

Synergy of S-CO₂ Power Cycle and CCS Systems

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ABSTRACT

Supercritical carbon dioxide (S-CO₂) cycles are currently researched for many applications ranging from nuclear energy through geothermal, solar and waste heat recovery systems. One of the major issue of their development is the design of compressor and heat exchangers close to the critical point. In addition, in the real operation carbon dioxide will not be pure and some impurities will be always present. Similar issues are currently faced with the carbon capture and storage (CCS) systems, which are used for the reduction of CO₂ from the flue gas of the fossil fired power plants in order to reduce the global warming. The removed CO₂ can be used for other technology such as extraction of oil or stored. CCS consists of three separate technologies (capture, transport and storage). While CCS technology for reduction of CO₂ from exhaust gas is quite promising there are several drawbacks. Very important are issues related to effect of impurities in the removed CO₂ gas. A similar issue is researched for the pinch point shift within the S-CO₂ cycle heat exchangers. In this case the captured CO₂ is a multiple-component mixture by definition. This paper is focused on the research of CO₂ mixtures and their effect on heat exchangers in the S-CO₂ cycles and the CCS systems. Some other effects on compressor are mentioned as well. The effect of typical impurities in the S-CO₂ cycles (N₂, He, O₂, and Ar) and from the CCS technology (H₂, H₂S, CH₄ and CO) on the heat exchanger size and pressure drop are investigated. It is shown that in most cases mixtures cause an increase of the heat exchanger volume and the increase of the pressure drop. The synergistic research on CO₂ mixtures is important for both technologies. This synergy will bring new interesting findings that will help development of both the CSS system and the S-CO₂ cycles.

INTRODUCTION

The supercritical carbon dioxide (S-CO₂) cycles are recently very perspective and are researched all around the world. They have many applications in many technologies ranging from nuclear energy through geothermal, solar and waste heat recovery systems. Nevertheless, this cycle has several issues. Probably the most important and well known is the existence of the pinch point in heat exchangers, which significantly affects their design. The pinch point is caused by the variations of heat capacity of CO₂ and occurs when the heat capacity of the hot and cold streams (each at a different pressure level) intersect. Due to the pinch point, the heat exchangers may have a large size and low efficiency. However, this point can be removed in several ways. One of them is the addition of small amount of other substance into the pure CO₂. [1]

Furthermore, as it is difficult to use a 100 % pure CO₂ in the S-CO₂ cycles so one may expect about 1% of mole fraction of other substances in it. These impurities are present in working medium and the resulting mixture of CO₂ may lead to the disappearance of the pinch point in the regenerative heat exchanger, on the other hand the impurities have a negative effect on other components such as compressor or cooler [2].

The CCS systems are very perspective for the reduction of CO₂ from the flue gas of the fossil fired power plants. However, the captured CO₂ is a multiple-component mixture with the same negative effect on the CCS system components as in the S-CO₂ cycles. This effect is especially high for the transport and the storage part of the CCS system.

In the CCS systems CO₂ is used in the supercritical state or close to the critical pressure as well as in the case of the S-CO₂ cycles. The reason is the better transport properties of CO₂ mainly the high density. The transport parameters depend on the phase of CO₂ [3]. It can be done in the gas phase or in the liquid phase. For the gas phase the transport pressure is about 15 MPa (depending on the storage, the transport line and the utilization). The liquid phase has a typical transport pressure of about 6.5 MPa. [3]

A compressor station is used to achieve the required transport pressure. Coolers cool down CO₂ to the required transport temperature which can be below 0°C (liquid phase). Hence problems with mixtures in the S-CO₂ cycles are quite the same as for the transport of CO₂. A full understanding of the effect of mixtures on heat exchangers and compressors is necessary.

A very interesting possibility is to use CO₂ from storage as a working medium in the S-CO₂ cycles or in other systems which use CO₂ as a working medium. However, mixtures from capture will probably have a negative effect on the cycle efficiency. Operating costs will be decreased if transport of pure CO₂ is problematic and CCS system is operated near the cycle. Mixture from CCS will reduce operating cost. Other way is the implementation of the S-CO₂ cycles in the compressor stations or other parts of the CCS systems as cycles for waste heat recovery.

