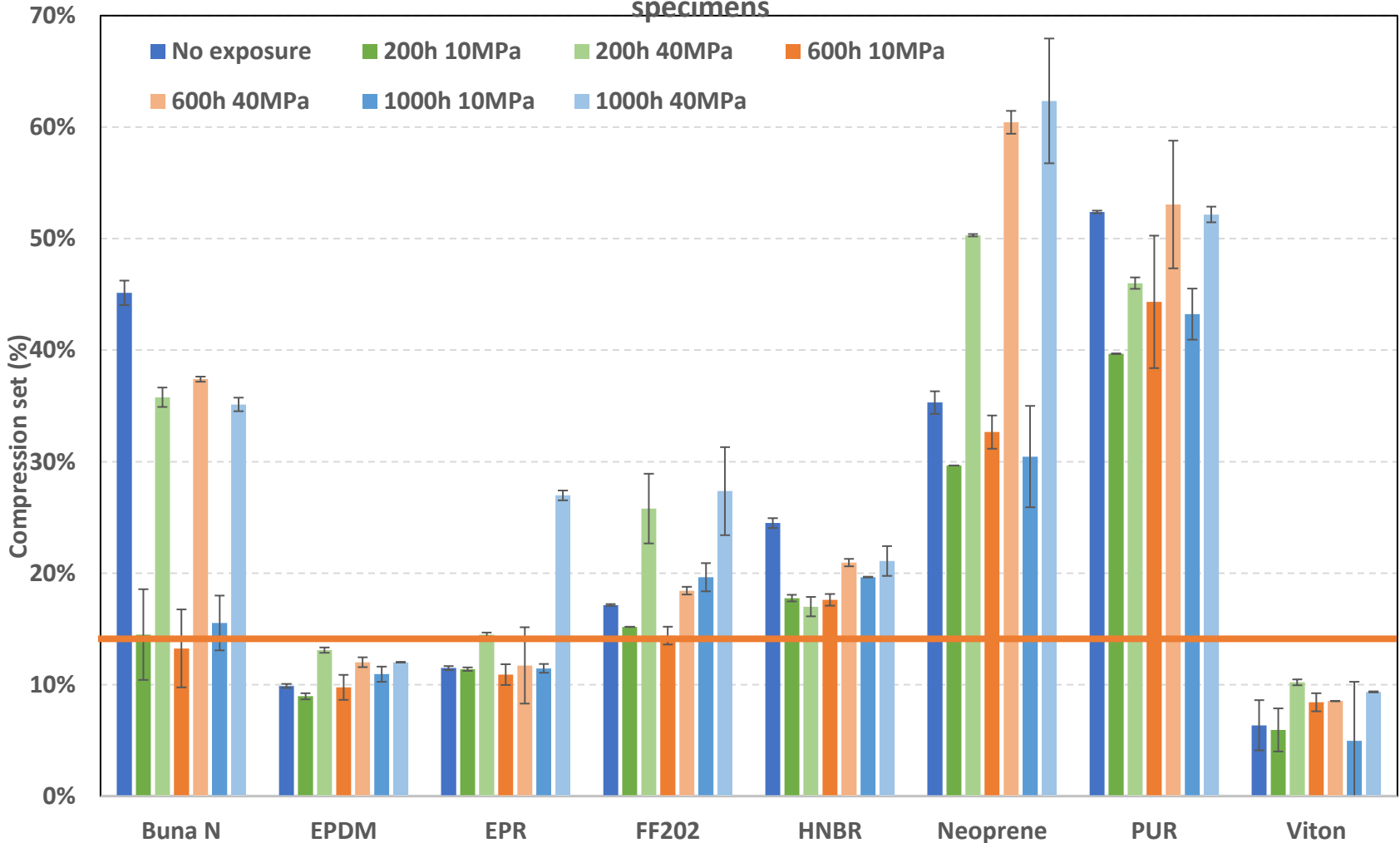


# Compression set data on different elastomers

## Exposure to 10 and 40 MPa sCO<sub>2</sub> at 100°C temperature

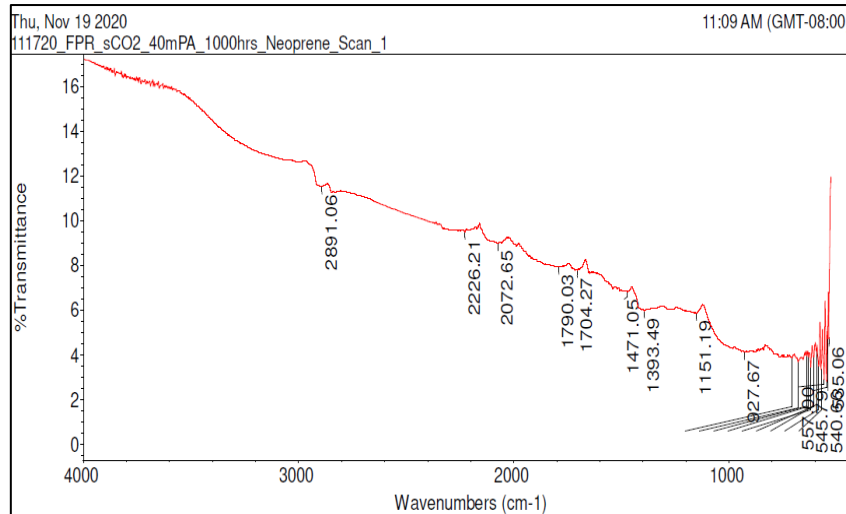
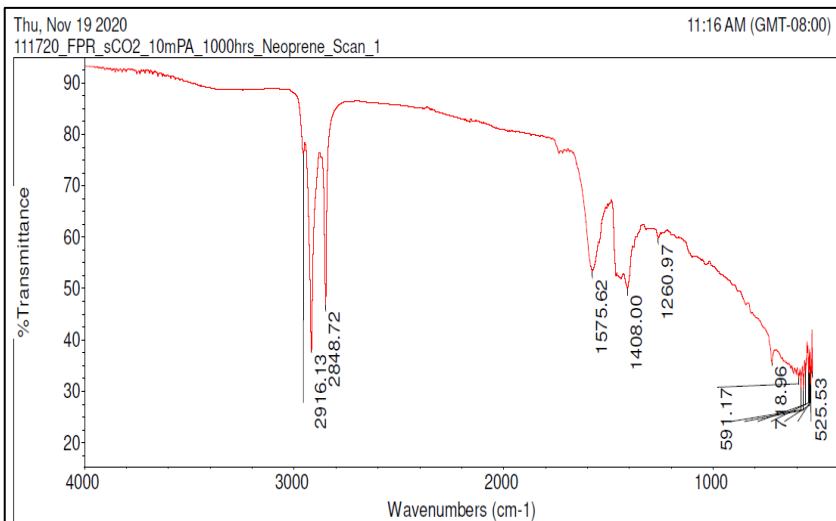
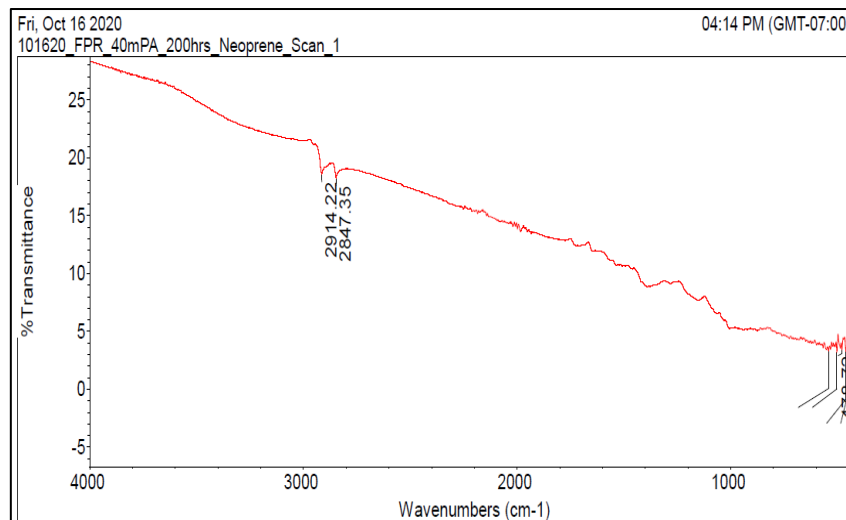
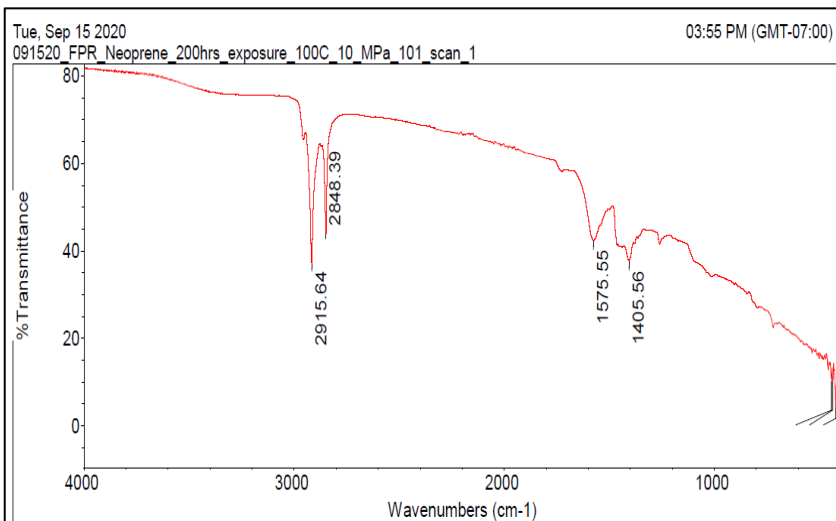


