



Experimental Demonstration of an Advanced CO₂ Axial Compressor for CO₂-based Power Cycles and Energy Storage Systems

The 8th Supercritical CO₂ Power Cycles Symposium

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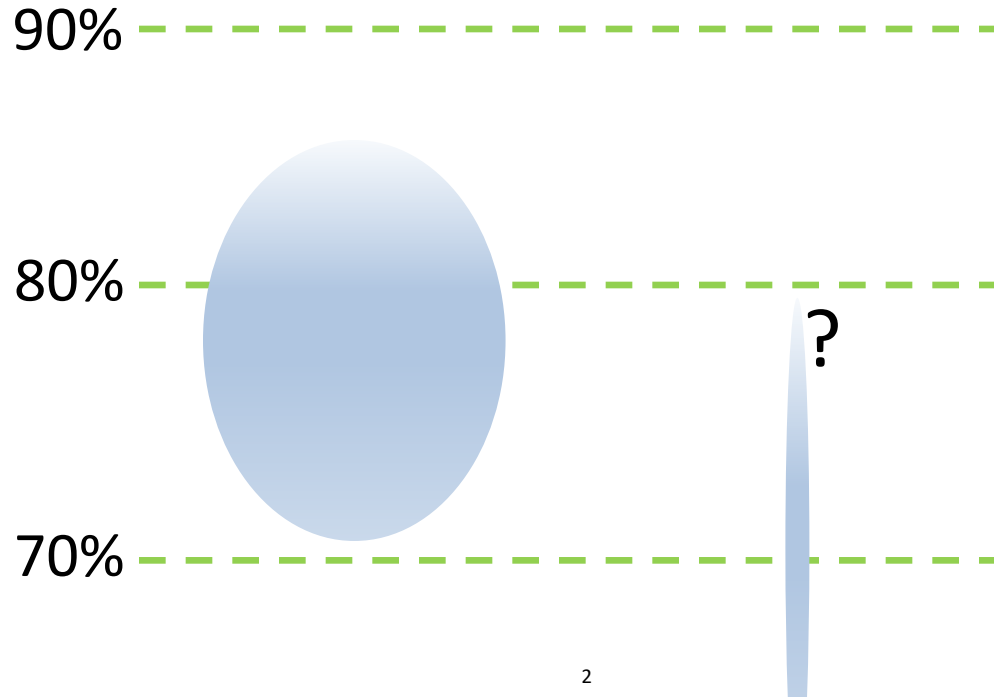
3 Echogen Power Systems, Akron, OH, USA

Feb 26-29, 2024

Centrifugal Compressor

Air

CO₂



Centrifugal Compressor

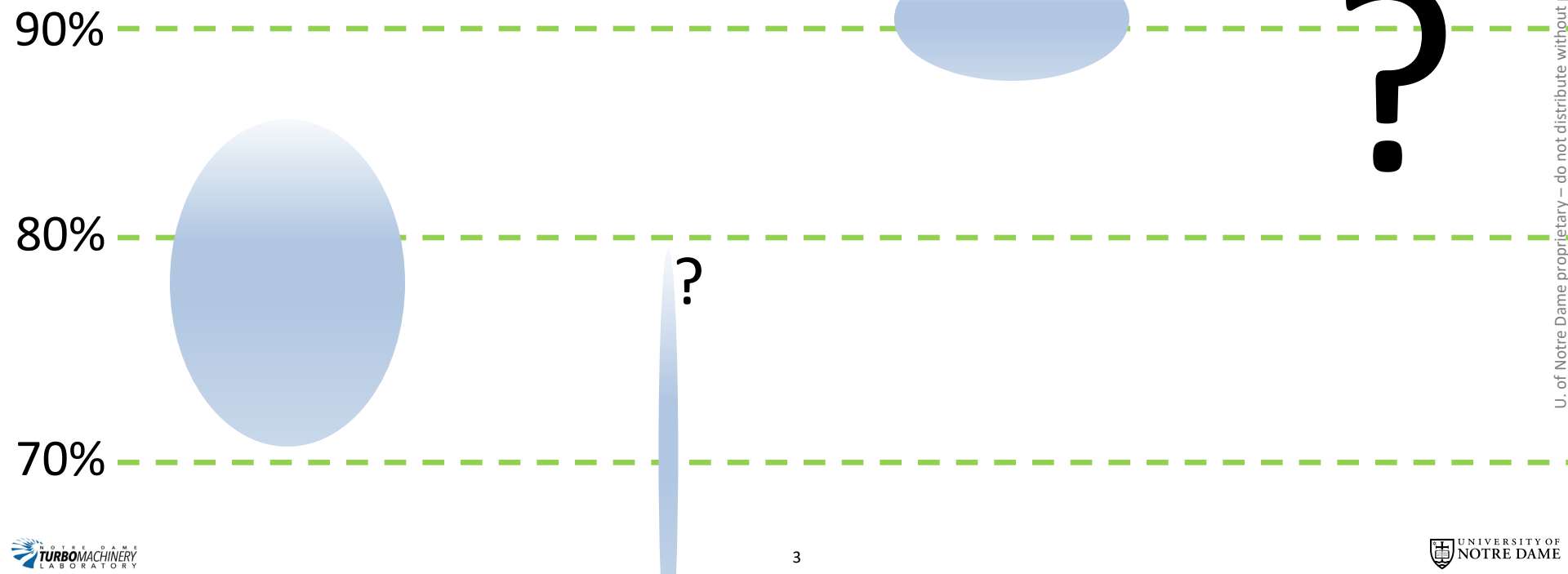
Axial Compressor

Air

CO₂

Air

CO₂



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❑ Question 1

Does the axial CO₂ compressor have high efficiency/performance potential?

❑ Question 2

Can we evaluate the performance of axial CO₂ compressor(s) experimentally with high fidelity?



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Mark G. Turner



Axial Compressor

		IGV	Rotor 1	Stator 1
Number of airfoils	-	43	69	114
Radius of Blade Leading Edge Tip	mm	131	129	128
Radius of Hub	mm	102	102	102
Leading Edge Blade angle at mid-span	deg	0	-58.78	48.53
Trailing Edge Blade angle at mid-span	deg	10.7	-42.46	14.0

Rotational Speed	rpm	19,800
Inlet Total Pressure	kPa	2,770
Inlet Total Temperature	°C	98.0
Total to Total Pressure Ratio	-	1.41
Mass flowrate	kg/s	125



[Stage 1 rotor]

[1] Matthew Ha, Justin Holder, Saugat Ghimire, Adam Ringheisen, and Mark. G. Turner, 2022, "Detailed Design and Optimization of the First Stage of an Axial Supercritical CO₂ Compressor," ASME Turbo Expo 2022, GT2022-82590.

[2] Justin M. Holder, Adam Ringheisen, Matthew Ha, Saugat Ghimire and Mark. G. Turner, 2022, "Improved Automated Turbomachinery Hot-to-Cold Transformation with Cold-to-Hot Capabilities For Off-Design Analysis," AIAA SciTech 2022 Forum, AIAA2022-2436.

IGV & Stator 1

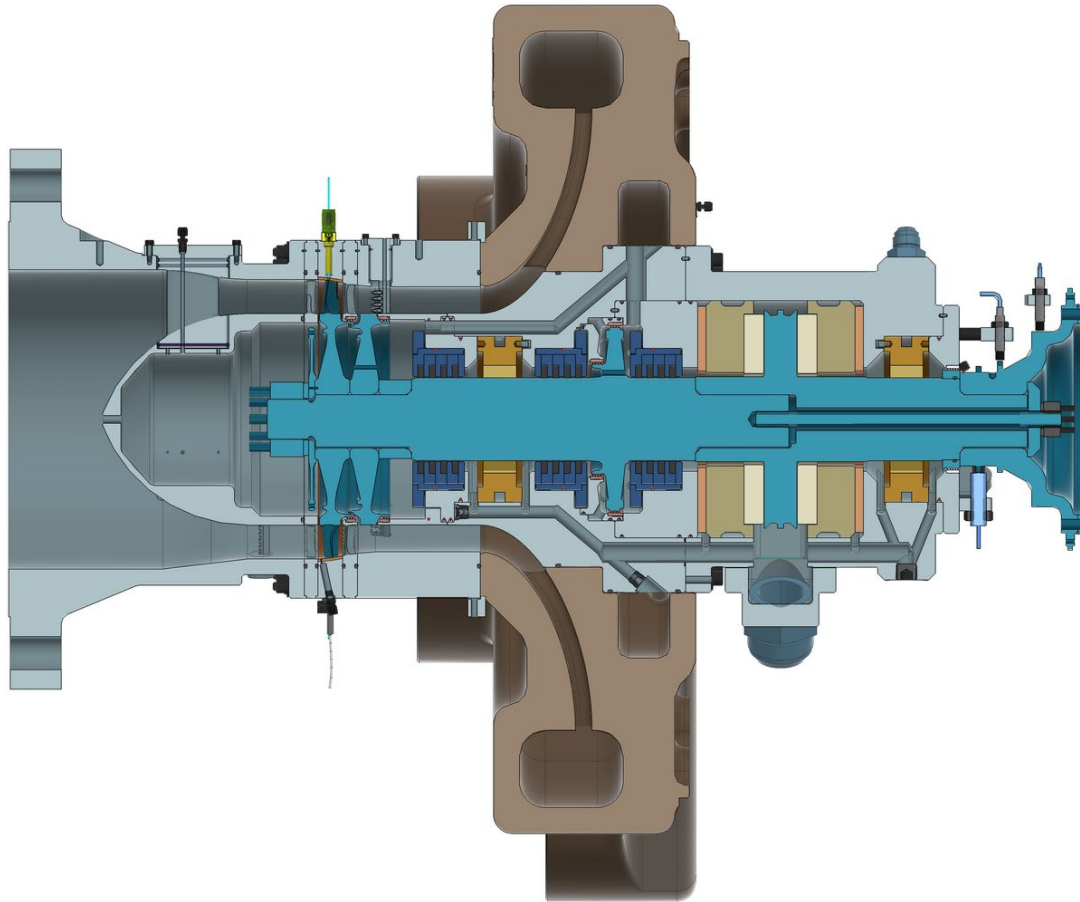


[IGV]