This paper is focused on the research of CO₂ mixtures and their effect on heat exchangers in the S-CO₂ cycles and the CCS systems.

THE DESCRIPTION OF THE S-CO₂ CYCLE

The S-CO₂ cycle is a gas cycle developed from the Ericsson-Brayton cycle, which offers many different layouts. The basic layouts are. [4].

- Simple Brayton cycle
- Re-compression cycle
- Pre-compression cycle
- Split expansion cycle
- Partial cooling cycle

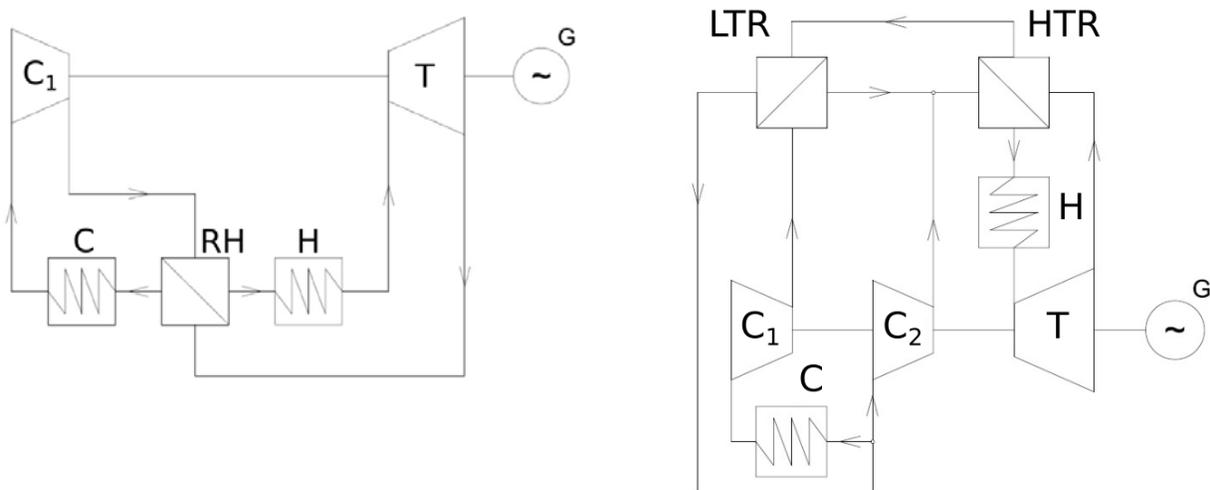


Figure 1.: Simple Brayton cycle (a) and re-compression cycle (b) layout

These cycles were described already in the second half of the 20th century [5]. There are many other layouts of these cycles for solar, geothermal power plant and waste heat recovery. The main advantages of the S-CO₂ cycles are that they are simpler and more compact compared to the Rankine-Clausius cycle. Hence, the S-CO₂ cycles are likely to have lower costs, shorter construction period and shorter commissioning period. These benefits come from the properties of CO₂. On the other hand, properties of CO₂ have a negative effect on some components and they affect the behavior of the cycle and the cycle efficiency.

The simple Brayton cycle and the recompression cycle are shown in Figure 1. These cycles have a turbine (T), one or two compressors (C1 and C2), recuperative heat exchanger(s) (RH or LTR and HTR), a cooler (C) and a heater (H).

THE DESCRIPTION OF THE CCS TECHNOLOGY

The CCS technologies are used to capture CO₂ from flue gas of the fossil fired power stations, transport it and store it on a selected place. The system first captures CO₂ from flue gas. The capture can be done by three basic methods: the pre-combustion method, the post-combustion method and the oxy-fuel combustion.