Compression set in O-rings after exposure to SCO<sub>2</sub> for 0h-600h at 100°C and 10 or 40 MPa  
 Compressed to 75% of original height, 22h at 110°C, 30 min recovery, average of 2 specimens



# Attenuated Total Reflectance FTIR on Neoprene

## Changing pressures sCO<sub>2</sub> at 100°C temperature



For longer exposure times (going from 200 hrs to 1000 hrs) at each pressure, peak intensity seems to increase for both pressures. Influence of pressure (10 MPa vs 40 MPa) is significant as can be seen with the decreased peak intensities.





## High level findings- Isobaric thermal cycling of Elastomers

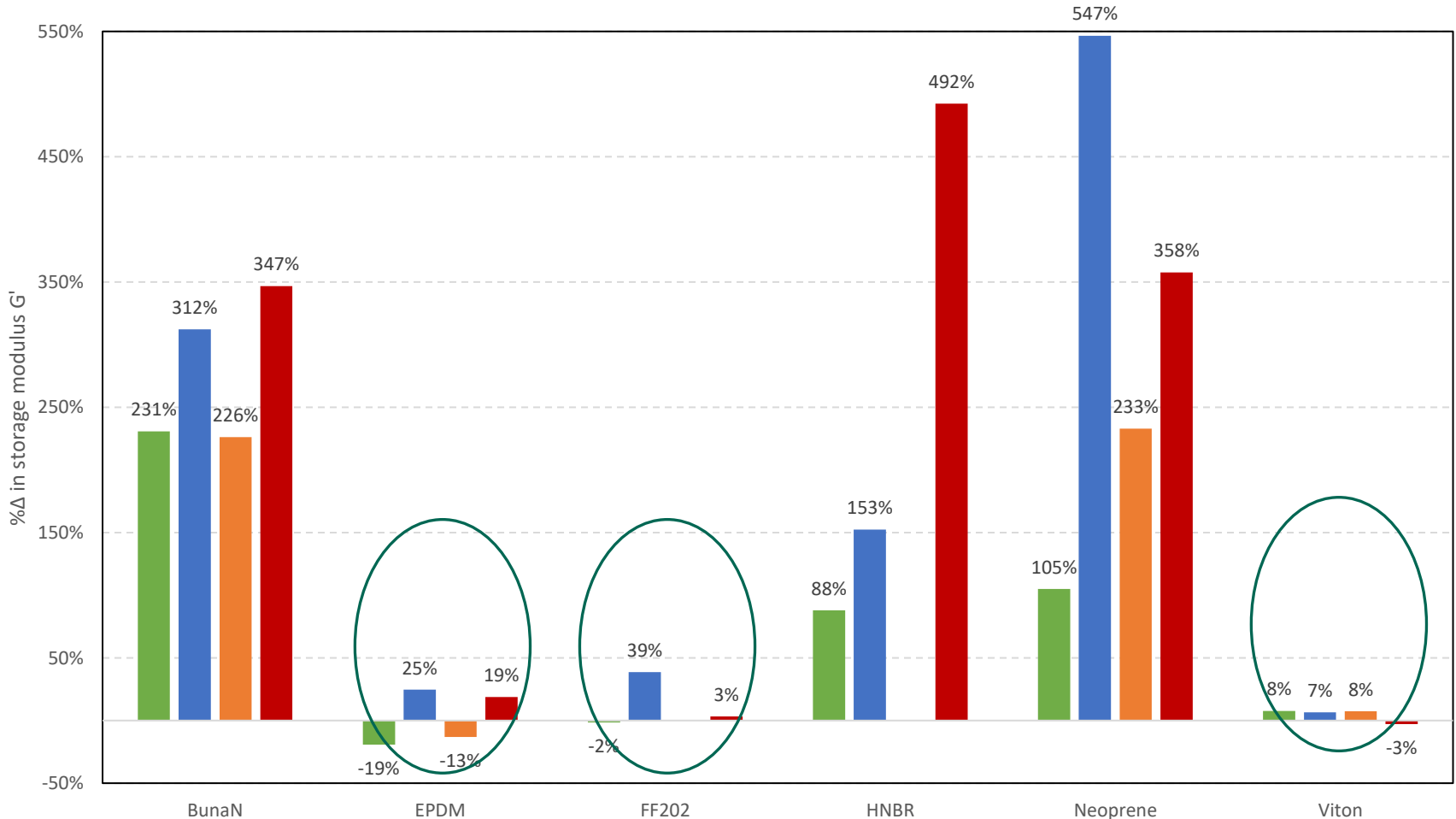
**FFKM, FKM, EPDM, EPR, Buna N,  
HNBR, Neoprene, PUR**

# Dynamic Mechanical Thermal Analysis (DMTA) on different elastomers

## Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure

O-rings after exposure to SCO<sub>2</sub> for 50/100 temperature cycles at 20 MPa,  
change in storage modulus G'  
DMTA rectangular torsion, 1 Hz, 5°C/min heating

■ 100°C 200h 10MPa   ■ 100°C 1000h 40MPa   ■ 50-150-50°C 50cyc 20MPa   ■ 50-150-50°C 100cyc 20MPa

