

Oxy-Combustion Flame Fundamentals for Supercritical CO₂ Power Cycles



Pete Strakey, NETL

6th International Supercritical CO₂ Power Cycles Symposium, March 27-29, 2018, Pittsburgh, PA



Outline



- Effects of pressure and diluents on flames.
- Identification of target conditions.
- Overview of characteristic time and length scales.
- CFD simulations of turbulent time and length scales.
- Chemical kinetic mechanisms.
- LES simulations with varying O_2 concentrations.

Effect of Pressure on Laminar Flame Speed



- Cantera with GRI 3.0 used to calculate premixed laminar flame speed.
- Flame speed with 31%O₂/69%CO₂ lower than air mainly due to lower diffusivity.

$$S_L \propto \sqrt{RR \cdot D}$$

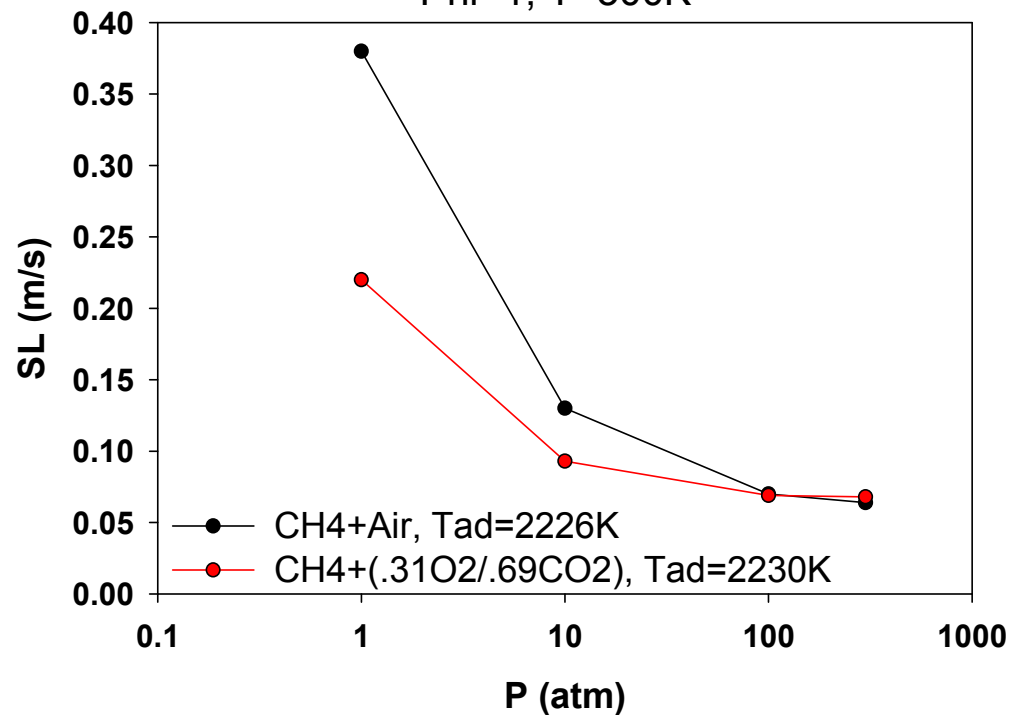
RR= Reaction Rate

$$D \propto 1/p$$

D= Molecular Diffusivity

- Overall reaction order for CH₄/O₂/CO₂ is ~ 1.4

Laminar Flame Speed
Cantera, GRI 3.0
Phi=1, T=300K

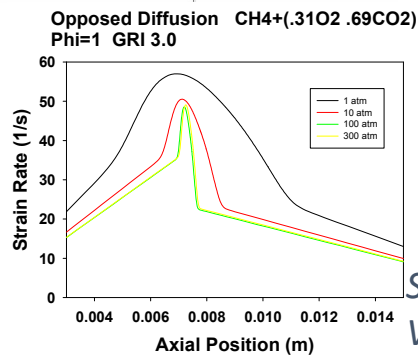
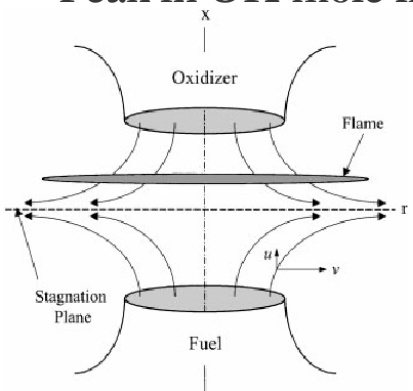


Cantera Non-Premixed Laminar Flame Profiles

- Temperature and OH profiles through flame region.
- Flame thins due to decrease in α being faster than decrease in S_L .
- Peak in OH mole fraction decreases due to three-body recombination reactions.