The capture of CO₂ in the pre-combustion method is done before the combustion and it is a part of fuel gasification. The capture in the post combustion method is simple for construction, because capture is done after combustion. Thus, this capture system can be built at the existing fossil power plants. In the oxy-fuel combustion the fuel is combusted with pure O₂ and with subsequently CO₂ captured. Capture of CO₂ can be done for cement, concrete, iron and steel industry as well. [3]

Other part of the CCS technology is the transport of CO₂. In this part CO₂ is transported to the specific place, where it is prepared for storage or for injection to the oil fields. The transport is selected according to the place of storage or according to the future use and based on the amount of CO₂ which is captured. Currently, the transport can be done in liquid or gaseous phase. The transport of the gaseous phase is done through pipeline. The pipeline can be used for both type of storage. The transport of liquid phase is done through tanks for CO₂ or by ship, train or truck according to the type of the storage method. The transport parameters of CO₂ are different for the gaseous phase and for the liquid phase. A compression station is used for the pipeline transport for the transport by tanks. Pipelines operates from 8.6 to 20 MPa with the ambient temperature from 4 °C to 38° C [3]. Booster stations must be used for the pipeline transport because of the pressure drop along the pipeline. The number of the booster stations depends on the length of the pipeline. The compression station for a pipeline is shown in Figure 2.

The transport pressure for liquid CO₂ is in the range from 0.52 MPa up to 7.3 MPa [3]. The most common parameters are pressure of 0.65 MPa and the temperature of about -50 °C [6]. A compression station for the transportation of liquid phase of CO₂ is shown in Figure 3. The storage can be done onshore or offshore. The transport for an onshore storage can be done with a pipeline or tanks. It is the same as for liquid. Type of transport depends on the distance between the capture and the storage sites.

The mixtures of CO₂ from capture differ based on the separation method of CO₂ and the type of industry on which the CCS system is employed. The basic components of mixture from capture are N₂, O₂, CO, Ar, H₂S, H₂ and H₂O. An example of mixture of CO₂ for transport in pipelines is shown in Table 1.

Table 1. CO₂ quality recommendation for pipeline transport [1].

Component	H ₂ O	H ₂ S	CO	CH ₄	N ₂	O ₂	Ar	H ₂	CO ₂
	Ppm	Ppm	Ppm	vol.%*	vol.%*	vol.%*	vol.%*	vol.%*	%
Concentration	500	200	2000	< 4	< 4	-	< 4	< 4	>95.5%
*all non-condensable gases									

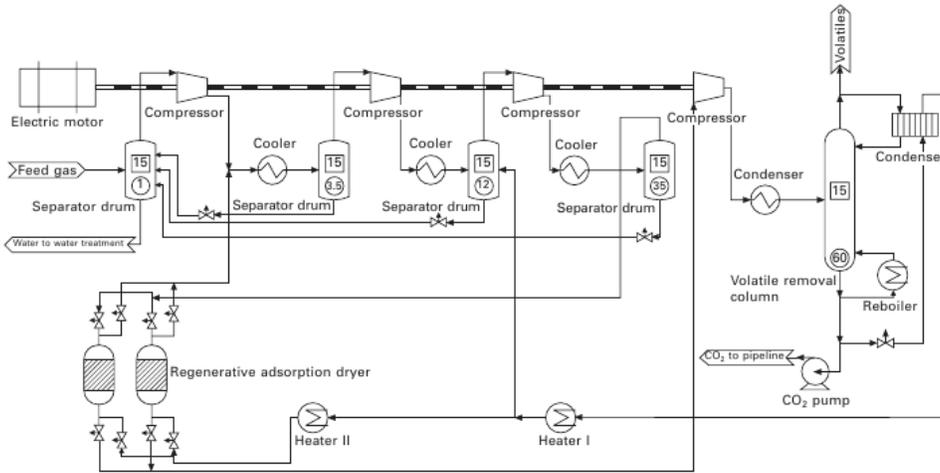


Figure 2.: Compression station for pipeline [3].