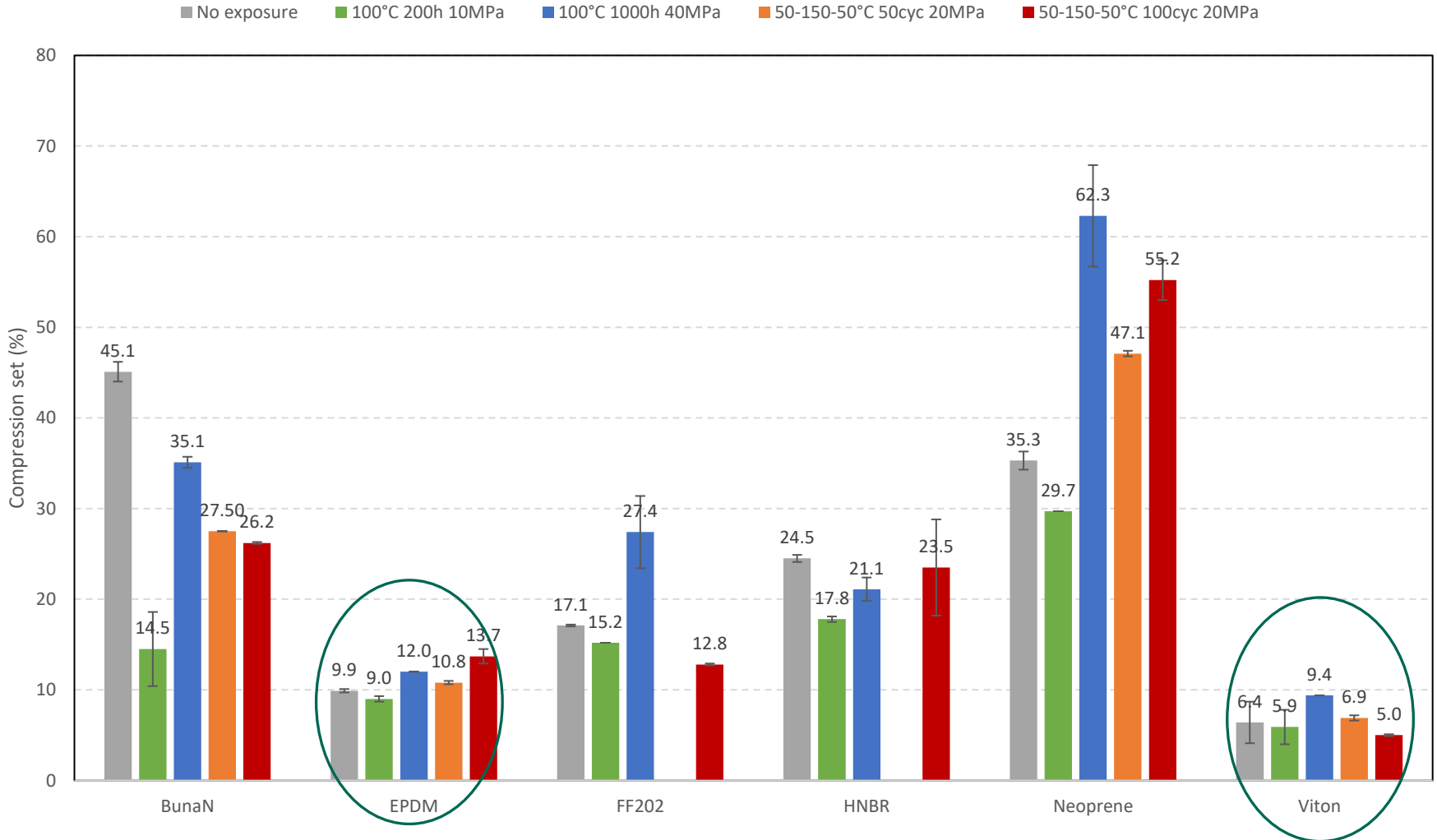


# Compression set data on different elastomers

## Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure



Compression set in O-rings after exposure to SCO<sub>2</sub> for 50/100 temperature cycles at 20 MPa  
Compressed to 75% of original height, 22h at 110°C, 30 min recovery, average of 2 specimens

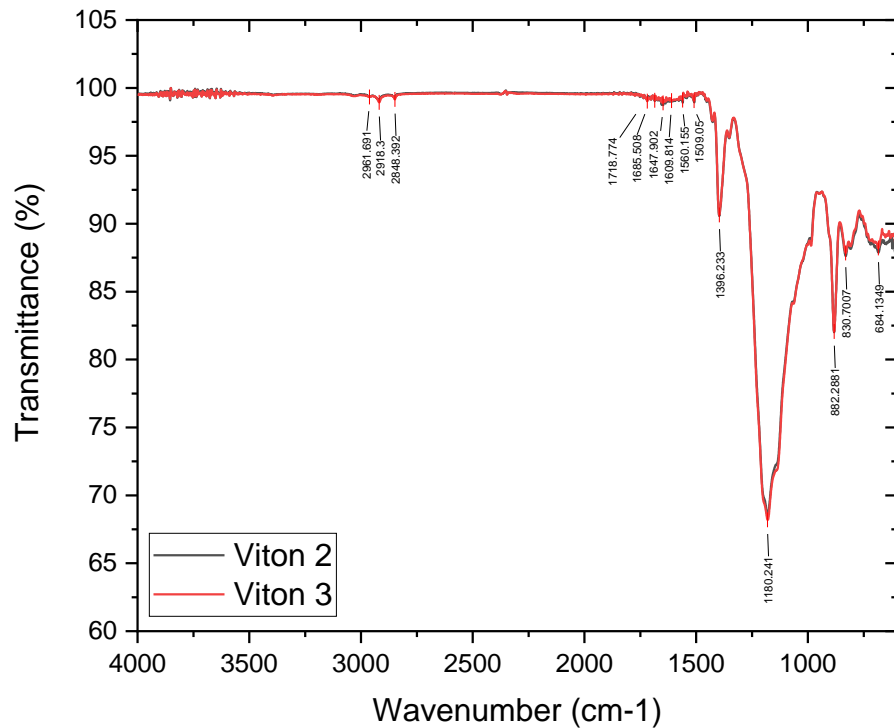


# ATR-FTIR data on different elastomers

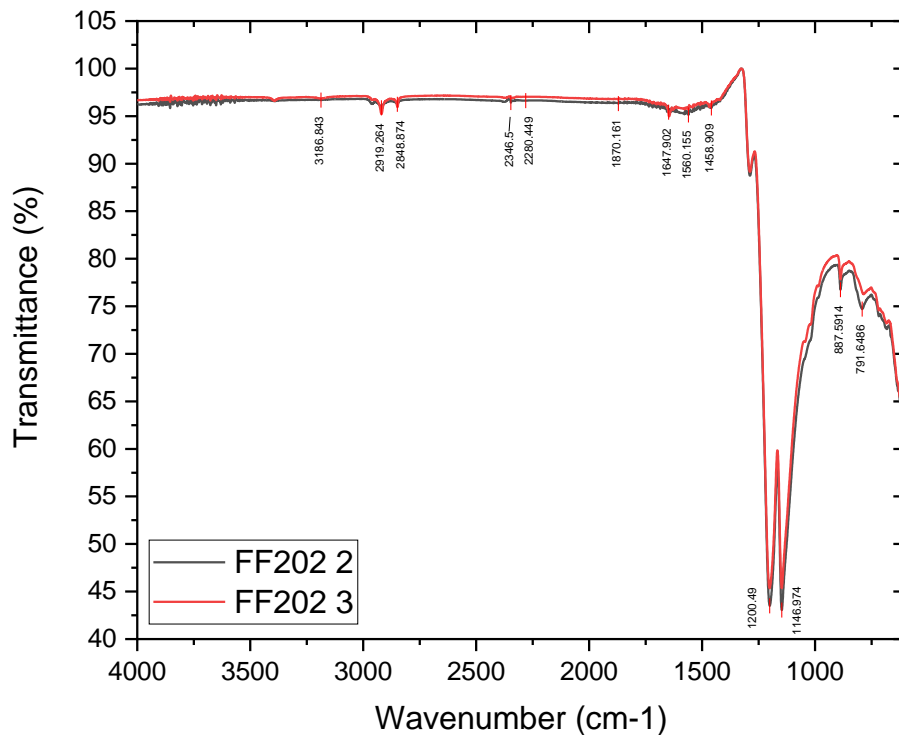
Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure



