Experience in Manufacturing Pipe and Fittings from INCONEL[®] alloy 740H[®] for **Demonstration Facilities for sCO₂ Service**

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Supercritical CO, **Power Cycles** Symposium

Age-hardened Ni-base alloy initially designed for boiler tube

Creep strength, microstructure stability and hot corrosion resistance

Characterized through many DOE programs **ASME Code Case 2702** (2011)Coal to sCO₂ and Solar Manufacturing capability facilitated through Demos

Reference: ASME Case 2702-8, Sec. 1, Ni-25Cr-20Co Material, UNS N07740, 2023; ASME Case 3056, Sec VIII, 2022.

740H Background





Allowable stress for various alloys

Simulated coal ash corrosion test at 700°C

Synergy between DoE programs

Manufacturing Capabilities and Limits

VIM/ESR, VIM/VAR **Cropped and conditioned ingot weight max** 30,000 lb All mill product forms have been made in commercial quantities Welding products available **Product size limits for forgings, pipes and** fittings are similar to other "hard" nickel alloys such as 625 **Currently product melted to order – long** lead times for fittings Competition with aerospace and oil and gas markets for production capacity **Cost is subject to raw material variability** Numerous nickel alloy mills are capable of making the alloy

Reference: Purgert et al, Materials for Advanced Ultra-Supercritical Steam Turbines, Final Report, https://doi.org/10.2172/1875111

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22" OD x 3.7" W pipe extruded at Wyman-Gordon, **Houston TX**



Largest 740H ingot produced by Special Metals in Huntington WV

Mill and fabricated **Property variability** – Annealed grain si Batch vs continuo – Aging time, temperature 1400-1500°F) **Test orientation** – Cooling rate and Long time static agi **Creep strength conv** Weld strength reduc Gaps: – Fatigue, fracture on components – Environmental eff - Residual propertie

References: Shingledecker, "Improving Economics of Generation 3 CSP System Components...", Final Technical Report, to be published by OSTI; McMurtrey, "Creep-fatigue Behavior and Damage Accumulation of Candidate Materials, Final Technical Report, https://doi.org/10.2172/1797935

Mechanical Properties

products	150
	140
ize (SA ≥ 2010°F) ous erature (4-16 hr	130
	120
	110
	100
	90
auto-aging	0.
Ing	m
vergence?	
ction	
toughness, creep	
fects	
IES	

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.2% YS (ksi) for selected fully heat-treated product forms. ASME nin 90 ksi (Baker)



Creep strength showing weld reduction (Shingledecker)





Cold Worked Tube Seamless tube process - Forged bar, extruded shell 0.90 Seamless 0.80 Welded – Cold drawn or pilgered 0.70 Redrawn .=_0.60 – Continuous or batch anneal *≊*0.50 읔0.40 - Processing similar to alloy 625 0.30 Welded tube 0.20 0.10 – Autogenous welded strip 0.00 - Semi-continuous process Tube OD, in **Cold worked tube sizes made to date** — 30-40% reduction in cost - Direct or redrawn - Weld strength issues Gaps Limited characterization of hoop properties — Min % reduction for redrawn tube

References: Seamless Tube - Purgert, et al. AUSC Final Technical Report, https://www.osti.gov/scitech/biblio/1346714 and Welded Tube - Shingledecker, et al., Final Technical Report OSTI report (XXX)

Seamless and Welded Tube





HX tube with spiral fins The 7th International Supercritical CO₂ Power Cycles • February 21 – 24, 2022 • San Antonio, TX, USA

Welded and redrawn, 0.375" OD x 0.080" W



Seamless HX tube: 0.29" OD x 0.043" W





Seamless pipe process - Extrude as ingot or billet - Condition OD & ID – Heat treat and inspect Welded pipe - Start with annealed plate – Heat treat and inspect - Weld creep strength penalty Gaps large thin-wall pipes Limited property assessment on large pipes

References: Seamless - Purgert et al., AUSC ComTest Final Report, https://doi.org/10.2172/1875111; Welded – Shingledecker...XXX

Seamless and Welded Pipe



Bend and weld using matching filler

Dimensional control and cracking on

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Pipe sizes made to date





Extruded seamless pipe 22" OD x 3.7" W



Small tube cold bends - Similar to alloy 230 or 625 **Pipe induction bends** - Bends made on 4" to 28" OD pipes Process parameter optimization - Good shape response – Surface condition No degradation of properties Gaps Start and stop strain-age cracking during reheating of thin-wall pipes with **OD** > 10" Robust bending model for agehardened alloys

Reference: deBarbadillo et al., Mfg of Large Superalloy Pipe Bends, Superalloy 718 and Derivatives 2023, TMS.