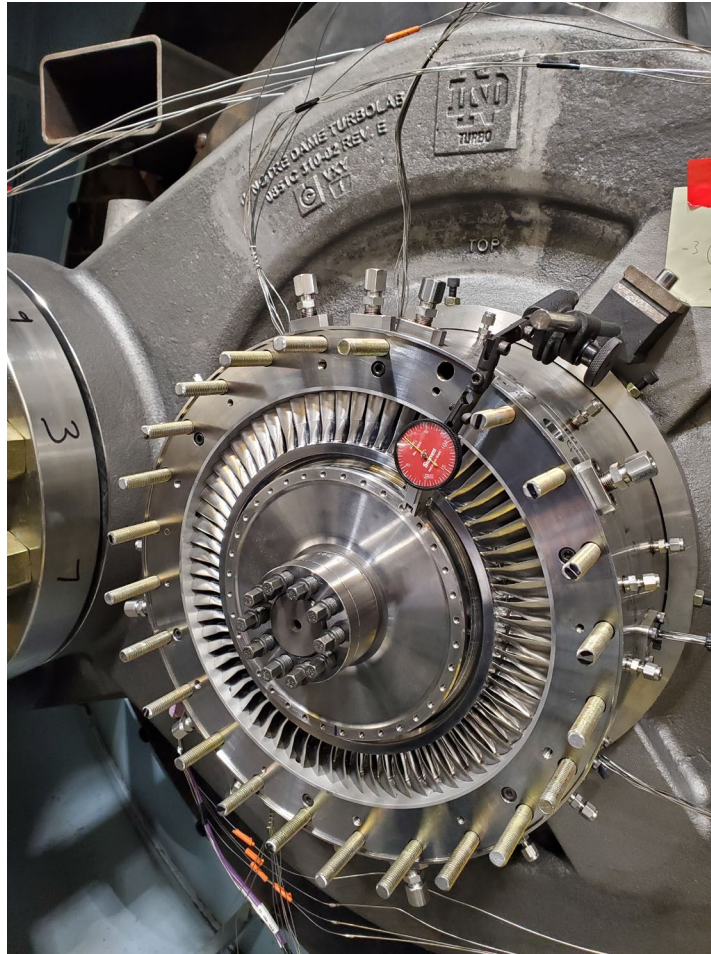


[Stator 1]