FTIR of Viton after 100 cycles of sCO<sub>2</sub>



FTIR of FF202 after 100 cycles of sCO<sub>2</sub>

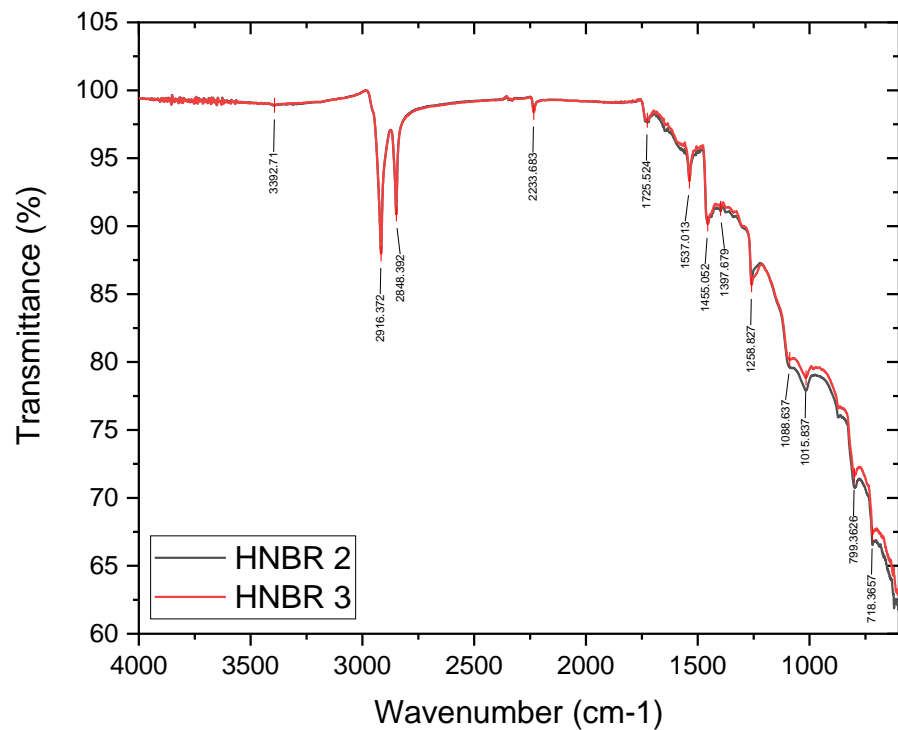


# ATR-FTIR data on different elastomers

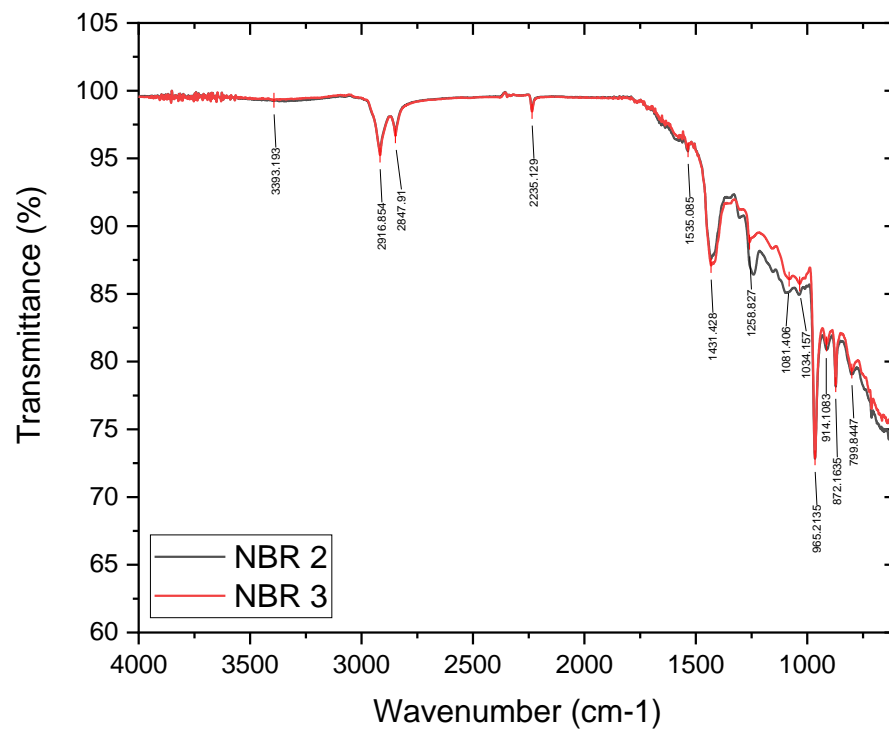
Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure