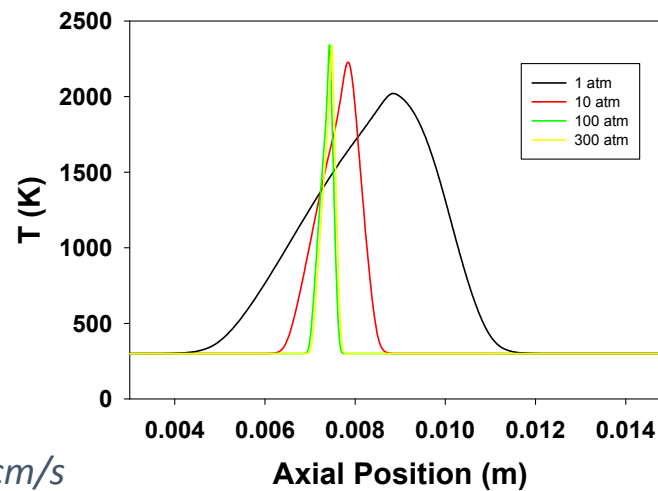
Laminar Flame Thickness

$$\delta_L = \frac{\alpha}{S_L} \quad \alpha = k/\rho C_p$$

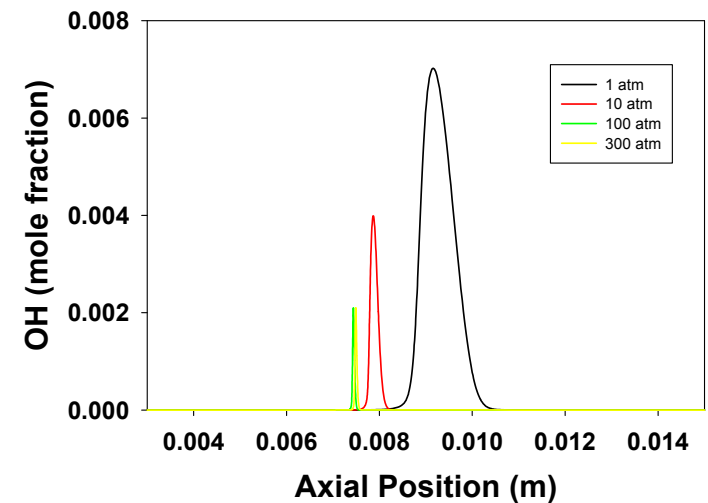


Sep= 2cm
 $V_F=V_O=27$ cm/s

Opposed Diffusion CH₄+(.31O₂ .69CO₂)
Phi=1 GRI 3.0

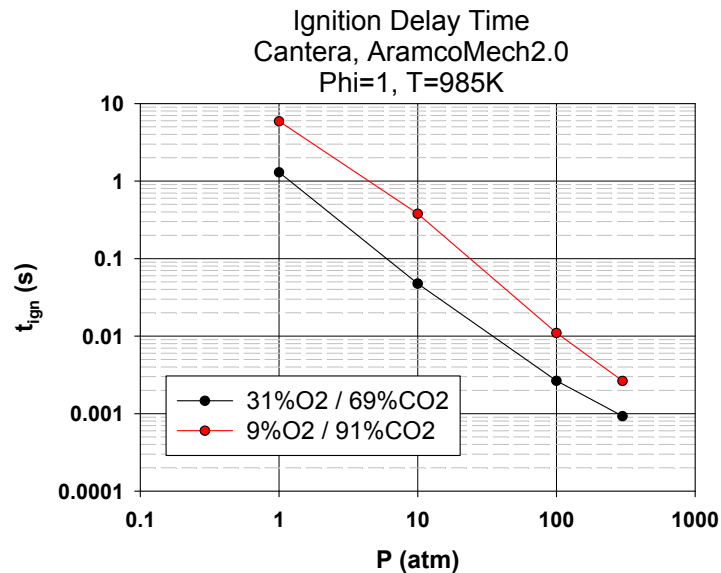
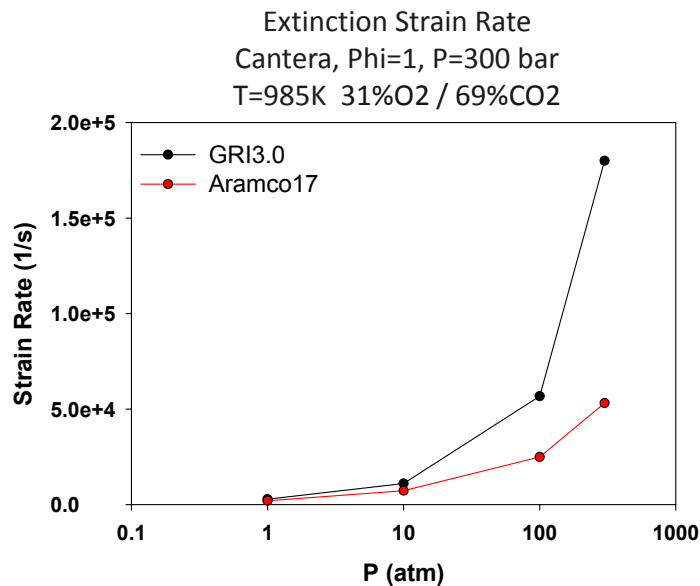


Opposed Diffusion CH₄+(.31O₂ .69CO₂)
Phi=1 GRI 3.0



Extinction Strain Rate & Ignition Delay Time

- Extinction strain rate increases with pressure due to flame thinning. Higher strain rate equates to higher turbulence at quenching.
- Significant discrepancy between GRI 3.0 and Aramco. GRI predicts faster kinetics.
- Ignition delay time ranges from 1-3 msec at Allam cycle conditions.



Allam Cycle

- Goal is to estimate some characteristic combustion scales for high pressure oxy-fuel flames for direct-fired sCO₂ cycles.
- Target is the Allam cycle conditions (O₂ 15% to 30% molar concentration)*.