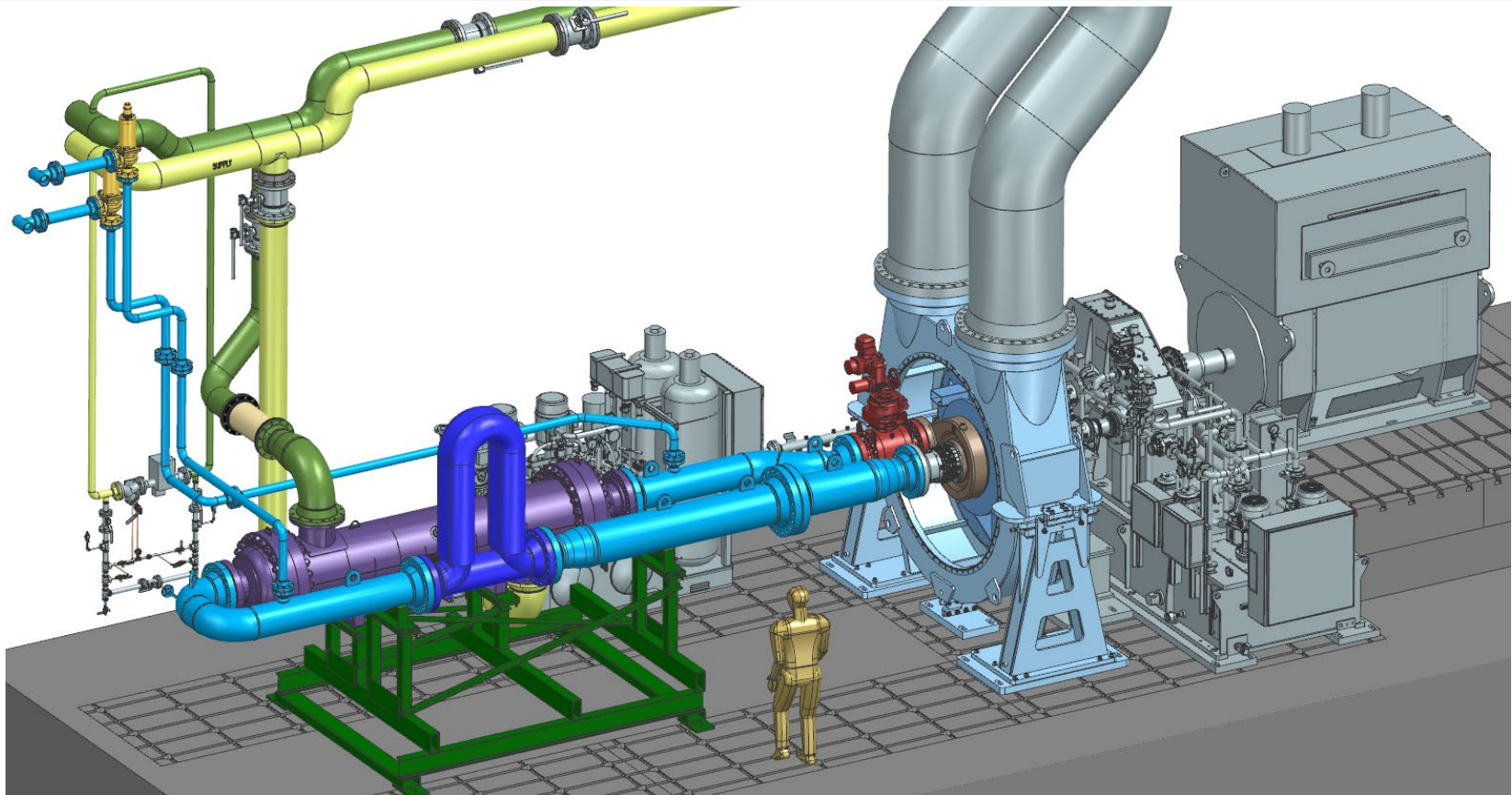
1.5 Stage Compressor Test Rig



Axial Compressor



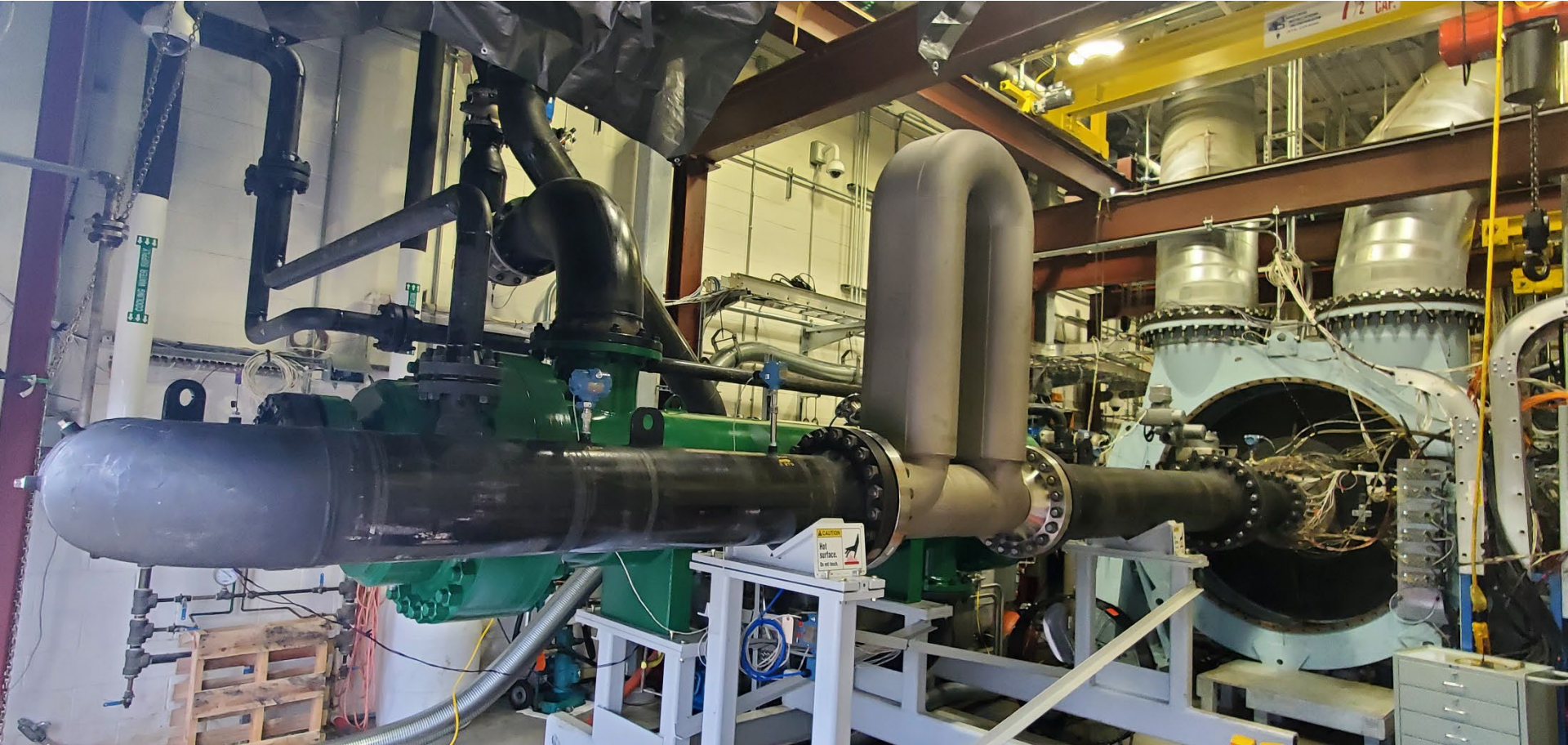
10MW sCO₂ Compressor Test Facility @ NDTL



(Ref) Jeongseok Kang, Alex Vorobiev, Joshua D. Cameron, Scott C. Morris, Ryan Wackerly, Kyle P. Sedlacko, Jason D. Miller, and Timothy J. Held, 2021, "10MW-class sCO₂ Compressor Test Facility at the University of Notre Dame," The 4th European sCO₂ Conference for Energy Systems, March 22-26, 2021-sCO₂.eu-144.

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10MW sCO₂ Compressor Test Facility @ NDTL



Facility : Cooling Towers & CO2 Inventory System



Cooling towers – 12MW

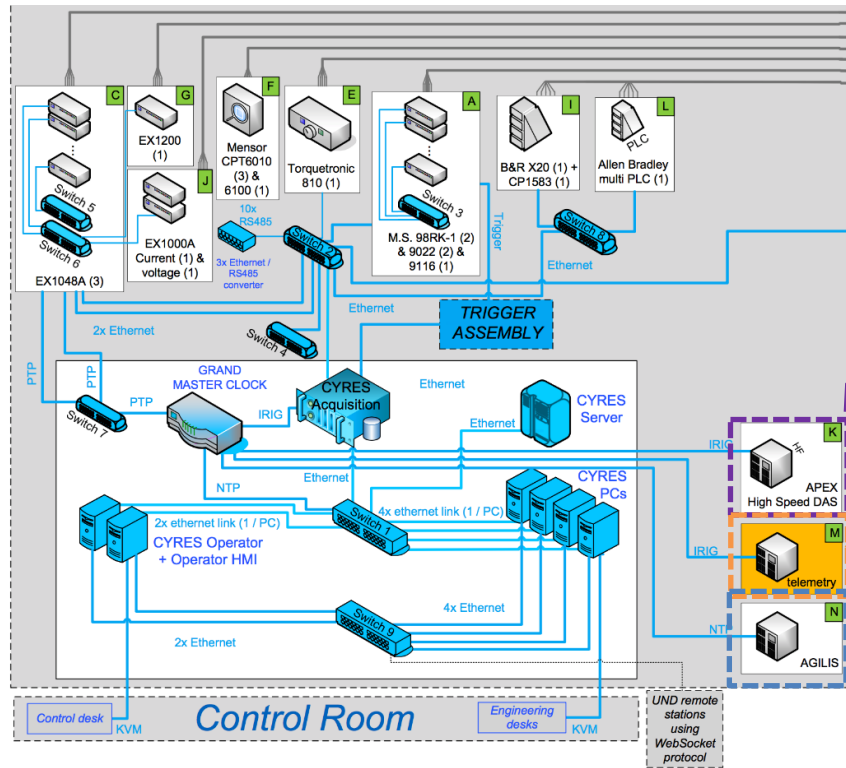
(CO₂ : 99.97% – 99.99%)



2 X 5 Ton (12,000LBS) CO2 tanks

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Architecture of Instrumentation & Data Acquisition System



Dynamic Data Acquisition

This block details the Dynamic Data Acquisition system, which includes:

- Sensors:** Accelerometers, Proximitors, Kulites, and Strain gauges.
- Signal Processing:** Each sensor type is connected to a Signal conditioner.
- Time Synchronization:** A Time server (+GPS) provides precise timing to the APEX Server (+S/W).
- Server:** The APEX Server (+S/W) receives and processes the data.

- 4 Dynamic DAQ systems
- 300 Channels
- Precision Filters
- Time stamped data

Telemetry

This block details the Telemetry system, which includes:

- Sensors:** Used with strain gauges, Kulites, RTDs, TCs, etc.
- Transmitters:** Rotating (Rotor Coil) and Stationary (Stator Coil).
- Receiver:** A Receiver Rack receives the RF Signal from the coils.

- 3 Telemetry systems
- Used with strain gauges, Kulites, RTDs, TCs, etc.
- Fixed Sampling Frequency at ~100KHz

NSMS

This block details the NSMS (Non-Synchronous Measurement System) system, which includes:

- Sensors:** NSMS probes.
- Signal Processing:** A Signal conditioner processes the probe signals.
- System:** The processed signals are sent to a rack-mounted system.

- 2 NSMS systems
- 16 light probes and channels

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$$\eta_{TT} = \frac{h_{T2S} - h_{T1}}{h_{T2} - h_{T1}}$$

$$PR(TT) = \frac{P_{T2}}{P_{T1}}$$

h_{T1} – mass specific total enthalpy, stage inlet

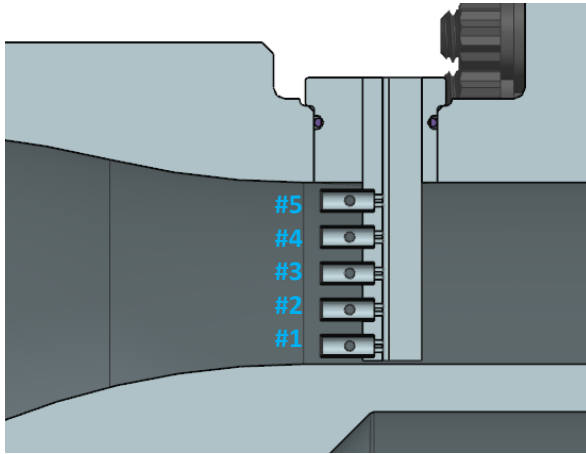
h_{T2} – mass specific total enthalpy, stage exit

h_{T2S} – mass specific total enthalpy for isentropic flow, stage exit

$$h_T = h(T_T, P_T)$$

$$h_{T2S} = h(s_{T1}, P_{T2})$$

$$s_{T1} = s(T_{T1}, P_{T1})$$



[Inlet Rakes : 3EA]

5 Kielheads per rake

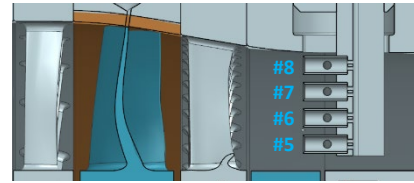
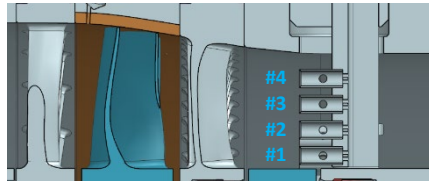
: 10%(#1), 30%(#2), 50%(#3), 70%(#4),
and 90%(#5) of the span