### FTIR of HNBR after 100 cycles of sCO<sub>2</sub>



### FTIR of NBR after 100 cycles of sCO<sub>2</sub>

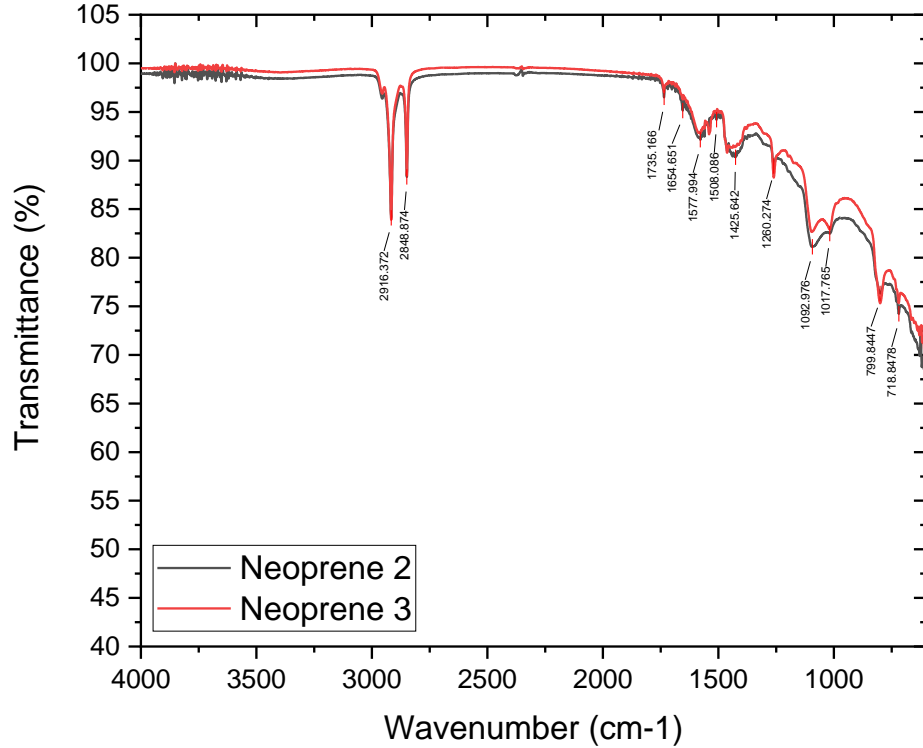


# ATR-FTIR data on different elastomers

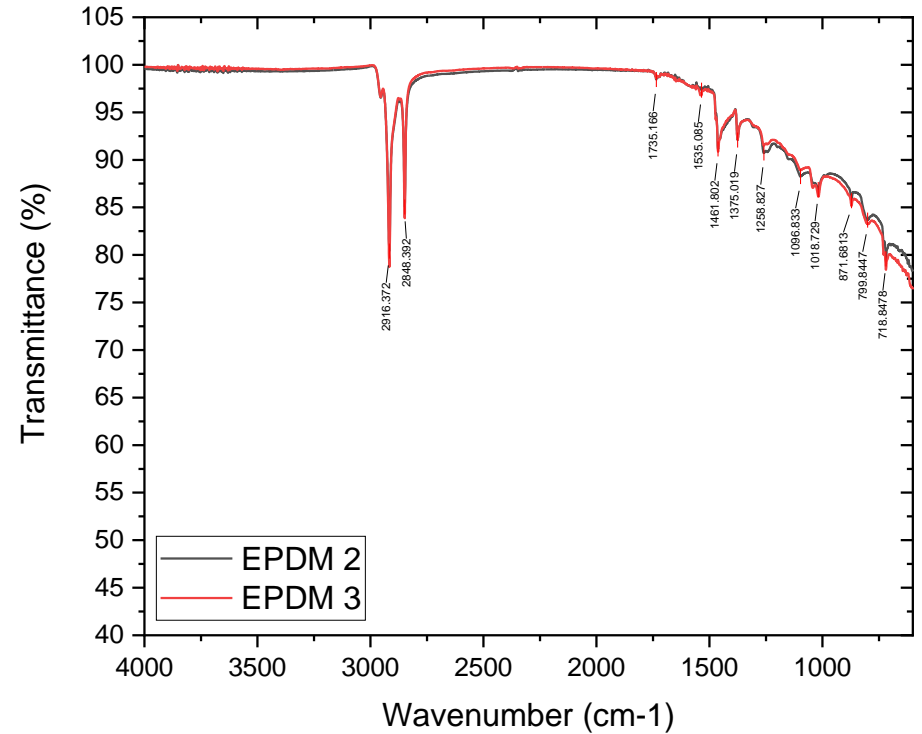
Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure



FTIR of Neoprene after 100 cycles of sCO<sub>2</sub>



FTIR of EPDM after 100 cycles of sCO<sub>2</sub>





## Overall trends observed with Thermoplastics for different sCO<sub>2</sub> exposures

**HDPE, PEEK, POM, Nylon 66, PPS,  
PTFE**

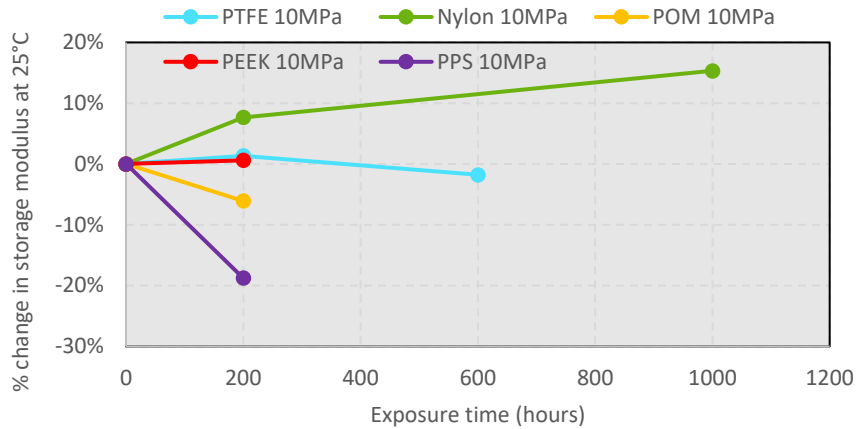


# Dynamic Mechanical Thermal Analysis (DMTA) on different thermoplastics

## Exposure to 10 MPa and 40 MPa sCO<sub>2</sub> pressures at 100°C temperature

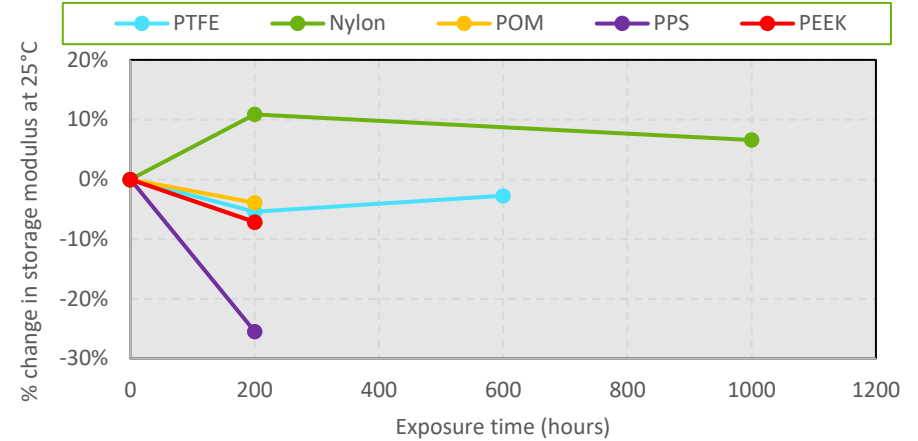
Effect of sCO<sub>2</sub> exposure at 100°C, 0-1000h at 10MPa, change in storage modulus

DMTA Rect. Torsion, 1 Hz, 0.3% strain, 5°C/min heating



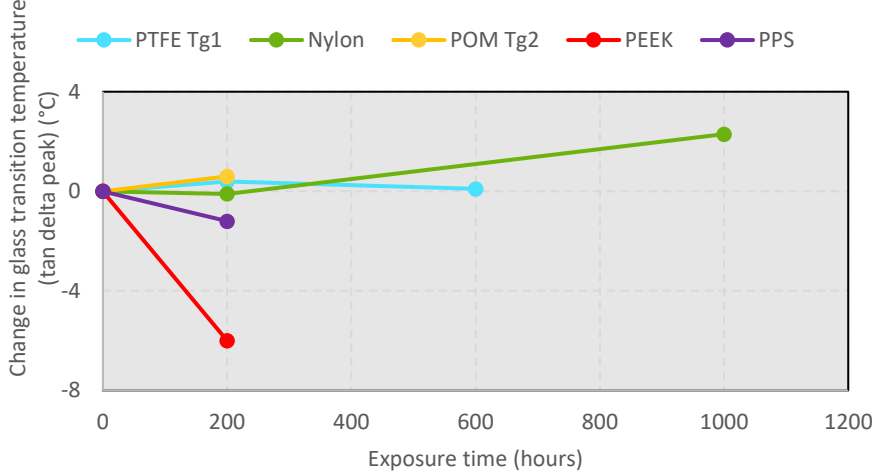
Effect of sCO<sub>2</sub> exposure at 100°C, 0-1000h at 40MPa, change in storage modulus

DMTA Rectangular Torsion, 1 Hz, 0.3% strain, 5°C/min heating



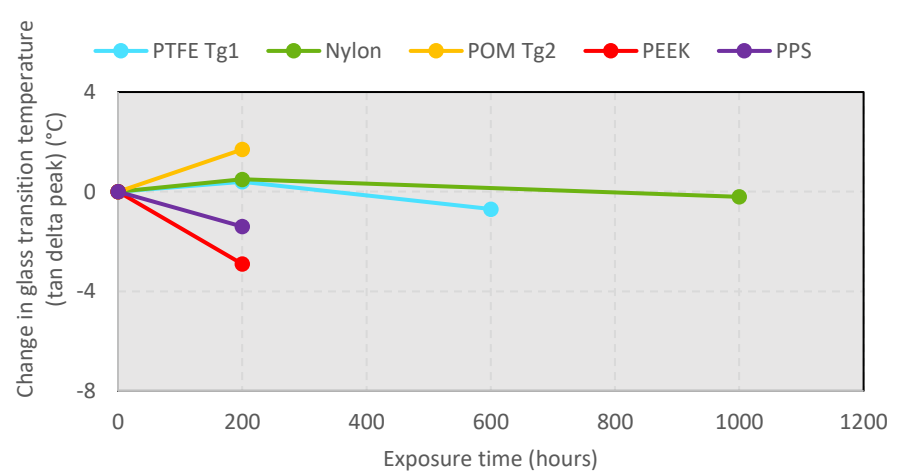
Effect of sCO<sub>2</sub> exposure at 100°C, 0-1000h at 10MPa, change in T<sub>g</sub>