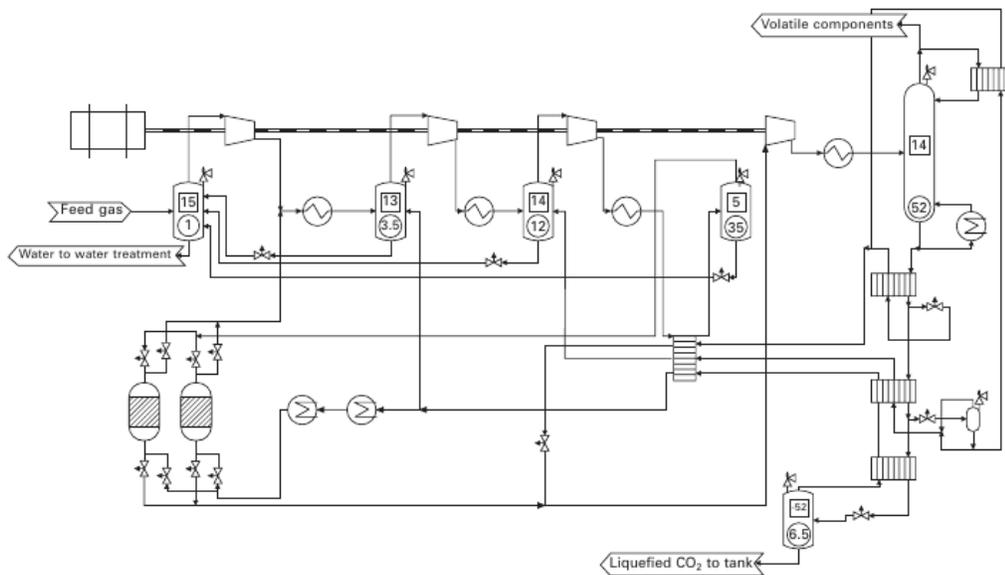


Figure 3.: Compression station for transport of liquid phase of CO₂ [3]

THE DESCRIPTION OF CO₂ PROPERTIES

Carbon dioxide is a triatomic molecule. CO₂ is gas at ambient conditions. The temperature of sublimation is -78.51 °C, the melting point temperature is -56.6 °C for pressure 518 kPa. The critical temperature is 30.98 °C and the critical pressure is 7.38 MPa. The critical density is 464 kg/m³. In the area near the critical point abrupt changes of density even for small temperature change occur. At the critical point the density of the gaseous and the liquid phase are equal.

These property changes affect the behavior of each component of systems with S-CO₂. The effect can be both negative or positive. In the case of compression near critical point the property changes have a positive effect on the compression (i.e. the reduction of the compressor work). The negative effect appears in a heat exchanger. According to pressures in the heat exchanger the pinch point may occur. The pinch point means the minimum temperature gradient in a heat exchanger. This problem is especially pronounced for heat exchangers with S-CO₂ on hot and cold side close to the critical temperature. For the recuperative heat exchanger, the zero temperature gradient may appear and the transfer of heat is stopped. This problem is caused by the variations of heat capacity of CO₂. Previous research shows that from the known heat capacity for hot and cold side. The location of the pinch point can be defined [1]. Figure 4 shows the temperature of the pinch point according to the pressure of hot and cold side of the heat exchanger. The pinch point can be removed with gaseous minor constituents which are injected in to the pure CO₂. However, this will introduce a negative effect on other components, they mainly the compressor work will increase.

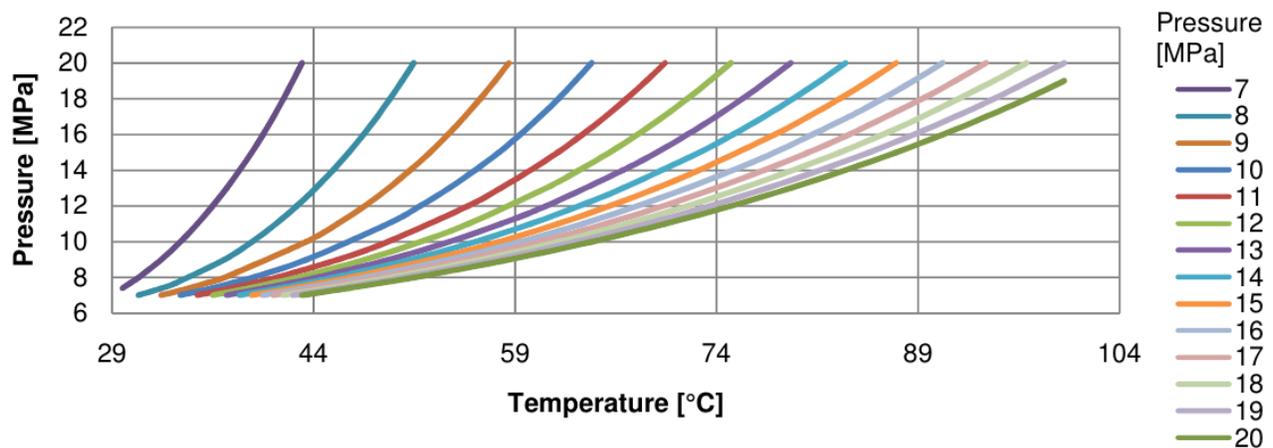


Figure 4.: Dependence of the pinch point location on the temperature and pressure [1]