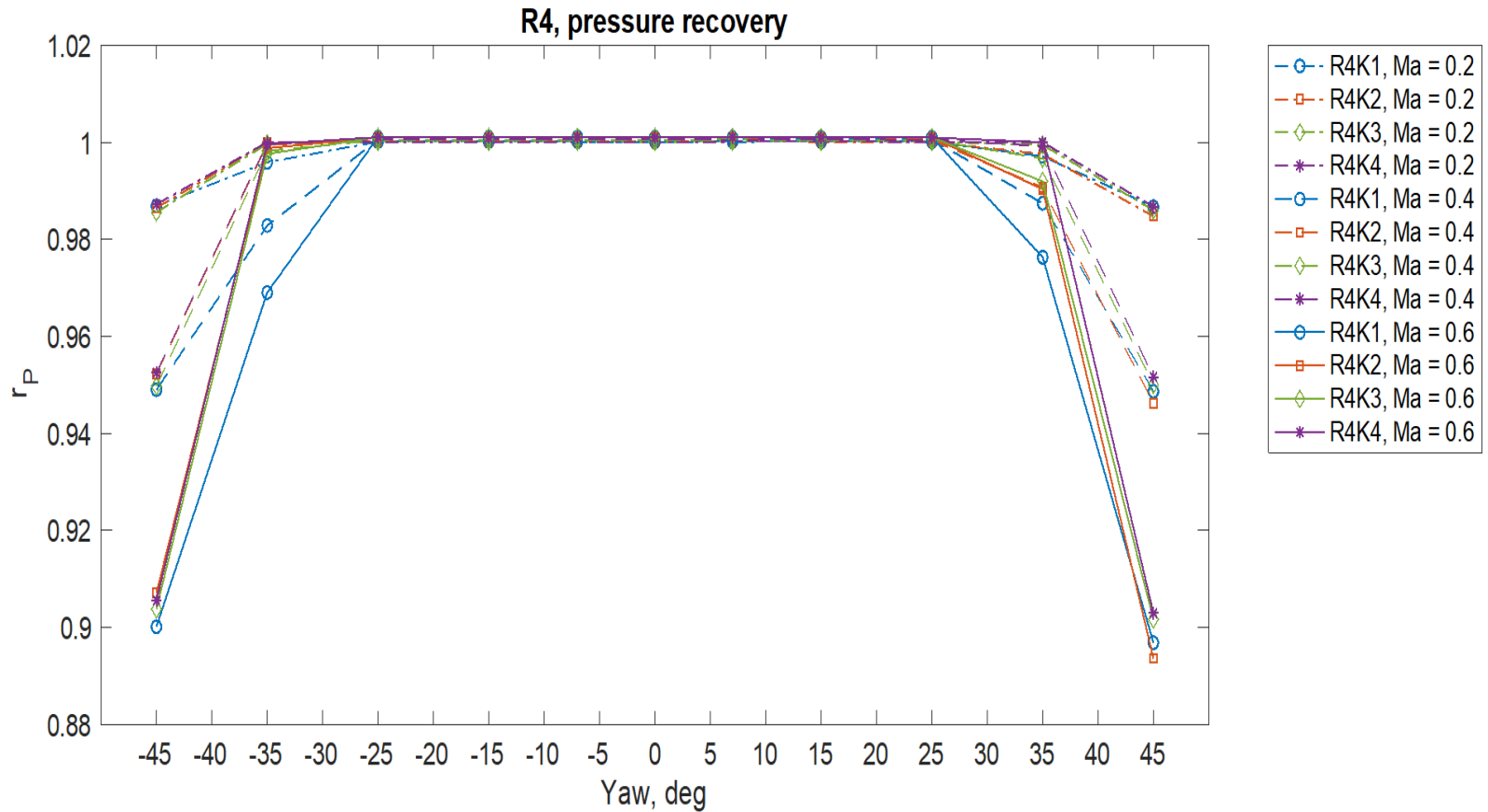
[Exit Rakes : 6EA]

4 Kielheads per rake X 2 set with different insertion depth

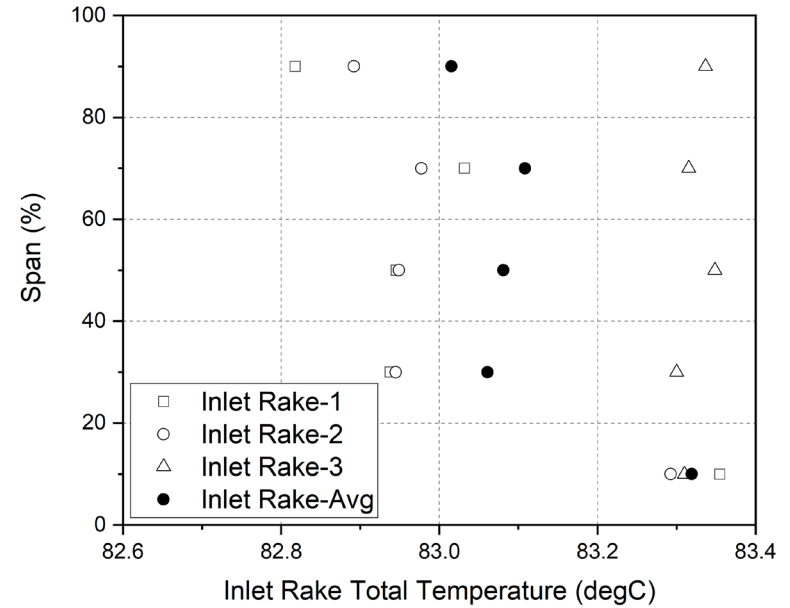
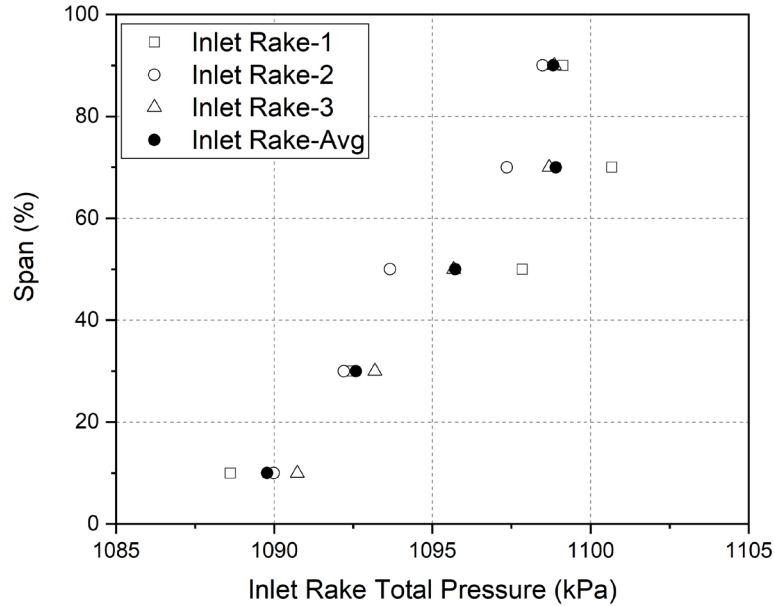
11.4%(#1), 22.5%(#3), 33.5%(#3), 44.6%(#4), 55.7%(#5), 66.8%(#6), 77.8%(#7), and 88.9%(#8) of the span



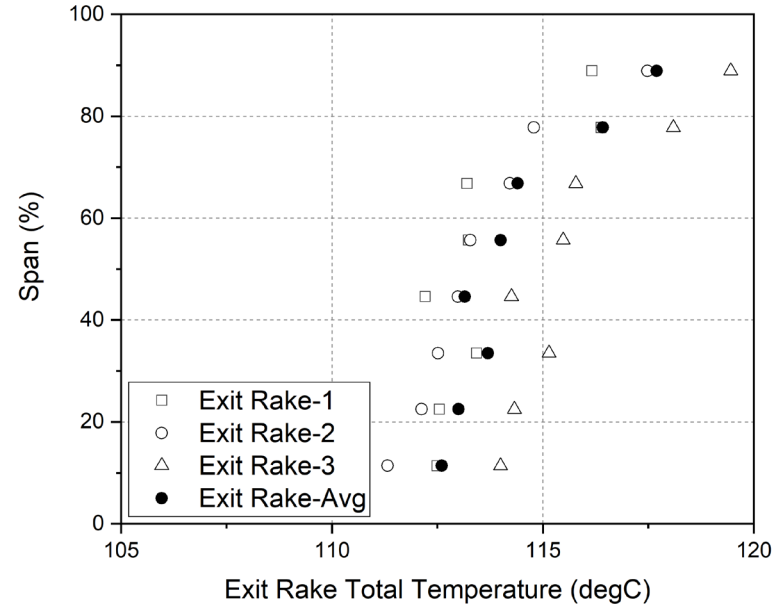
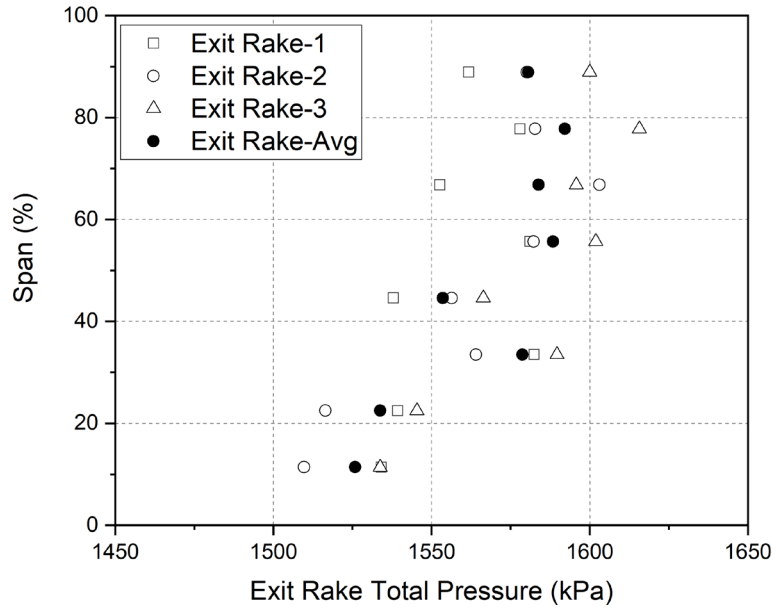
Rake Calibration