DMTA Rectangular Torsion, 1 Hz, 0.3% strain, 5°C/min heating



Effect of sCO<sub>2</sub> exposure at 100°C, 0-1000h at 40MPa, change in T<sub>g</sub>

DMTA Rectangular Torsion, 1 Hz, 0.3% strain, 5°C/min heating

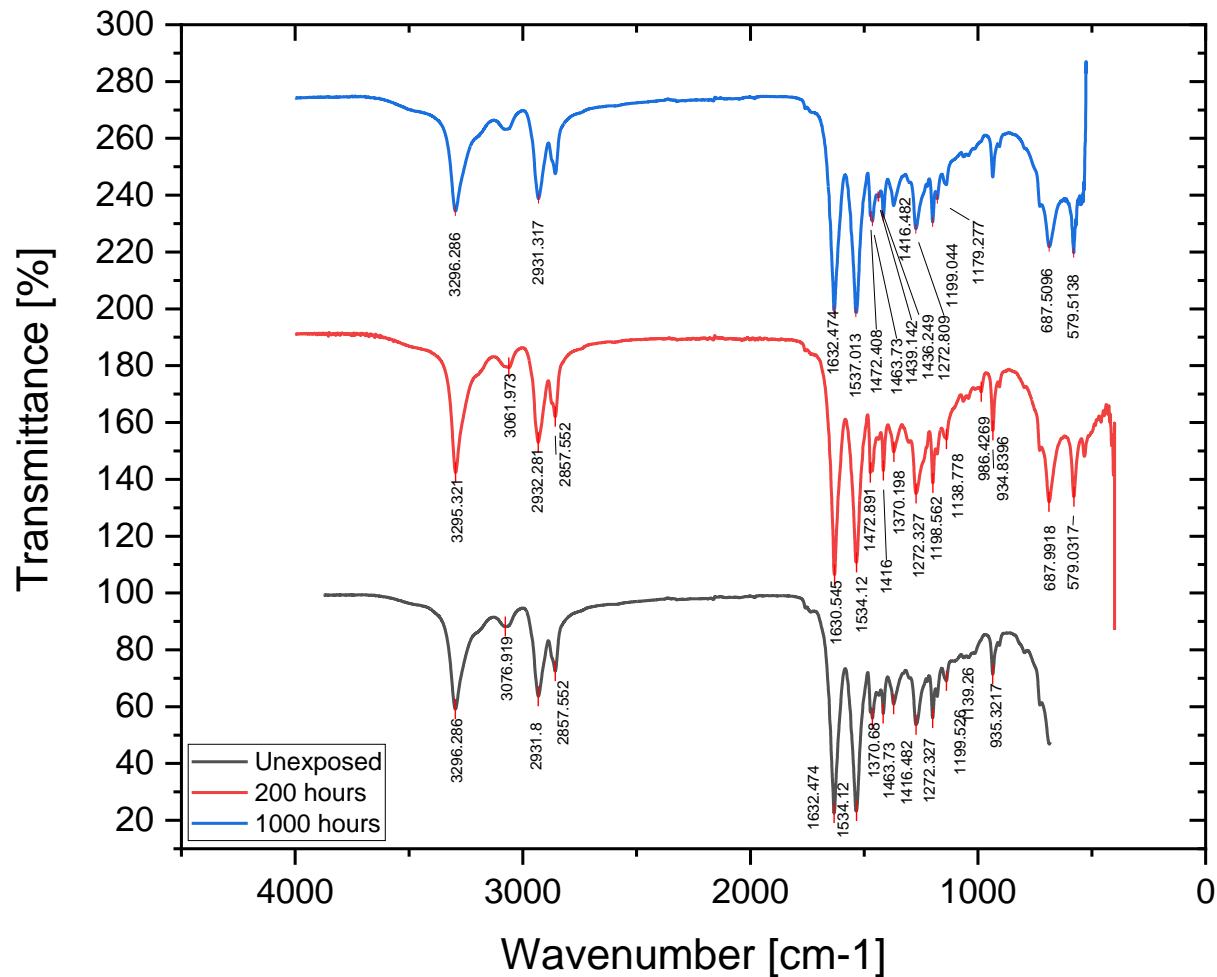






# Attenuated Total Reflectance FTIR on Nylon 6,6 10 MPa pressure sCO<sub>2</sub> at 100°C temperature

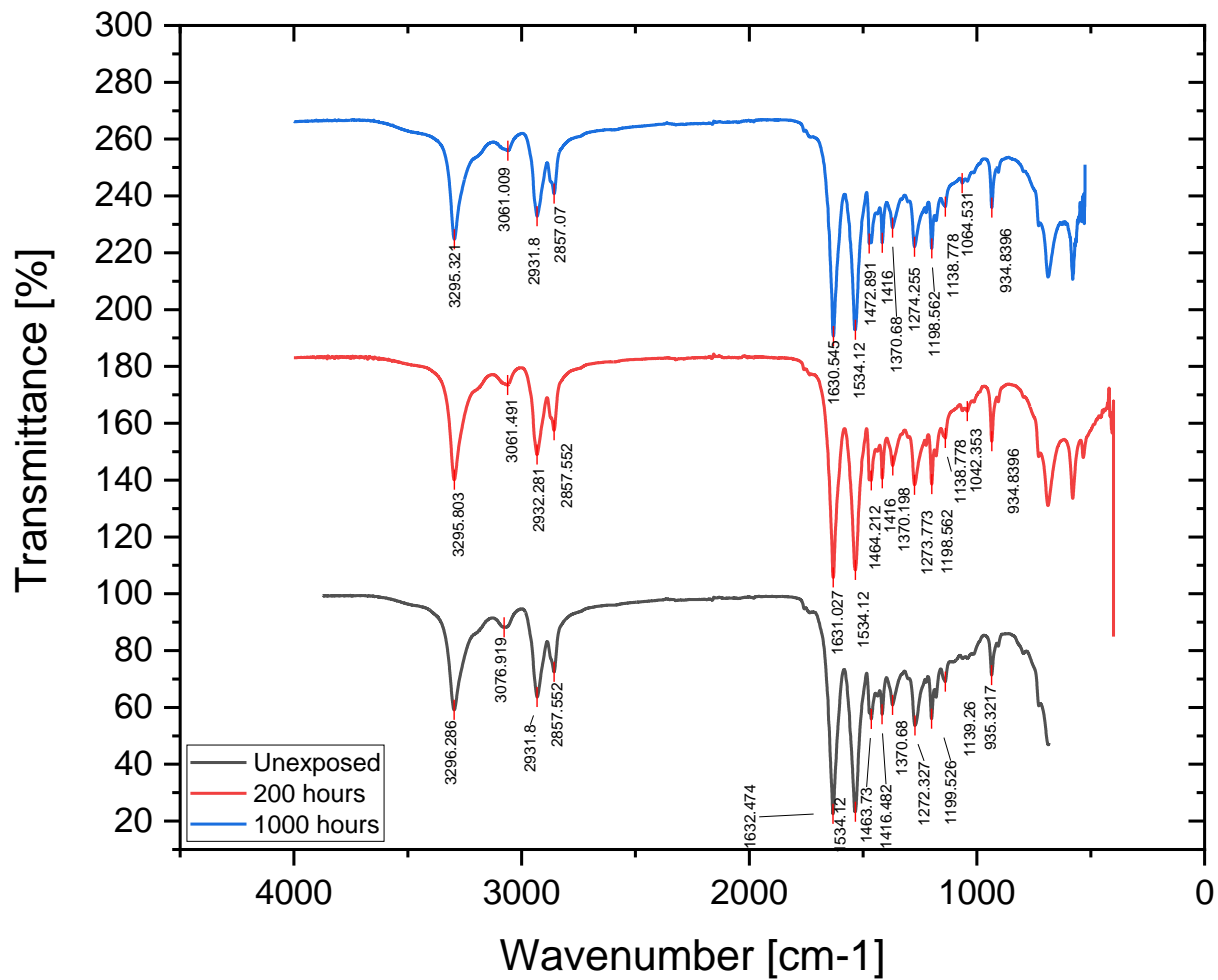
## Nylon-6,6 10 MPa sCO<sub>2</sub> Exposure