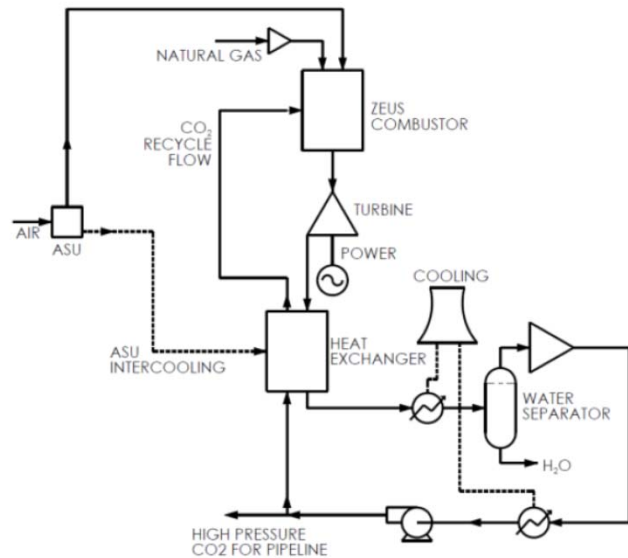


Figure 1. BASIC ALLAM CYCLE NATURAL GAS FLOW DIAGRAM.

Table 1. ALLAM CYCLE KEY POINTS (ISO CONDITIONS)

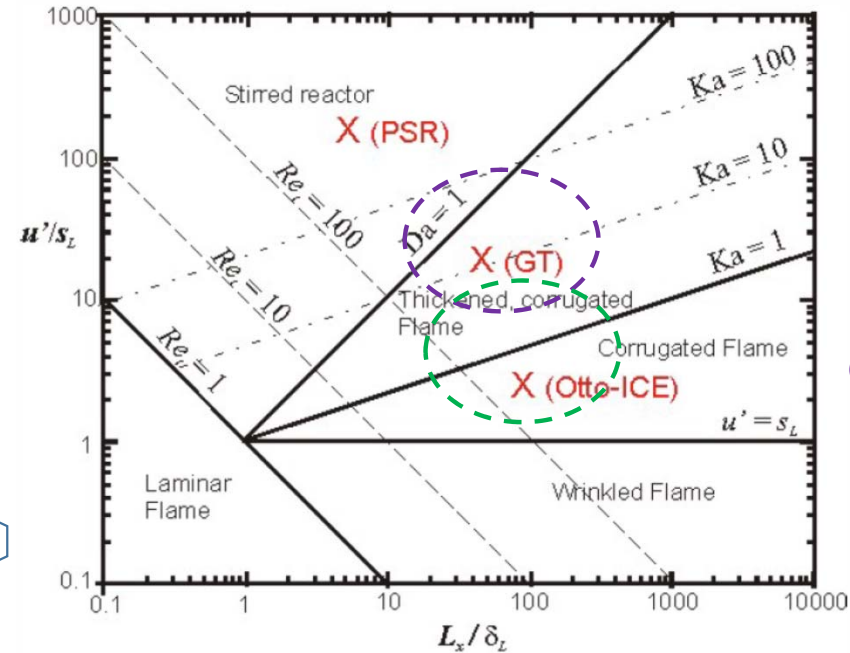
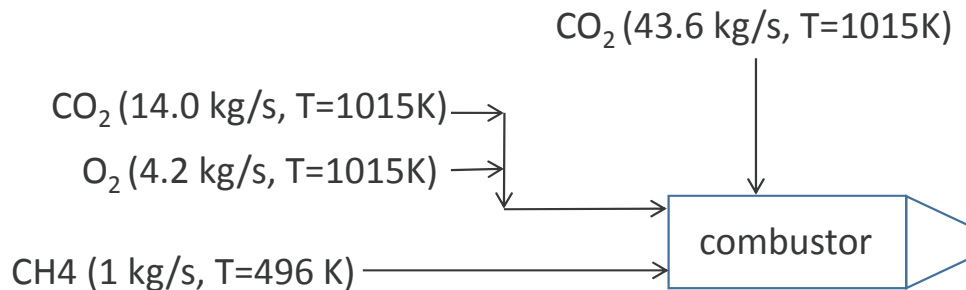
Point	Pressure (Bar)	Temperature (°C)
Turbine Inlet (A)	300	1150
Turbine Outlet (B)	30	775
CO ₂ Compressor Inlet (D)	30	20
CO ₂ Compressor Outlet (E)	80	65
CO ₂ Pump Inlet (F)	80	20
CO ₂ Pump Outlet (G)	300	55
Combustor Inlet (I)	300	750

Borghi Combustion Diagram

- Borghi Diagram indicates regime of combustion (wrinkled flames, corrugated flames, stirred reactor, etc).