Example Data from Inlet Rakes (100% speed)



Example Data from Exit Rakes (100% speed)



Uncertainty Analysis (1) - Efficiency

$$\eta_{TT} = \frac{h_{T2S} - h_{T1}}{h_{T2} - h_{T1}}$$

$$\delta\eta^2 = \left(\frac{\partial\eta}{\partial h_{T1}} \delta h_{T1} \right)^2 + \left(\frac{\partial\eta}{\partial h_{T2}} \delta h_{T2} \right)^2 + \left(\frac{\partial\eta}{\partial h_{T2S}} \delta h_{T2S} \right)^2$$

$$\delta\eta^2 = \left(\frac{\eta - 1}{h_{T2} - h_{T1}} \delta h_{T1} \right)^2 + \left(\frac{\eta}{h_{T2} - h_{T1}} \delta h_{T2} \right)^2 + \left(\frac{1}{h_{T2} - h_{T1}} \delta h_{T2S} \right)^2$$

$$\delta h^2 = \left(\frac{\partial h(T, P)}{\partial T} \delta T \right)^2 + \left(\frac{\partial h(T, P)}{\partial P} \delta P \right)^2$$

$$\delta h^2 = \left(\frac{\partial h(s, P)}{\partial s} \delta s \right)^2 + \left(\frac{\partial h(s, P)}{\partial P} \delta P \right)^2$$

$$\delta s^2 = \left(\frac{\partial s(T, P)}{\partial T} \delta T \right)^2 + \left(\frac{\partial s(T, P)}{\partial P} \delta P \right)^2$$

$$\begin{aligned}
 \delta\eta^2 &= \frac{1}{(h_{T2} - h_{T1})^2} \left\{ (\eta - 1)^2 \left[\left(\frac{\partial h(T, P)}{\partial T} \Big|_{T1} \delta T \right)^2 + \left(\frac{\partial h(T, P)}{\partial P} \Big|_{T1} \delta P \right)^2 \right] \right. \\
 &+ \eta^2 \left[\left(\frac{\partial h(T, P)}{\partial T} \Big|_{T2} \delta T \right)^2 + \left(\frac{\partial h(T, P)}{\partial P} \Big|_{T2} \delta P \right)^2 \right] \\
 &\left. + \left(\frac{\partial h(s, P)}{\partial s} \Big|_{T2S} \right)^2 \left[\left(\frac{\partial s(T, P)}{\partial T} \Big|_{T2S} \delta T \right)^2 + \left(\frac{\partial s(T, P)}{\partial P} \Big|_{T2S} \delta P \right)^2 \right] + \left(\frac{\partial h(s, P)}{\partial P} \Big|_{T2S} \delta P \right)^2 \right\}
 \end{aligned}$$

□ Total uncertainty of the isentropic efficiency (η_{TT}) = $\pm 1.96\%$

* Including

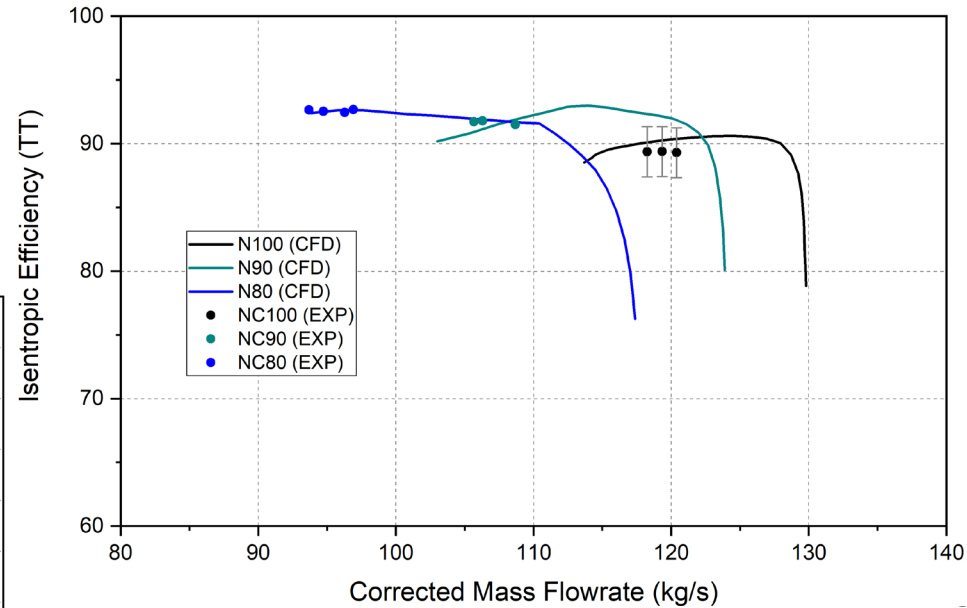
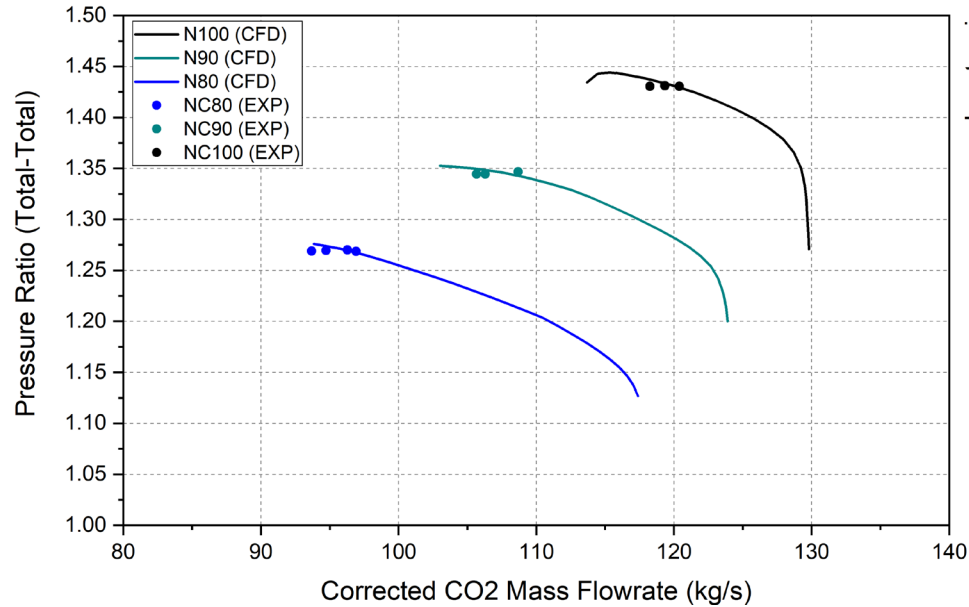
- ✓ Calibrated E-Type Thermocouple
- ✓ DAQ system uncertainty
- ✓ Accuracy of pressure scanner
- ✓ CO2 property (Refprop 10.0)

$$PR(TT) = \frac{P_{T2}}{P_{T1}} = \frac{P_{REF} + P_{NS02}}{P_{REF} + P_{NS01}}$$

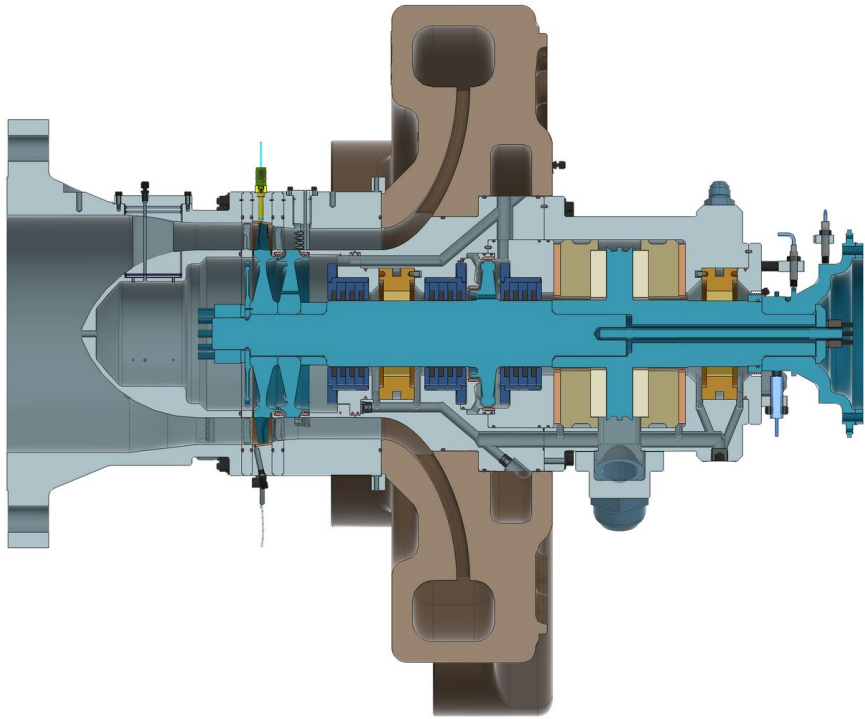
$$\left(\frac{\delta PR}{PR}\right)^2 = \frac{\delta P_{REF}^2 + \delta P_{NS01}^2}{(P_{REF} + P_{NS01})^2} + \frac{\delta P_{REF}^2 + \delta P_{NS02}^2}{(P_{REF} + P_{NS02})^2}$$