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# Attenuated Total Reflectance FTIR on Nylon 6,6 40 MPa pressure sCO<sub>2</sub> at 100°C temperature

## Nylon-6,6 40 MPa sCO<sub>2</sub> Exposure

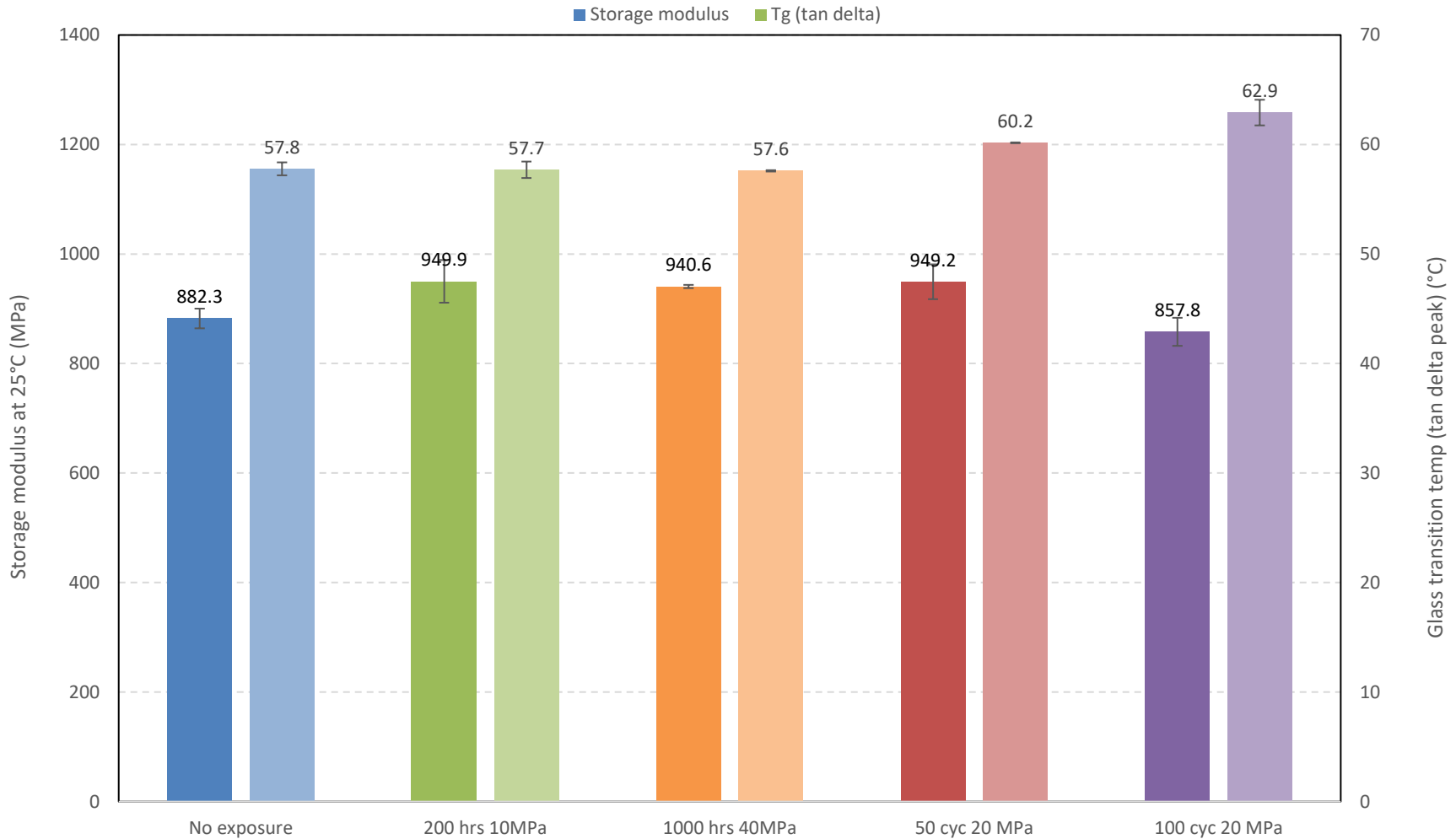


# Dynamic Mechanical Thermal Analysis (DMTA) on Nylon 6,6

## Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure



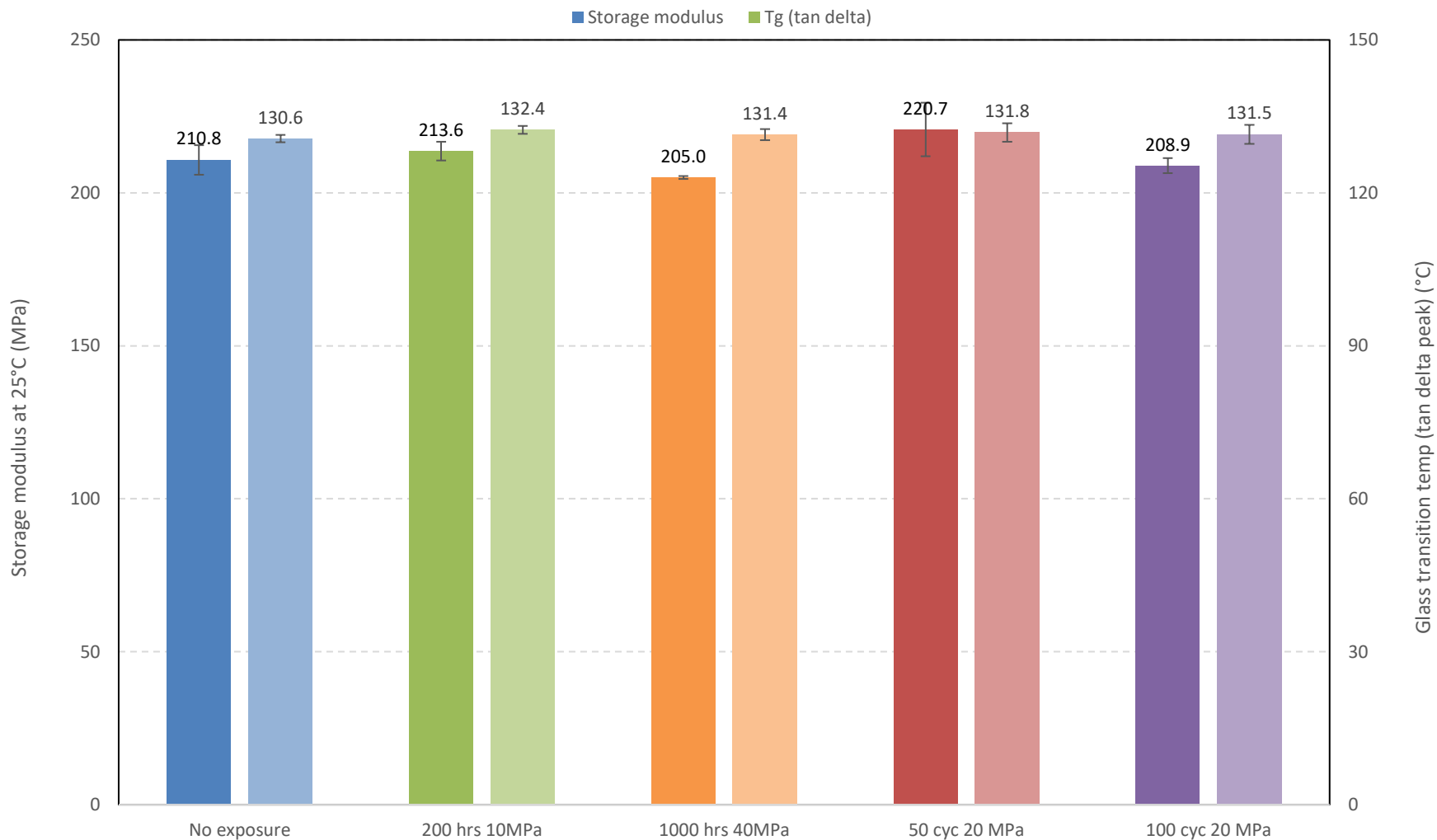
SCO<sub>2</sub> exposure, Nylon 6/6, before and after 50-150-50°C thermal cycles at 20 MPa  
DMTA Rectangular Torsion, 1 Hz, 0.07% strain, 5°C/min heating