need: $\frac{u'}{S_L}$ and $\frac{l_T}{\delta_L}$

$P=300$ bar
 50 MW Thermal Input
 $\Phi=0.95$



Gas Turbines
 IC Engines

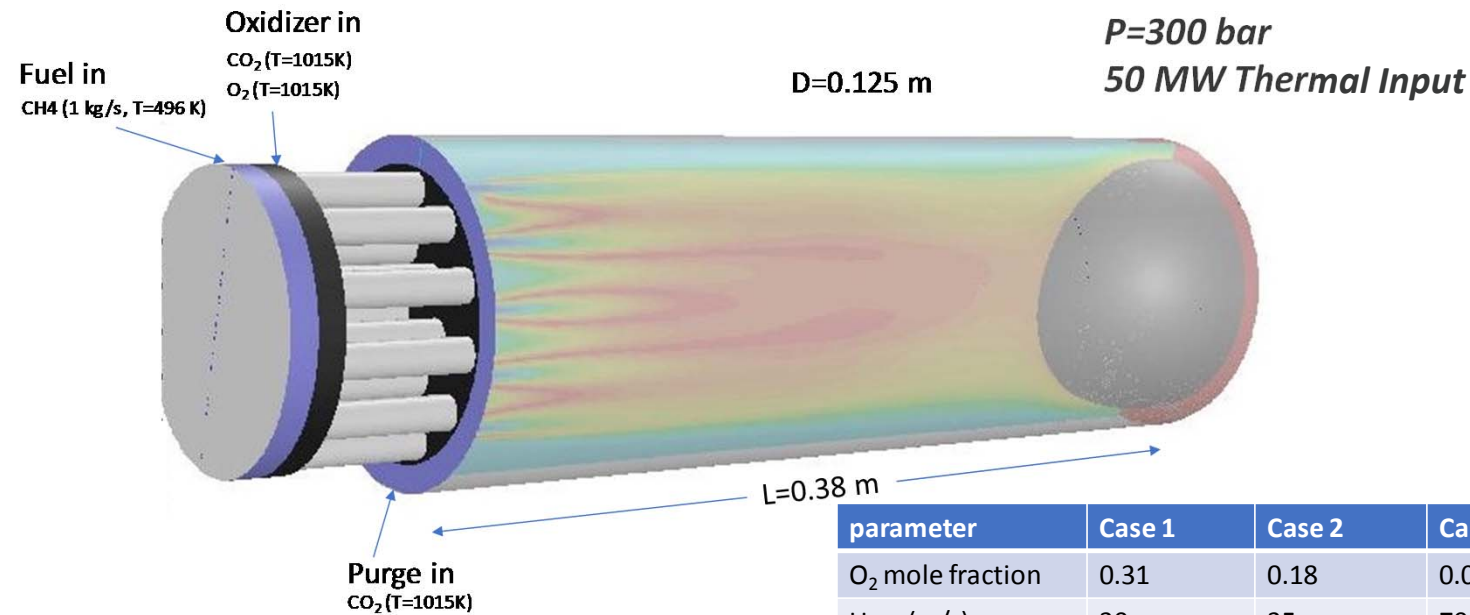
Characteristic Scales and Dimensionless Numbers

- Included here for completeness...

$Ka = \frac{\tau_{chem}}{\tau_K} = \frac{\delta_L^2}{l_K^2}$	Karlovitz Number (chemical time / Kolmogorov time)	<i>K > 1 means the smallest eddies can enter and thicken the flame front</i>
$Da = \frac{\tau_{turb}}{\tau_{chem}} = .247 \left(\frac{k}{\varepsilon}\right) \left(\frac{S_L^2}{\alpha}\right)$	Damkohler Number (turbulent time / chemical time)	<i>Da >> 1 means the chemistry is fast compared to turbulent mixing</i>
$\delta_L = \frac{\alpha}{S_L}$	Laminar flame thickness (thermal diffusivity / laminar flame speed)	
$l_K = \left(\frac{\nu^3}{\varepsilon}\right)^{1/4}$	Kolmogorov length scale (kinematic viscosity / turbulent dissipation rate)	
$l_T = 0.2 \frac{k^{1/2}}{\varepsilon}$	Integral length scale (turbulent kinetic energy / turbulent dissipation rate)	
$u' = \sqrt{\frac{2k}{3}}$	Turbulent fluctuating velocity	

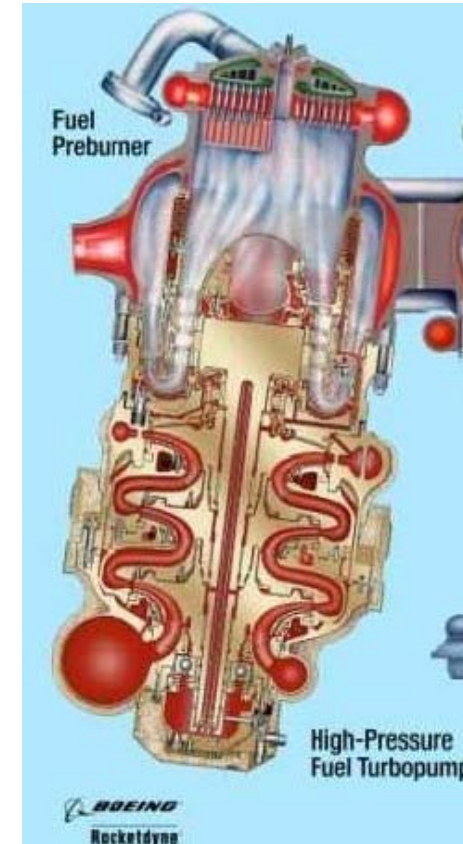
50 MW Conceptual Combustor

SSME Preburner type combustor – 21 coaxial injectors, 4M Cells



- Flow split of CO_2 between injectors and wall purge was varied to produce cases 1 to 3.

parameter	Case 1	Case 2	Case 3
O_2 mole fraction	0.31	0.18	0.09
U_{bulk} (m/s)	30	35	70
l_T (m)	1.9×10^{-3}	2.2×10^{-3}	2.0×10^{-3}
U' (m/s)	7.5	10.7	23.8
S_L (m/s)	0.58	0.082	0.05
τ_{ign} (s)	9.2×10^{-4}	1.6×10^{-3}	2.5×10^{-3}