□ Total uncertainty of the pressure ratio (TT) @ 100% speed = ± 0.0028

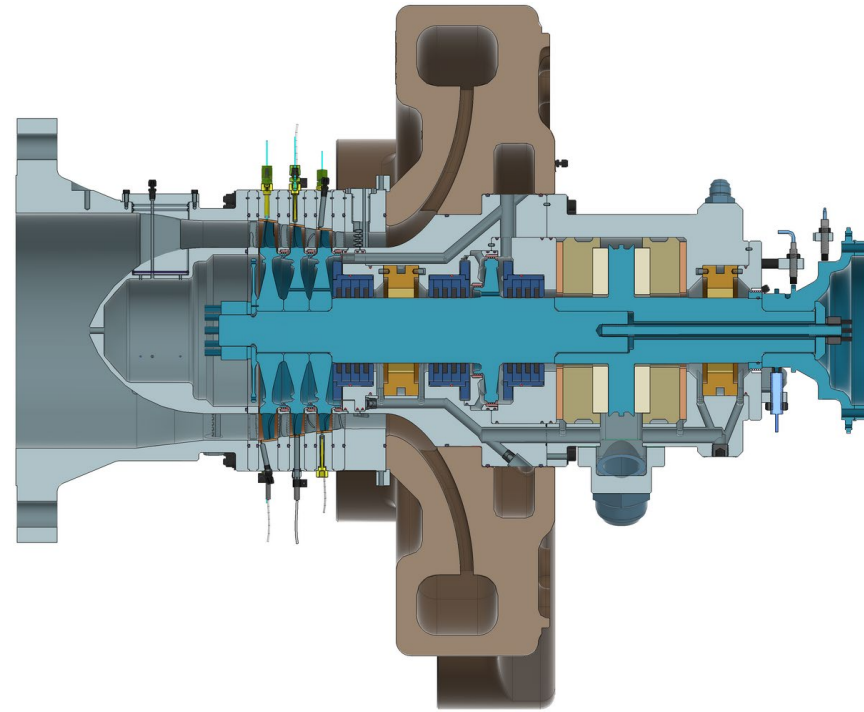
Isentropic Efficiency & Pressure Ratio (TT)



0850 Test Rig (Single and Three Stage)



Single Stage



Three Stage

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Centrifugal Compressor

Axial Compressor

Air

CO₂

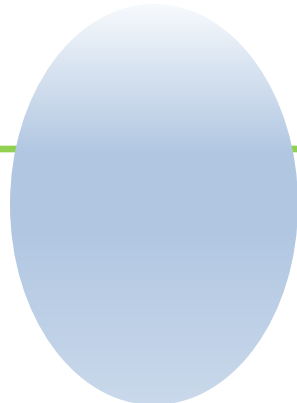
Air

CO₂

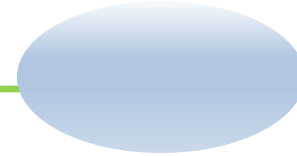
90%

80%

70%



?



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❑ Question 2

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CONCLUSION

• **I** A performance of a **1.5 stage axial CO₂ compressor** has been experimentally measured at the 10MW-class sCO₂ compressor test facility at the University of Notre Dame. The goal of the research is to measure compressor performance with **high fidelity** and to demonstrate the high efficiency potential of the axial-type CO₂ compressor for various CO₂ cycle application.

• **II** The measured total-to-total isentropic efficiency of the compressor at 80%, 90%, and 100% of the speed was about **92.6%, 91.7%, and 89.3%** respectively with the total uncertainty of the isentropic efficiency at 100% speed (19,800rpm) was $\pm 1.96\%$ which is well above the reported highest isentropic efficiency of the compressor so far.

□ Acknowledgement

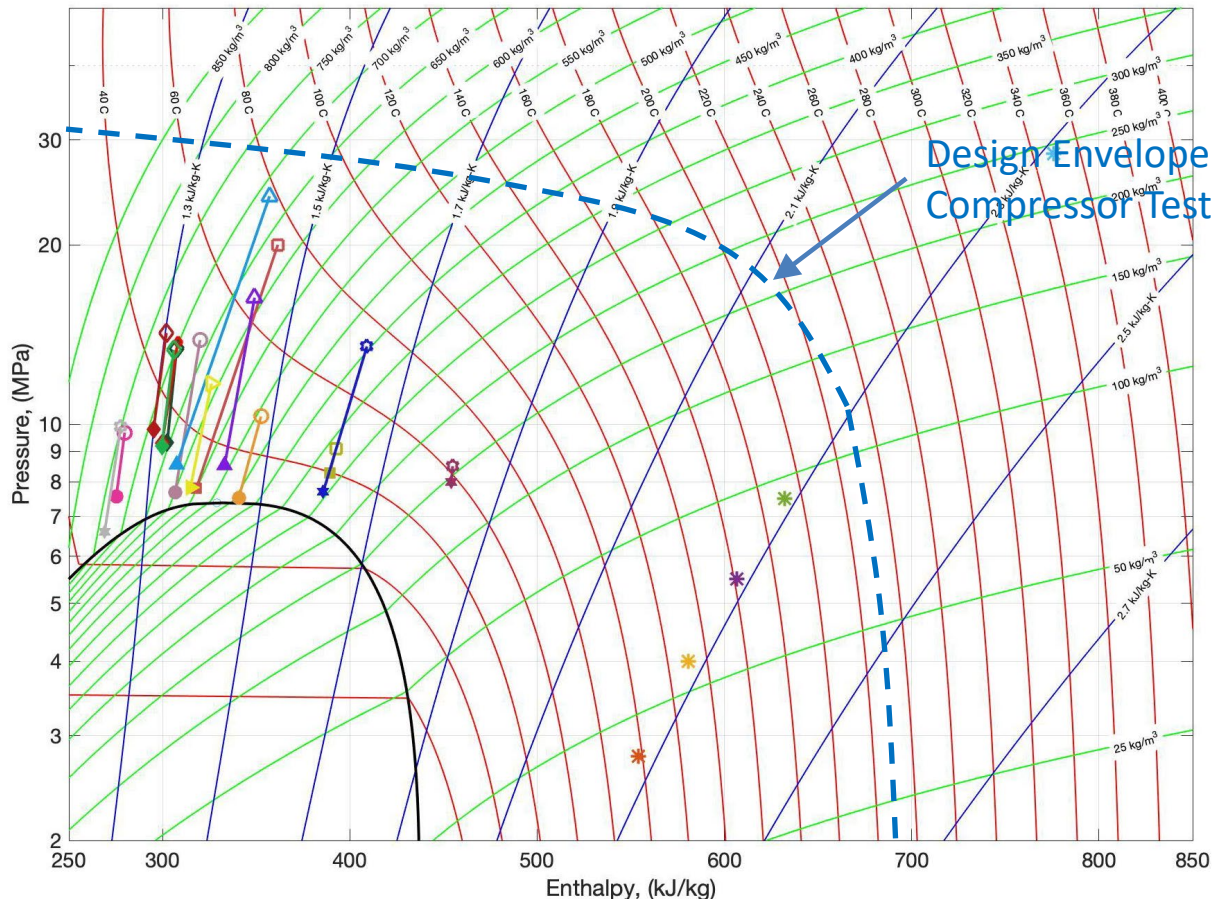


This material is based upon work supported by the U.S. Department of Energy's Office of Energy Efficiency and Renewable Energy (EERE) under the Solar Energy Technologies Office Award Number DE-EE0008997.

□ Thank you for your attention! Q & A

[Appendix]