CO₂ FROM THE CCS TECHNOLOGIES

CO₂ from CCS technology has a different quality of mixture according to the capture process and the system where the capture is done. The mixtures are different and depend on capture technology. Table 2 shows the mixtures for the pre-combustion, the post-combustion and the oxy-fuel combustion. CO₂ from capture is a multiple-component mixture with the same negative effect on components in the CCS systems as in the S-CO₂ cycle. These effects are important mainly for the transport and the storage. So the above mentioned problems with mixtures in S-CO₂ cycles are quite the same for the transport of CO₂ in the CCS systems. A full understanding of the effects of mixtures on heat exchangers and compressors is thus necessary.

It was shown that the CCS systems and the S-CO₂ cycles have the same issues. The possibility to use CO₂ from capture as a working medium in the S-CO₂ cycles or in other systems which use CO₂ as a working medium is very interesting. However, the mixtures will probably have a negative effect on the cycle efficiency, even if the cycle will be operated near the transport line or the capture and storage site. The S-CO₂ cycles can be implemented in compression stations or in other parts of the CCS systems as a cycle for waste heat recovery [7]. The mixtures from the CCS systems thus might decrease the cost of the cycle.

According to the Table 2 it is obvious that the fraction of CO₂ is more than 95 % and the concentration of impurities is less than 5 %. From previous research it is known that the effect of mixtures on a heat exchanger is quite small for 1 % of mole fraction of other substance [2]. Table 3 shows this effect for a cooler. Results from Table 3 are for the shell and tube heat exchanger.

The gaseous mixtures have an effect on the design, the heat transfer and the pressure drops. Figure 5 shows the effect of mixtures on the pressure drops for different binary mixtures. The primary medium is CO₂ and mixtures of CO₂; the cooling medium is water. The parameters for the calculation are shown in Table 4.

The heat exchanger is a single pass shell and tube heat exchanger in the counter current flow arrangement. The outer casing consists of a high pressure casing with the dimensions of 120 x 10 mm. Inside the high pressure tube there is a set of 37 tubes, each with the dimensions of 10 x 1.5 mm.

Table 2. Mixtures of CO₂ for different capture technology [8].

Table 3. Total length of cooler for mole fraction 0.01 and 0.05. [2]

Mole fraction	0.01	0.05	[-]
Pure CO ₂	2.33		[m]
CO ₂ with He	2.60	4.91	
CO ₂ with Ar	2.44	3.17	
CO ₂ with CO	2.52	3.65	
CO ₂ with O ₂	2.49	3.49	
CO ₂ with N ₂	2.51	3.45	

Table 4. Main parameters of the cooler.

Mass flow of side with CO ₂	2.5	[kg/s]
Mass flow of side with H ₂ O	2	[kg/s]
Inlet temperature of side with CO ₂	60	[°C]
Outlet temperature of side with CO ₂	32	[°C]
Inlet temperature of side with H ₂ O	25	[°C]
Pressure of side with CO ₂	12	[MPa]
Pressure of side with H ₂ O	1.5	[MPa]