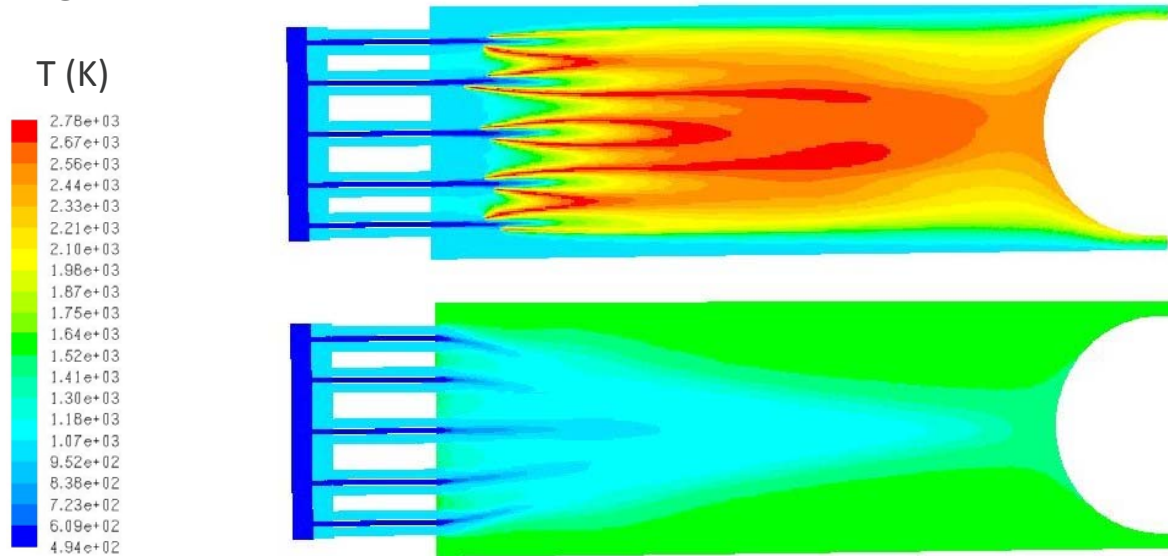
Turbulent Time and Length Scales

Two Limiting Cases:

Case 1: 25% of CO₂ by mass mixed in with O₂
($X_{O_2}=0.31$, $\phi=0.95$)

Case 3: Fully mixed (100% of CO₂ mixed in with O₂)
($X_{O_2}=0.09$, $\phi=0.95$)

*Steady RANS k-e
DRM19 reduced CH₄ mechanism
No Combustion model*



Case 1

25% of CO₂ with O₂ ($X_{O_2}=0.31$)
75% of CO₂ through purge

$l_T=1.9$ mm
 $U'=7.5$ m/s

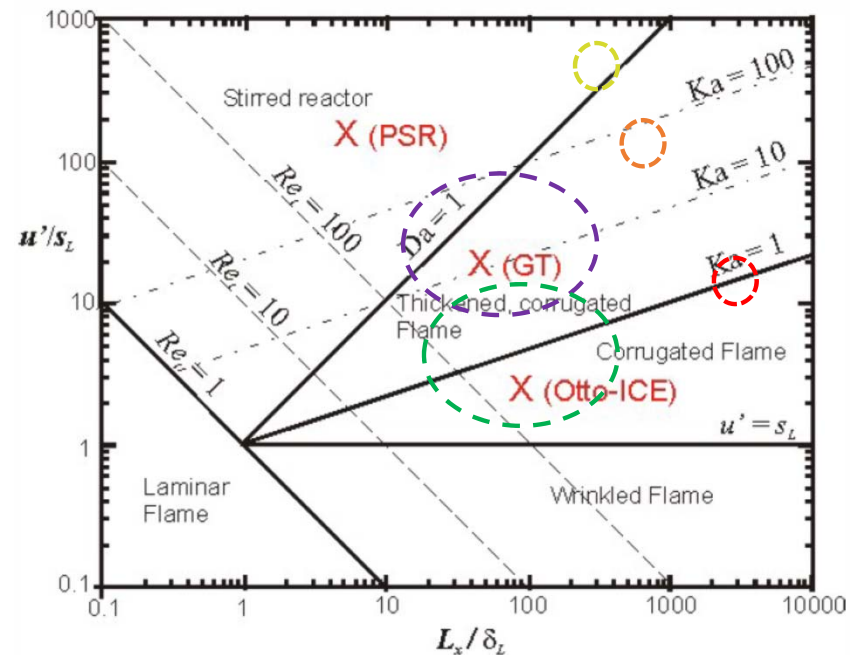
Case 3

100% of CO₂ with O₂ ($X_{O_2}=0.09$)

$l_T=2.0$ mm
 $U'=23.8$ m/s

Borghgi Diagram for Oxy-Combustion

- Three cases shown for 300 bar oxy-combustion define a range of conditions (O_2 from 9-31%) spanning the thickened, corrugated flame regime and stirred reactor.
- Significantly outside the range of gas turbine and IC engine operation.
 - $Re\#$ and/or $Ka\#$ significantly larger than gas turbines or IC engines.
- Requires assessment of appropriate turbulent combustion models.



Gas Turbines
 IC Engines
 sCO₂ 31%O₂
 sCO₂ 18%O₂
 sCO₂ 9%O₂

Chemical Kinetic Mechanisms



- No detailed mechanisms validated at sCO₂ conditions. Best available is likely Aramco Mech (U. Galway). Validated with flame-speed up to 60 bar and ignition delay to 260 bar. Likely better than GRI 3.0.
- Huge mechanism, 103 species, 480 reactions after reduction to C₂ and smaller.
- Need for compact skeletal mechanisms amenable to CFD modeling (10-30 species maximum).