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## Dynamic Mechanical Thermal Analysis (DMTA) on PTFE Cycling from 50°-150°-50°C at 20 MPa sCO<sub>2</sub> pressure

SCO<sub>2</sub> exposure, PTFE, before and after 50-150-50°C thermal cycles at 20 MPa  
DMTA Rectangular Torsion, 1 Hz, 0.1% strain, 5°C/min heating





## Polymer compatibility in sCO<sub>2</sub> –

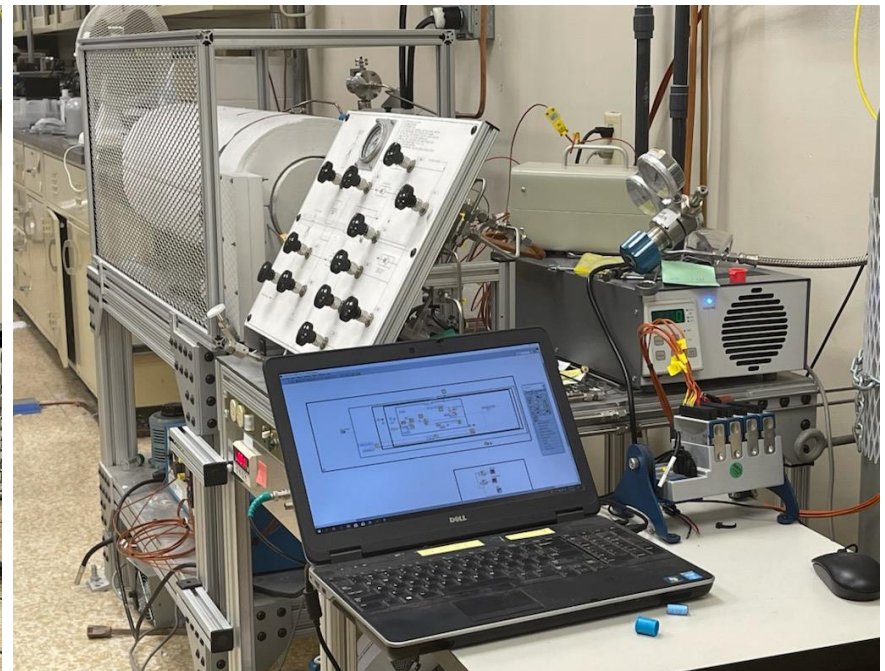
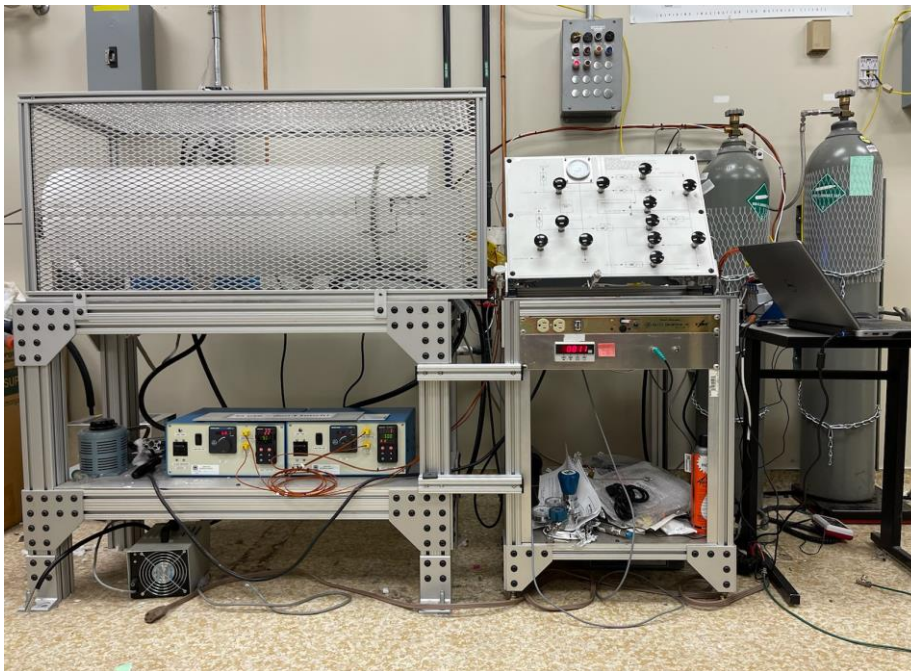
- **Data for lower temperature (55-60°C) and pressure (100-1800 psig) exists; R&D required for temperature range (60-150°C) and pressures (4000-6000 psig)**
- **In-situ monitoring of polymer degradation and failure modes**
  - **polymer failure initiation and growth during the process instead of a post-mortem approach**
  - **Physical and mechanical property degradation studies supported by chemical characterization**
- **Test methods and standards development**
- **Cycling experiments with changes in temperature and sCO<sub>2</sub> pressures**
- **Solubility and permeation of sCO<sub>2</sub> in polymers and influence of fillers and plasticizers on this phenomenon**
- **Factors controlling rapid gas decompression – depressurization rate**
- **Effect of impurities such as H<sub>2</sub>S and chemical aging of polymers**
- **Research and development new material resistant to sCO<sub>2</sub> attack**

**We have scratched the surface...**

## NEXT STEPS FY2020



- Research and development for new materials resistant to  $s\text{CO}_2$  attack at  $150^\circ\text{C}$  and  $250^\circ\text{C}$
- Effect of barrier coatings (metallic and non-metallic) on elastomers – high temperatures possible?
- New characterization tests to understand material degradation mechanisms
- Collaborative work and proposals for polymers and metal alloy work in  $s\text{CO}_2$





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