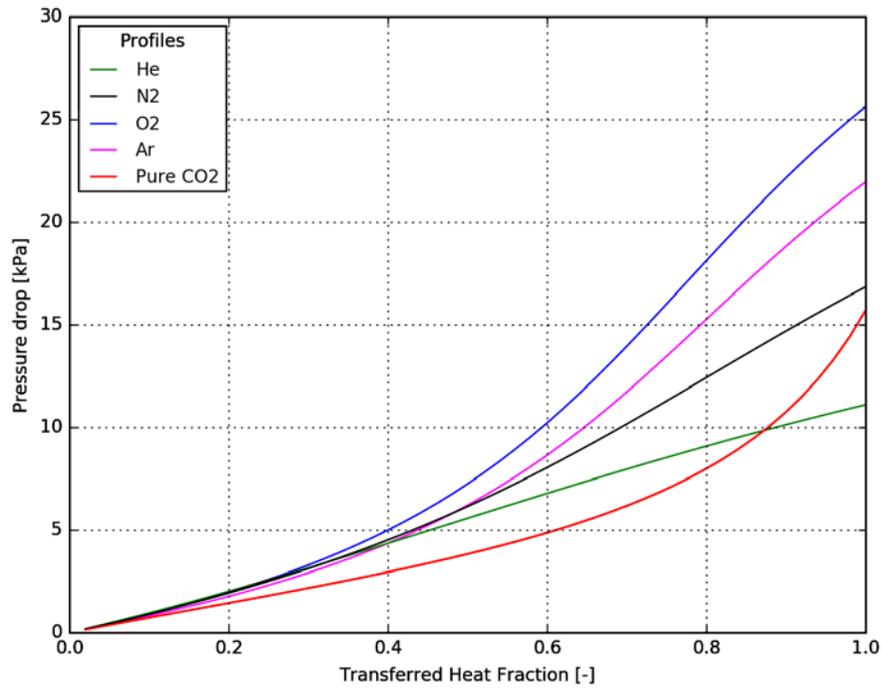


Figure 5.: Pressure drops for mixtures of CO₂ (CO₂ with He, N₂, O₂, Ar)

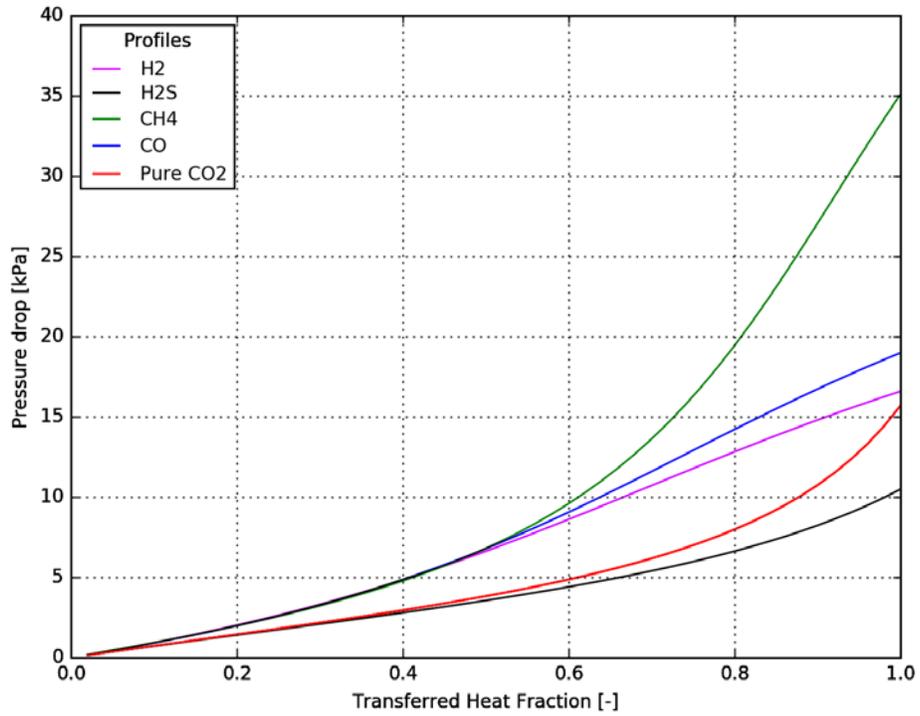


Figure 6.: Pressure drops for mixture of CO₂ (CO₂ with H₂, H₂S, CH₄, CO)

The used gases are N₂, He, O₂, and Ar. These gases are the typical impurities in the S-CO₂ cycle. They have a positive effect on the shift of the pinch point. On the other hand, they have a negative effect on the heat transfer and the total length. According to the Table 3 this effect is significant. According to the Figure 5 it is obvious that the used mixtures increase the pressure drop except for helium.

The similar results can be seen for other mixtures. Figure 6 shows the pressure drops for other binary mixtures with H₂, H₂S, CH₄ and CO. These are the typical components of mixture of CO₂ from the capture technology. Figure 6 shows similar result as Figure 5. It can be seen that all mixtures except the mixture of CO₂ - H₂S increase the pressure drop.