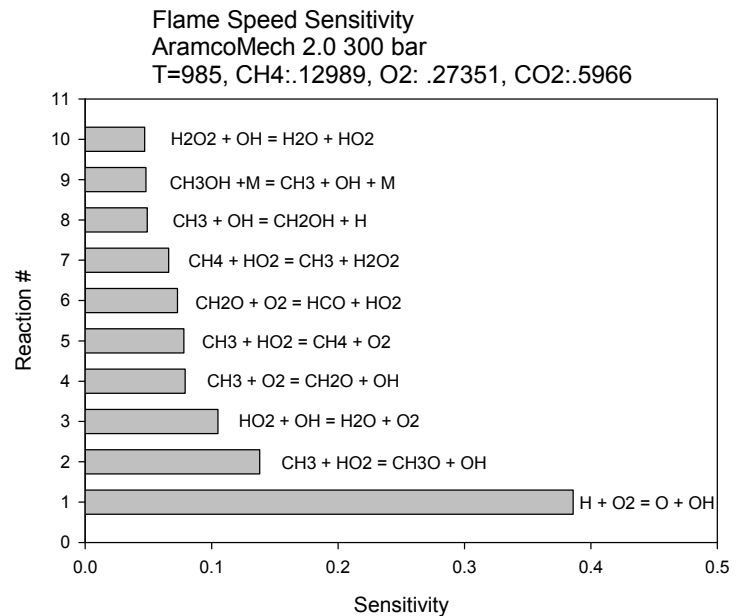
Need flame speed, species profiles and induction time data for direct-fired conditions!

Mechanism Reduction



- Combination of reaction path analysis, flame-speed sensitivity and ignition delay time sensitivity.
- Optimized for Allam cycle combustor conditions
 - 300 bar
 - $T_{\text{preheat}} \sim 1000\text{K}$
 - Oxidizer: 25% O_2 + 75% CO_2
- Several skeletal mechanisms developed with 33, 29, 26 and 17 species.

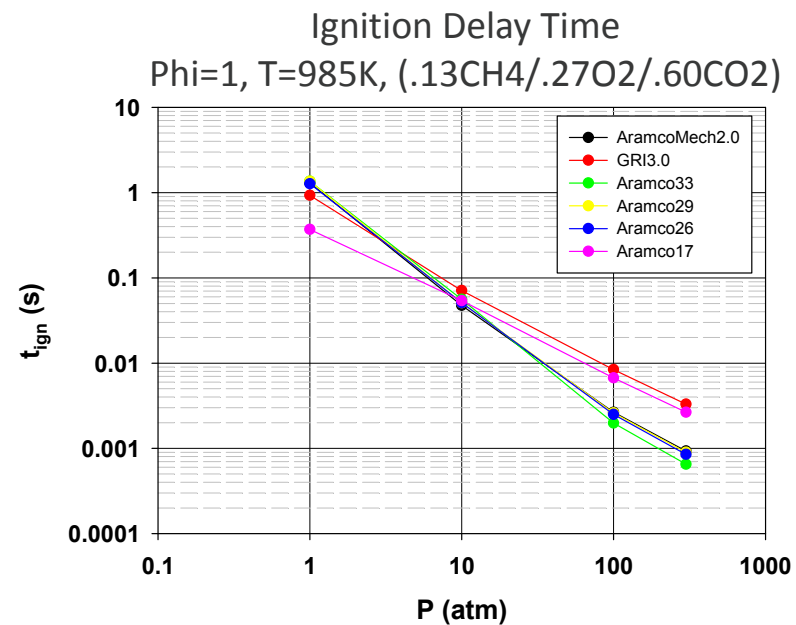
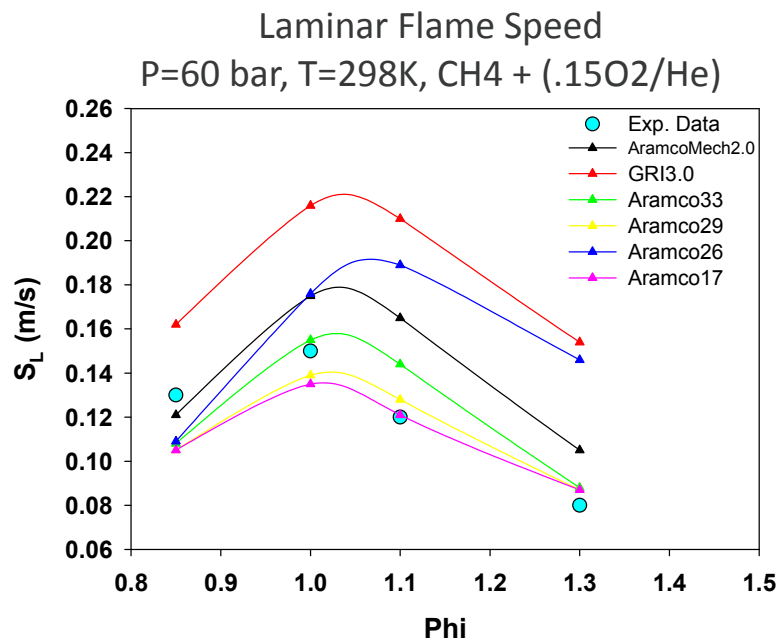
Flame speed sensitivity at 300 bar



Mechanism Reduction

- Performance comparison of various skeletal mechanisms.