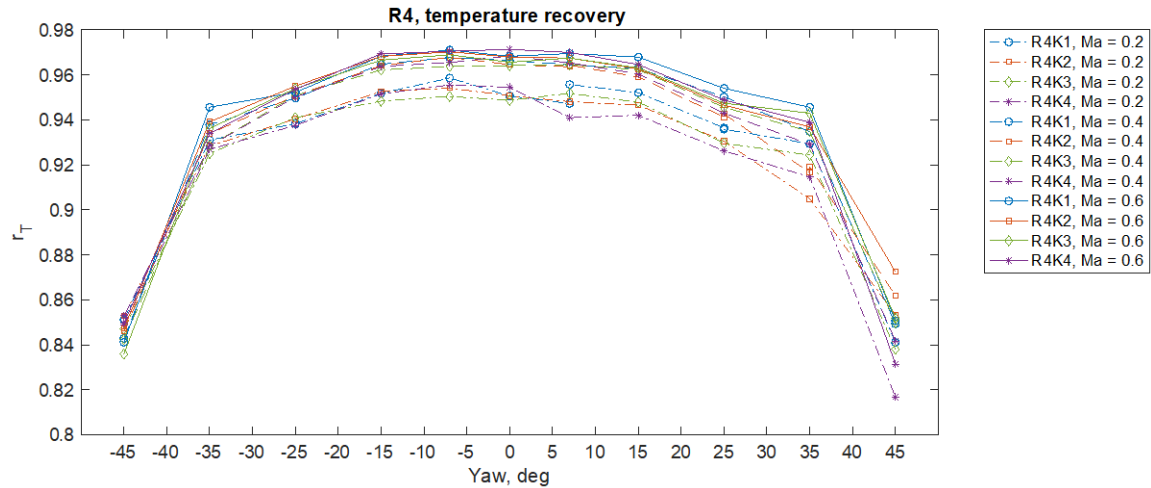
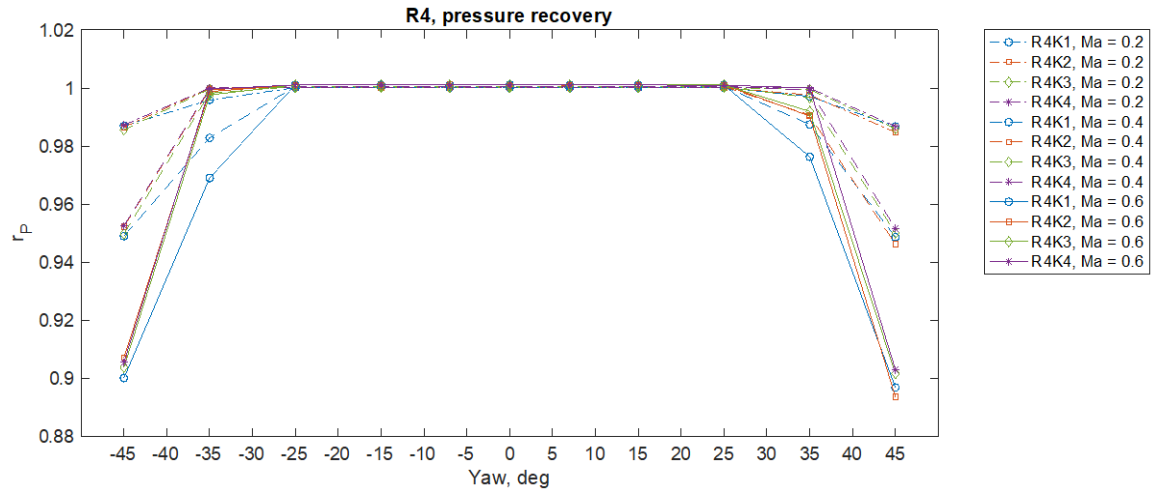
Design Envelope of NDTL sCO₂ Compressor Test facility



Design Envelope of NDTL's sCO₂ Compressor Test Facility

- T = const
- D = const
- S = const
- Wright (2009, SNL)
- Wright (2011, SNL)
- ◆ Kimball (2013, BMPC)
- Pasch (2014, SNL)
- Lee (2014, KAIST & KAERI)
- ◆ Clementoni (2014, BMPC)
- ◆ Clementoni (2016, BMPC)
- Cha (2016, KAIST & KAERI)
- ★ Cho (2016, KIER)
- ◆ Clementoni (2017, NNL)
- ▲ Allison (2018, SWRI)
- ▲ Cich (2018, SWRI)
- ▲ Hacks (2018, Univ. of Duisberg-Essen)
- ★ Cho (2018, KIER)
- ★ Cho (2019, KIER)
- ★ NDTL (EPS) Inlet Conditions For All Stages
- ★ NDTL (EPS) 1-Stage Outlet Conditions
- ★ NDTL (EPS) 2-Stage Outlet Conditions
- ★ NDTL (EPS) 3-Stage Outlet Conditions
- ★ NDTL (EPS) Full Scale and Stage Outlet Conditions

Rake Calibration

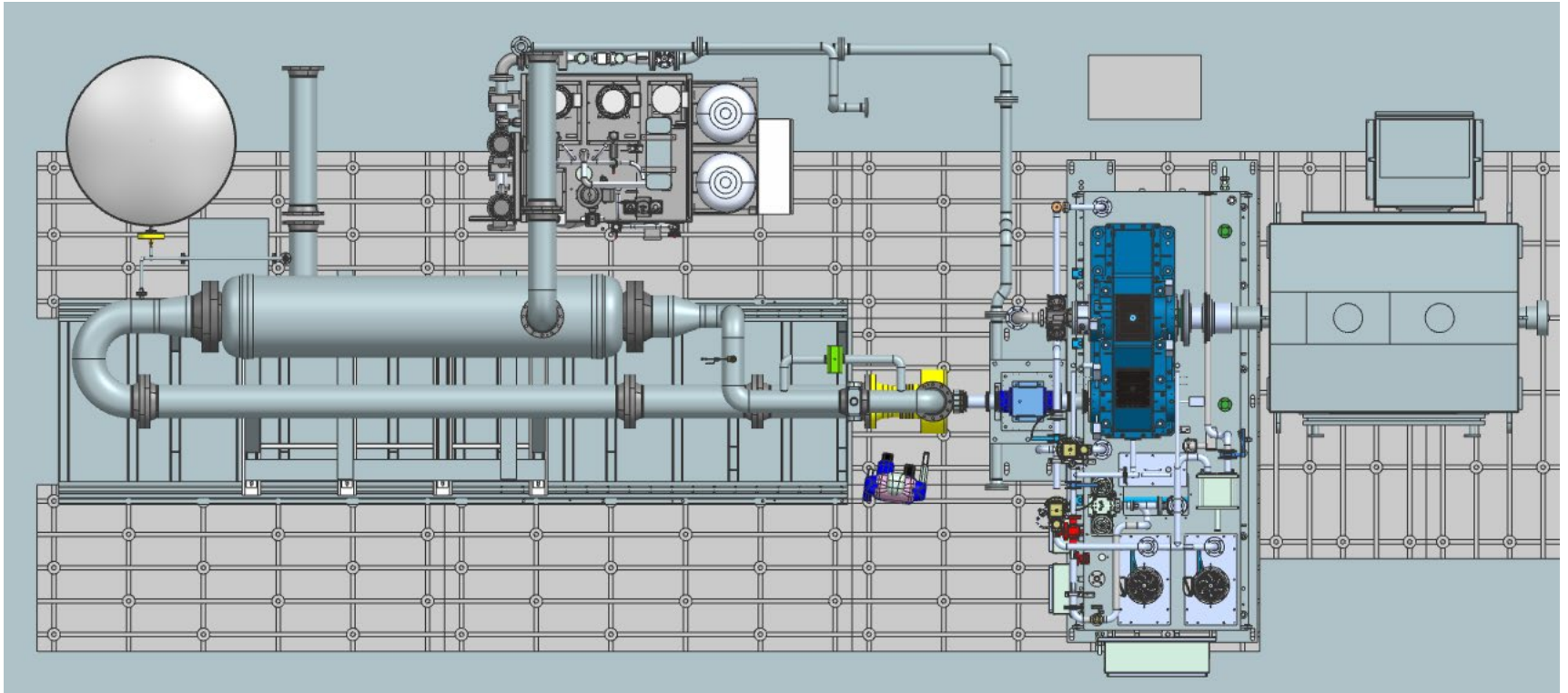


☐ sCO₂ Compressors – Type, Flowrate, Efficiency

Main Author	Year	Institution	Compressor Type	Compressor Driving Power
Steven A. Wright	2009	Sandia National Laboratories	Centrifugal	50 kWe
Masanori Aritomi	2011	Tokyo Institute of Technology	Centrifugal	
Jeff S. Noall	2014	Barber Nichols Inc., Sandia National Laboratories	Centrifugal	55 kW
Jekyoung Lee	2014	Korea Advanced Institute of Science and Technology	Centrifugal	
Timothy Held	2014	Echogen Power Systems	Centrifugal	2.7MW
Eric M. Clementoni	2016	Bechtel Marine Propulsion Corporation	Centrifugal	36.8 - 15.8 kW
Jae Eun Cha	2016	Korea Advanced Institute of Science and Technology	Centrifugal	
Junhyun Cho	2016	Korea Institute of Energy Research	Centrifugal	90 kW
Eric M. Clementoni	2017	Naval Nuclear Laboratory	Centrifugal	
Timothy C. Allison	2018	Southwest Research Institute	Centrifugal	
Eric M. Clementoni	2018	Naval Nuclear Laboratory	Centrifugal	
Jacqueline Lewis	2018	Naval Nuclear Laboratory	Centrifugal	
Alexander Hacks	2018	University of Duisburg-Essen, Research Center Rez	Centrifugal	7 kW
Seungjoon Baik	2018	Korea Advanced Institute of Science and Technology	Centrifugal	26 kW
Stefan D. Cich	2018	Southwest Research Institute, GE Global Research	Centrifugal	4.9 MW
Bongsu Choi	2019	Korea Institute of Energy Research	Centrifugal	90 kW
Yann Le Moullec	2019	EDF R&D China, Shouhang IHW		2.4 MW
Junhyun Cho	2019	Korea Institute of Energy Research	Centrifugal	90 kW
Eduardo Anselmi	2019	Cranfield University	Centrifugal	45 kW
Logan Rapp	2019	Sandia National Laboratories		1MW