Tube and Pipe Bends

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Start of bending



Steady state bending

0.95 0.9 0.8 0.65 0.6 0.55

Strain-age ID crack at bend stop





Wall thickness around circumference







Small fittings - Flanges, elbows, concentric reducers, wyes, tees, saddles, valve parts – Produced on conventional equipment – Narrow hot working range Large fittings - Few capable forgers Large machining costs Gaps Limited mechanical property testing Long delivery time

Reference: Small fittings – deBarbadillo et al., Development of Fittings Capability for AUSC applications, 8th EPRI Conf, ASM, 2016. Large fittings – Purgert et al. AUSC ComTest Final Technical Report https://doi.org/10.2172/1875111.



Few forge shops with experience

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Hammer forged flange



section



Machined flange

Casting - Experimental, no commercial parts **Cold Forming** Hydroformed tee (two suppliers) - Properties acceptable **HIP Gas Atomized Powder** - DOE FE funded project led by GE R&D - HIP and machined elbow Weld joint porosity acceptable – Low creep strength due to residual **PPB Costing study showed significant** savings Wire and Powder Additive Limited experimental _ No process issues

Reference: Huang et al., Low-cost HIP fabrication of Advanced Power Cycle Components, Final Technical Report, https://doi.org/10.2172/182264

Process Alternatives

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Steps in manufacturing hydroformed tee





Steps in manufacturing 740H HIP elbow





HIP 740H plate successfully welded to wrought 740H plate







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Age hardened Ni-base alloys considered difficult to cut and machine High hardness, work hardening, abrasive, galling, distortion

- Variable hardness in thick section Carbide tools generally required Single point turning tests at TechSolve Inc
- **Tested three heat treated conditions** Kennametal KC5010-RP used on Sph and SA+A bars, Sandvik 1105-SM used on SA bar
- "Spheroidized" condition gave better tool life and lower machining cost compared to SA or SA+A Condition
- **Properties recovered after final heat** treatment

Gaps

Needs validation for complex part with multiple operations

Reference: Adinamis, Appendix to AUSC Final Report, https://doi.org/10.2172/1875111.

Machining











Cost for removal of cubic inch of material vs cutting speed Criterion: 0.030" flank wear The 7th International Supercritical CO₂ Power Cycles • February 21 – 24, 2022 • San Antonio, TX, USA

Cutting test

Hardness of trial bars





Tool life vs cutting speed for 740H in three conditions



740H designed with weldability as key requirement – Nickel alloy welding – Superalloy welding **ASME Case 2702 rules** – **PWHT mandatory** No local solution anneal ____ - GTAW and GMAW only – Weld strength reduction factor Field fabrication experience Welder training, qualification and experience Gaps - Service experience Repair

References: Purgert, et al. AUSC ComTest Final Report, https://doi.org/10.2172/1875111. Gollihue, et al. Practical Guide to Welding INCONEL alloy 740H, Proc. 7th EPRI Conf, ASM, 2013



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GE Power mockup for **AUSC ComTest: Thick-wall girth** welds, socket welds, butt welds, overlays, dissimilar metal welds

Strain-age (SRC) cracking - Common in age-hardened alloys – Not limited to welding – Short term and long term **Experience with 740H in STEP Heater** Weld cracks found in pressure testing – 3% of 1300 welds required repair Metallographic evidence of SRC ____ Lehigh U testing identified critical variables **Guidelines for successful welding** Gaps Many variables, no model ____ No single definitive test ____ No long-time service data _____

Reference: Shingledecker, et al., Innovative Method for Welding..., SETO Final Technical Report, 2023, https://doi.org/10.1007/978-3-031-27447

Stress Relief Cracking





3 Weld 20 #2





740H Tensile Test Plots - 800°C



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Recrystallization and precipitatefree zones in SRC region

Mill product forms - Tube, pipe, bar, welding products to commercial orders, sheet & plate demonstrated Size limit capability demonstrated All product to date from alloy developer Capacity competition with aerospace Reprocessing Large pipe extrusions to commercial orders Welded tube and pipe demonstrated Fittings Standard forged fittings capability demonstrated for various parts and vendors Not stocked, currently long lead items Machinability characterized Alternative manufacturing methods need further validation Bends **Capability demonstrated** Some quality issues remain with thin wall induction bends

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Welding Alloy specific procedures developed - Welding guidance documents Weld strength reduction factor, definition beyond base case Guidelines for avoiding stress relief cracking Stress relaxation cracking sensitivity not defined Properties Excellent oxidation/hot corrosion resistance in most environments Nominal tensile properties reproduced in all product forms Limited data base for creep properties in commercial mill products and fabrications Application specific properties on relevant product forms Very limited characterization of service performance and repair Codes & Standards Novelty of age hardened materials Correspondence between ASME sections for enhancements



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740H - 25 Years

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