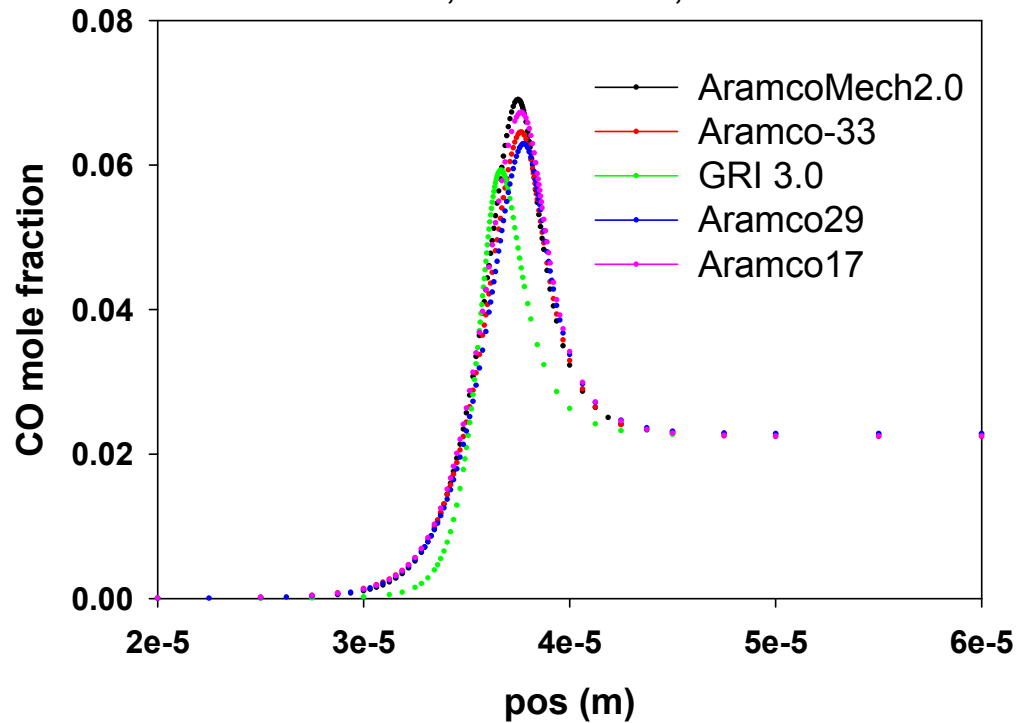
- Flame speed and ignition delay improve with the inclusion of more species and reactions.
 - 33 species mechanism able to predict flame-speed and ignition delay fairly well.
 - 17 species able to predict flame-speed to within ~30% of detailed mechanism.



Mechanism Reduction

- Performance comparison of various skeletal mechanisms.
 - All do very well for CO production profiles.
- CO prediction important for accurate cycle efficiency calculations.

Laminar Flame Profiles
P=300 bar, T=995K
CH4=.12989, O2=.27351, CO2=.5966



LES Modeling: Temperature Contours

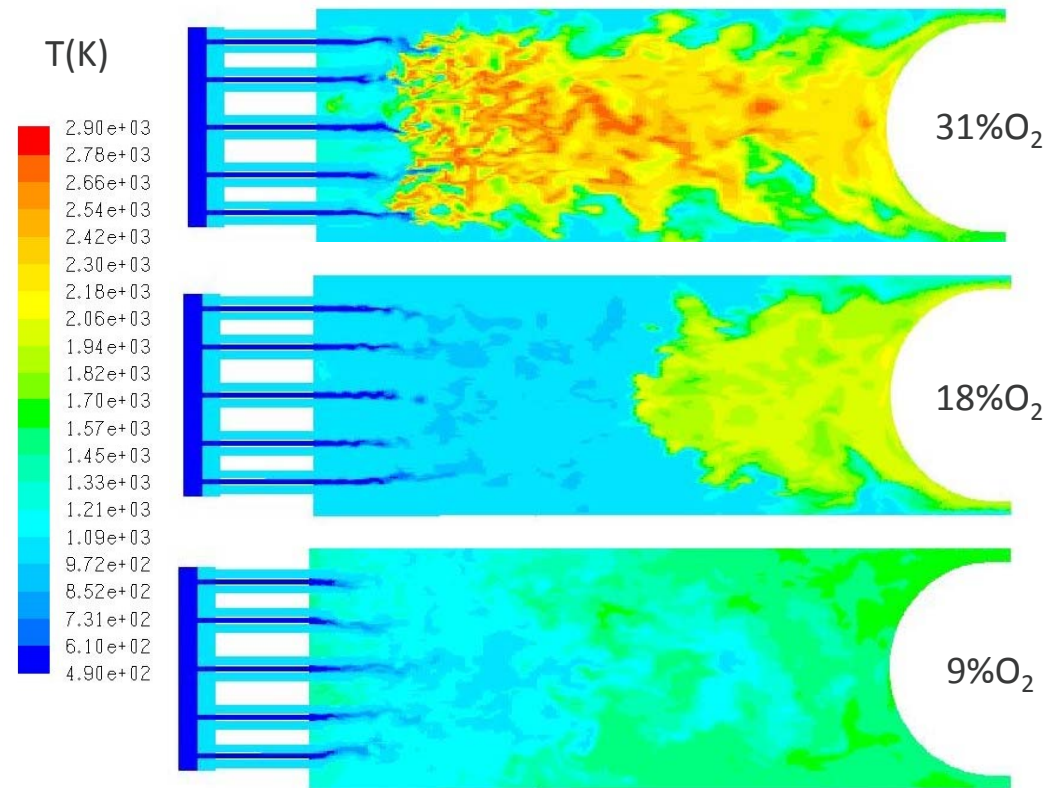
*Large Eddy Simulation, Dynamic k-e transport
17-species skeletal mechanism*

No Combustion Model

Phi=0.95

- Combustor exit temperature is the same for all three cases (~1520 K).
- Combustion transitions from lifted flame to stirred reactor as O₂ is decreased. Consistent with Borghi diagram.
 - Peak temperature decreases (2730 K to 1614 K).
 - Core velocity increases (30 m/s to 70 m/s).