Capacity of
Test Facility

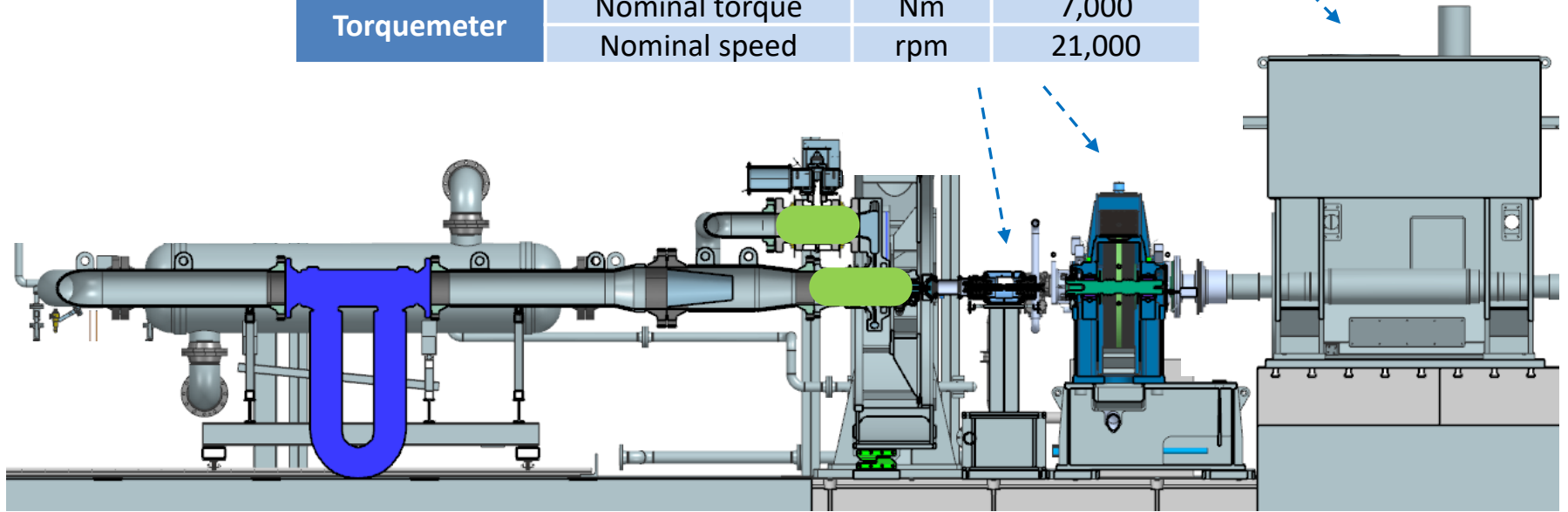
sCO₂ Compressor Test Facility (Top view)



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sCO₂ Compressor Test Facility – Specification of Drive System

Motor	Max. power	MW	10
	Full load speed	kg/s	116
Gear Box	Max. output speed	rpm	19,945
	Rated power	MW	10
Torquemeter	Nominal torque	Nm	7,000
	Nominal speed	rpm	21,000



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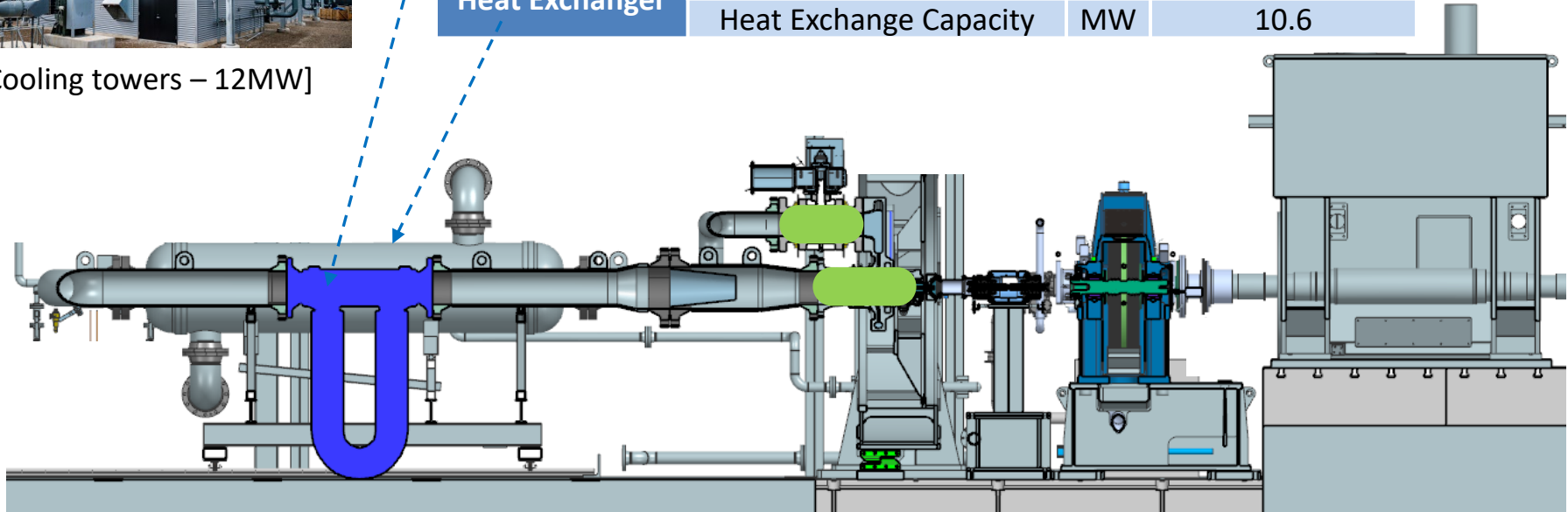
sCO₂ Compressor Test Facility – Specification of Main Loop

[Specification of a main CO₂ Loop]



[Cooling towers – 12MW]

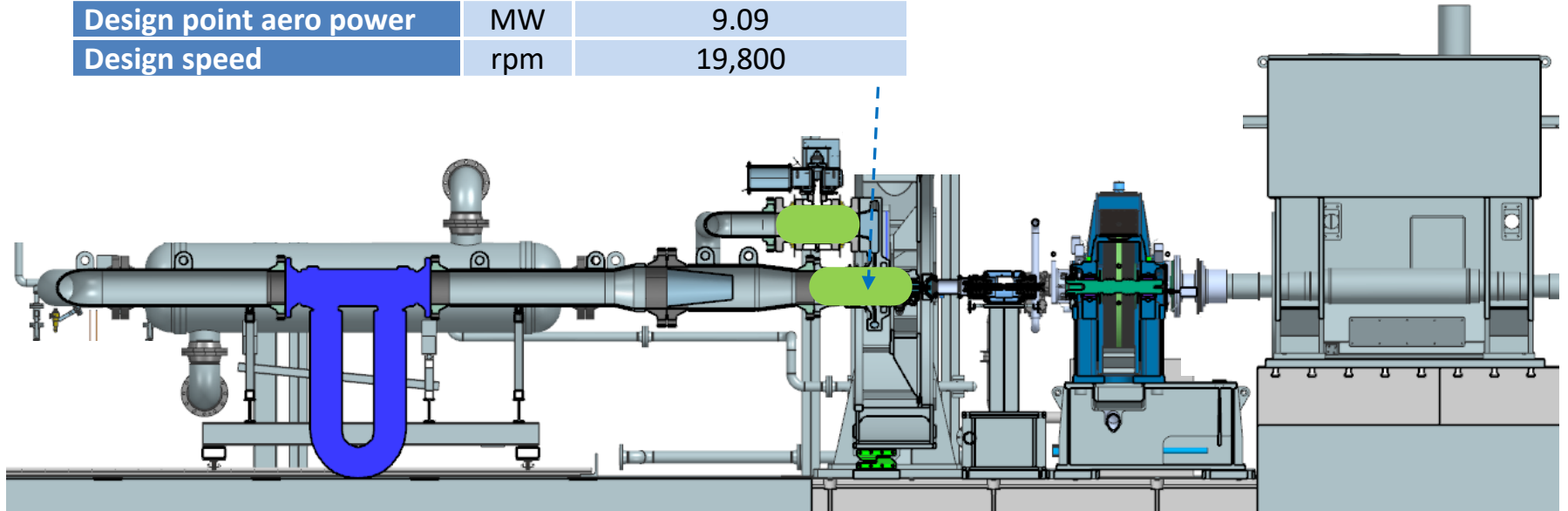
Flowmeter	Type	-	Coriolis
	Size	in	12
	Mass flow rate accuracy	%	0.10
Heat Exchanger	Max. flowrate	kg/s	907
	Type	-	Shell and tube
	Heat Exchange Capacity	MW	10.6



First Compressor to Test

Compressor type		Axial compressor
# of compressor stages	-	1 / 2 / 3
Inlet total pressure	MPa	2.77
Inlet total temperature	°C	97.94
Mass flow rate	kg/s	116
Pressure ratio	-	2.706
Design point aero power	MW	9.09
Design speed	rpm	19,800

- Aerodynamic performance
- Aeromechanic characteristics
- Detail Flow survey



I Development of Advanced High Efficiency **Axial** Compressor

- Aero Design : 90+% (Ha et al., 2022)
- Experimental Evaluation : Current Study