

Experimental Demonstration of a Coal Fired Primary Heat Exchanger in a sCO₂-based Power Cycle

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Project Team and Discussion Agenda

Project Team

- Brigham Young University
- **Reaction Engineering International**
- Riley Power, Inc (Babcock Power)
- Echogen Power Systems
- Linde
- San Rafael Energy Research Center (SRERC)

Agenda

- SRERC Test Facility
- L1500 Furnace
- Furnace Modeling
- Primary Heat Exchanger Design
- Testing Campaigns
- Conclusions
- Acknowledgments

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SRERC Test Facility

Facility Research Focus:

- Nuclear Reactor & Fuel Processing
- Power Cycle Technologies
- Solar Thermal Energy Systems
- Manufacturing

Facility Upgrades

- Electrical
- Piping
- Cooling System
- Auxiliary systems
 - CO₂ inventory system
 - Safety system and equipment
- Foundations and Facilities



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Fig4: Satellite View of San Rafael Energy Research Center Facility with L1500 Furnace.

Fig5: Echogen Power Systems Thermal Management Fig6: Linde CO₂ Storage Tank Installed at System Installed at SRERC. SRERC.



L1500 Furnace

- 3-zone configuration: radiative, transition and lacksquareconvective sections.
- Refractory lined

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- Dual-register, dual-swirl low-NOx burner
- Equipped with primary, inner secondary and outer secondary air injection.



Burner

configuration, radiative, transition and convective.



1500kW_{th} pilot-scale entrained flow combustor

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Fig2: L1500 Furnace Burner w/Inlet Fuel Manifold

L1500 Furnace Cont.

- Water-cooled, cross-flow heat exchanger in convective section (shown in foreground).
- A baghouse captures particulate entrained in \bullet process air.
- Gravimetric feed system with auger screw
- Fuels for this program consist of natural gas and western US bituminous coal.

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Fig3: L1500 Furnace. Convective Section (in foreground) with Exhaust Piping and Cooling Manifold.

Impact of Firing Rate

- Increasing the firing rate from 0.879MW to 1.76MW (Param2) was effective in enhancing heat transfer.
- A simultaneous increase in excess air played a crucial role in decreasing peak heat flux.

Total PHX Duty

Maximum Inc. Heat Flux to PHX

Table1: CFD Results, Baseline and Param2 Cases

Units	Baseline	Param2
MW	0.632	1.143
W/m2	218,000	196,000

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Fig7: CFD Heat Flux Comparison, Baseline and Param2 Cases

Fig8: CFD Gas Temperature Comparison, Baseline and Param2 Cases

Impact of Extended HX Surface

- Extending the heat exchanger by 2ft decreased peak heat fluxes by nearly 6%, as demonstrated in Param6 compared to Param2.
- Param6 was the selected lacksquareinstallation option.

Total PHX Duty

Maximum Inc. Heat Flux to PHX

Table2: CFD Results, Param2 and Param6 Cases

Units	Param2	Param6
MW	1.143	1.135
W/m2	196,000	185,000

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Impact of Burner Swirl

Higher peak temperatures observed

Impact of Staging Air

- Higher peak temperature
- Increased incident flux

Impact of Bluff Body

Swirl reduction produced a narrower flame sheet near burner Rapid gas mixing yielded substoichiometric combustion and higher fluxes in some cases

Staging air elongates the flame, reducing front-end heat flux Downstream mixing issues observed producing substoichiometric combustion

Addition of the bluff body enhanced mixing while extending heat release Observed unfavorable peak heat flux due to intensified mixing

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Impact of Natural Gas Flame Running on 100% natural gas lacksquare

- Increased heat fluxes at the lacksquarenear-burner end of the radiant section.
- Produced a substantial increase in peak tube metal temperatures (from 1100°F to $1400^{\circ}F$
- Generated a 10% rise in predicted heat transfer to the PHX.

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Fig10: PHX Total Heat Transfer Comparison Between Coal and Natural Gas

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100% Nat. Gas

Design Conditions:

	Units	(USC)	Units	s (SI)
CO ₂ Inlet Temperature	°F	779	°C	415
CO ₂ Outlet Temperature	°F	1112	°C	600
CO ₂ Flow Rate	lb/hr	43640	kg/s	5.5
CO ₂ Operating pressure Max Allowable Working	PSIA	2955	MPa	20.37
Pressure	PSIA	3975	MPa	27.41
 Tangent wall desig 	n per	ASME	Sect.I	
Material selection	Super	304H		
 Limited surface area due to retrofit 				
application.				
Sensible heat transfer presented design				
challenges				
 Managing heat flux 	x is cri	tical fo	or mai	ntainir
PHX integrity.				
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Fig11: Primary Heat Exchanger (PHX) Installation

- Embedded heat flux sensors aid in verifying thermal modeling
 - 6 Locations
 - Qty: 2, Near-wall
 - Qty: 2, Mid-wall
- Flow balancing valves are used to manage flow distribution and maintain desire flux levels.
- Skin thermocouples monitor tube metal temperatures.

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Fig14: (Right) Flow Balancing Valve Installation with Outlet Header.

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- Heat transfer model aligns well with test data for the radiant module but significantly differs in the convective section due to observed fouling.
- Thermal resistance assumptions impacted sCO₂ exit temperature predictions.
- PHX efficiency = 60-65% (meets predictions).
- Peak heat input of 1.63MW from fuel.
- Adjusting sCO₂ flow rate demonstrated the capability to achieve full design conditions.

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Overall Heat Transfer to PHX

Measured total PHX pressure drop: • dP = 4.7bar (68psi) Model predicted total PHX pressure drop: dP = 3.6bar (52psi)Incorporating valve and pressure drop, dP = 4.2

PHX Pressure L

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Measured Total SUPERCRITICAL STORAGE COMPANY, INC

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i) d piping lo bar (61ps	osses yields a i, 89%)	tota
Loss Compa	rison	

Temperature distribution in the radiant panels aligned well with predictions.

Sensor Position	CO ₂ Temps at Convective Outlet °C	CO ₂ Temps at Radiant Outlet (unbalanced) °C	CO ₂ Temps at Radiant Outlet (adjusted) °C
1	371	552	563
2	370	544	556
3	366	553	565
4	368	547	556
5	367	557	567
6	364	550	555
7	354	551	564
8		556	554
9		61*	59*
10		548	555
11		554	561
12		560	567
13		562	584
14		583	564
15		563	583
16		590	583

Table3: PHX Tube Temperature Distribution Comparison Between Unbalanced and Adjusted Flow Balancing Valves

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Testing

Campaign 2 Achievements Additional +70Hrs continuous operation. • Avg. 1MW of heat input to PHX.

Fig22: Flow Distribution During Campaign 2 Endurance Testing

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Conclusions

- Increased heat rate of 1.76MW.
- Peak heat flux maintained below 175,000 W/m2.
- Near-burner crossmember arrangement reduces peak heat flux.
- Increased excess air mitigates adiabatic flame temperature.
- Measured data aligns well with model predictions.
- Pressure losses aligned with predictions, and flow distribution improved by adjusting balancing valves.
- Flux sensor readings require further review for accuracy.
- Ongoing testing goals:
 - Obtain/full design conditions. Investigate material integrity to reduce risks associated with design and manufacturing.

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