Multicomponent mixtures will likely have a similar effect as the binary mixtures. However, the trend will be probably different. Research of multicomponent mixture is necessary for both CCS systems and the S-CO₂ cycles and will be done in the future.

SUMMARY AND CONCLUSIONS

It was shown that the CCS systems and the S-CO₂ cycles suffer from the same issues when impurities are mixed with the pure CO₂. These impurities are always present in the captured CO₂ and to some extent are present in the S-CO₂ cycles as well. The mole fraction of mixtures depends on the separation system and on the source of CO₂.

The CCS technology, especially its transport part, consists of similar components (heat exchangers and compressors) as the S-CO₂ cycles. Although the design of compressors for the CCS system transport part is slightly different than that for the S-CO₂ cycles, the effect of mixtures on compression is similar. Shift of critical point is possible, but with a negative effect on the compression near the critical point.

The mixtures can be used to remove the pinch point, but in most cases their use leads to the reduced heat transfer, which results in larger heat exchangers with higher pressure drop. So far only the binary mixtures were researched, but similar behavior is expected for the multicomponent mixtures. This research will be done in the future.

Research of the effect of mixtures on the heat exchangers and compressors is one type of the S-CO₂ cycle and the CCS system synergy. Mixtures in the CCS technology and the S-CO₂ cycles are primarily considered as impurities. However, same gases can be injected into the pure CO₂ on purpose in order to shift the pinch point. Other type of synergy is the use of CO₂ as a working medium in the S-CO₂ cycles in the compressor stations or other part of the CCS system as a cycle for waste heat recovery. Implementation of the S-CO₂ cycles to the CCS systems is very interesting and has a good perspective for the future systems. CO₂ from capture can be used as a working medium, thus reducing issues with CO₂ storage and transport. Therefore, the synergistic research on CO₂ mixtures is important. Synergy of research for both technologies, the CCS system and the S-CO₂ cycles, will bring new interesting findings that will help development of both the CSS system and the S-CO₂ cycles.

NOMENCLATURE

CO ₂	=	Carbon dioxide
Ar	=	Argon
He	=	Helium
N ₂	=	Nitrogen
O ₂	=	Oxygen
CCS	=	Carbon capture and storage
CO	=	Carbon monoxide

H₂ = Hydrogen
H₂S = Hydrogen Sulfide
CH₄ = Methane

REFERENCES

- [1] Vesely L., Dostal V., Research on the Effect of the Pinch Point Shift in Cycles with Supercritical Carbon Dioxide. The 4th International Symposium - Supercritical CO₂ Power Cycles: 2014.
- [2] Vesely L., Dostal V, Bartos O., Novotny V., Pinch Point Analysis of Heat Exchangers for Supercritical Carbon Dioxide with Gaseous Admixtures in CCS Systems, 2015: The 8th Trondheim Conference on CO₂ Capture, Transport and Storage, Energy Procedia.
- [3] Maroto-Valer M. M., Developments and innovation in carbon dioxide (CO₂) capture and storage technology Volume 1: Carbon dioxide (CO₂) capture, transport and industrial applications, Woodhead Publishing Limited, 2010, ISBN 978-1-84569-533-0
- [4] Dostal J., Dostal V., 2010, Advanced optimization of thermal cycles with supercritical carbon dioxide, Prague: CTU Department of Fluid Mechanics and Energy.
- [5] Angelino G., Carbon Dioxide Condensation Cycles for Power Production, 1968: ASME Paper No. 68-GT-23.
- [6] Roussanaly S, Jakobsen J.P., Hognes E.H. , Amy L. Brunsvold A.L., Benchmarking of CO₂ transport technologies: Part I-Onshore pipeline and shipping between two onshore areas, 2013: International Journal of Greenhouse gas control.
- [7] Yann Le Moullec, 2012 Conceptual study of a high efficiency coal-fired power plant with CO₂ capture using a supercritical CO₂ Brayton cycle, Department of Fluid Dynamics, Power Generation and Environment.
- [8] Brown S., Martynova S., Mahgerefteha M., CO₂ QUEST: Techno-economic assessment of CO₂ quality effect on its storage and transport, 2014: GHGT – 12, Energy Procedia.