Temperature Snapshots at Quasi-Steady Conditions



LES Modeling: CO Contours

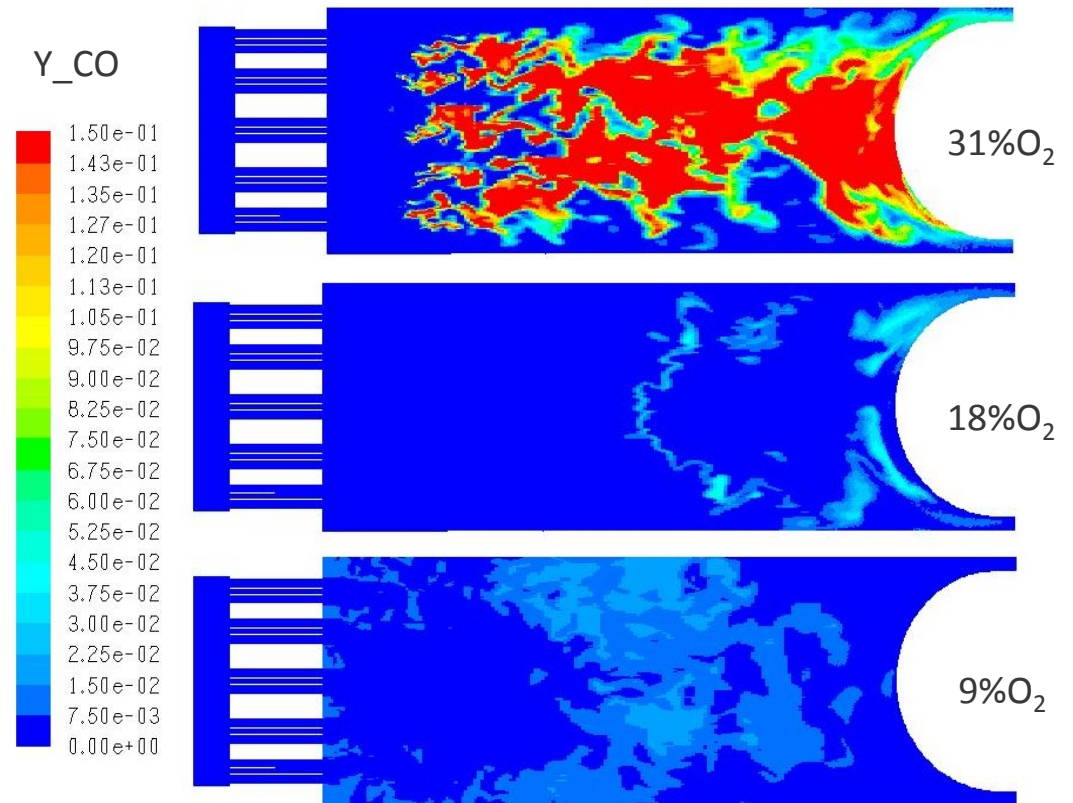
*Large Eddy Simulation, Dynamic k-e transport
17-species skeletal mechanism*

No Combustion Model

Phi=0.95

- Combustor exit temperature is the same for all three cases (1520 K).
- For 31% O₂ case, peak CO concentration well above equilibrium value ($X_{CO}=0.25$).
- For all cases, peak CO is significantly higher than equilibrium.

CO Mass Fraction Snapshots at Quasi-Steady Conditions



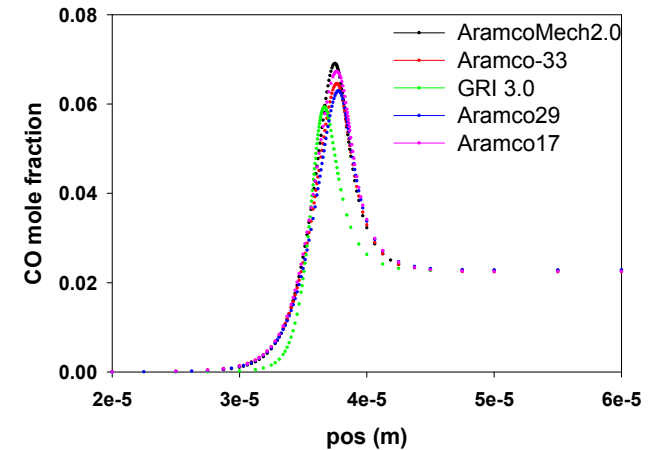
LES Modeling: CO Summary



Case	Oxidizer flow (kg/s)	Purge flow (kg/s)	O2 mole %	Equilibrium Flame Temp(K)	Equilibrium Flame CO mole %	LES Peak Temp(K)	LES Peak CO Mole %	LES Avg CO mole %
1	16.8	43.6	31.0	2690	2.4	2730	25.0	3.5
2	30.4	30.0	18.0	2100	0.15	2060	5.0	1.0
3	60.4	0.0	9.0	1612	0.0018	1614	3.0	0.013

Equilibrium Calcs
 Comb Exit:
T=1612 K
X_{CO} = 0.0018 %

- Peak CO concentrations well above equilibrium levels.
- Average CO concentrations at combustor exit also well above equilibrium levels.
- Cycle efficiency calculations indicate roughly a 0.75 % pt. drop in efficiency per mole % CO in working fluid.



Concluding Remarks



- **Oxy-combustion at 300 bar is somewhat uncharted territory.**
 - Conditions more representative of rocket engines.
 - Limited data available.
- **Need for validated detailed chemical kinetic mechanisms as well as reduced mechanisms.**
- **Must take care in selecting appropriate combustion models (fast mixing, flamelet, EDC, PDF, etc...).**
- **CO production highly sensitive to flame temperature and may be well above equilibrium.**