

# University R & D Session

## KAIST Activities

2016. 3. 30

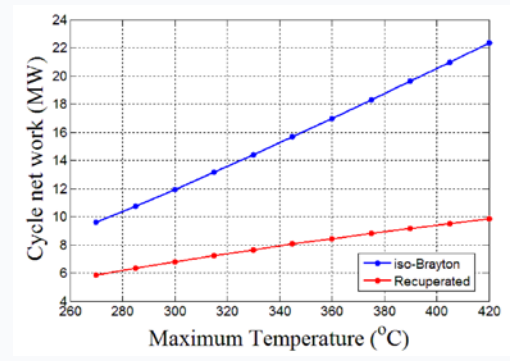
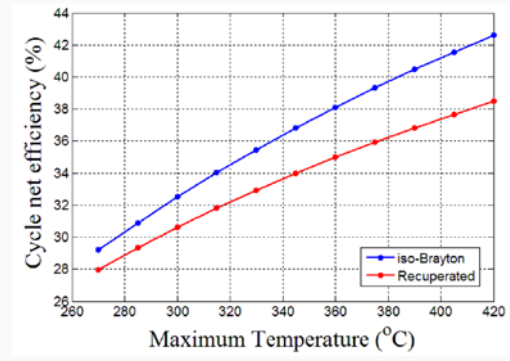
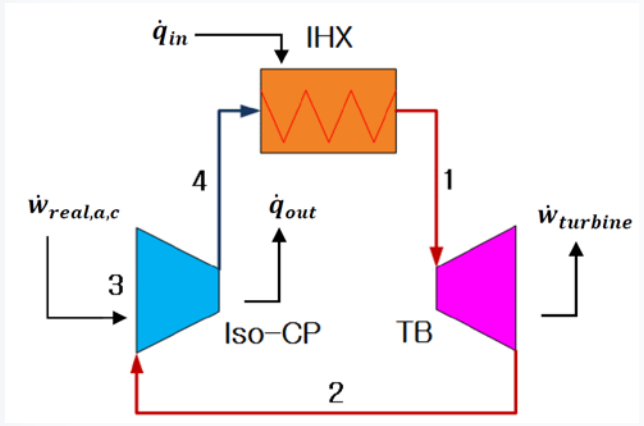
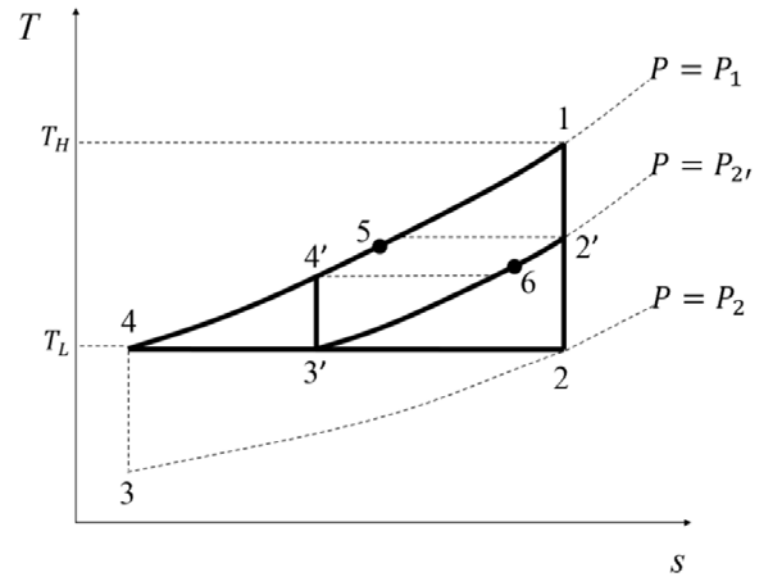
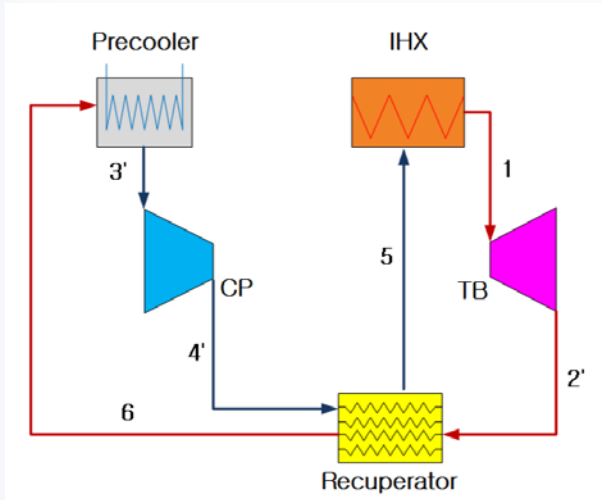
Jeong IK Lee

Associate Professor  
Dept. of Nuclear & Quantum Engineering, KAIST

# Issues Studied in KAIST

- **Larger power system requires higher specific power**
- **Advanced turbomachinery and heat exchanger design and analysis methodologies**
- **New type of components or systems**
- **Transient analysis (Startup, Shutdown, Incidents...)**
- **Specific Technical Issues to Specific Heat Source**
- **Critical Flow and Phase Change**
- **Materials**

# Increasing Specific Power

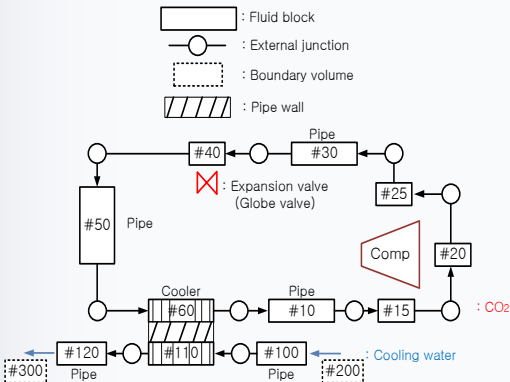
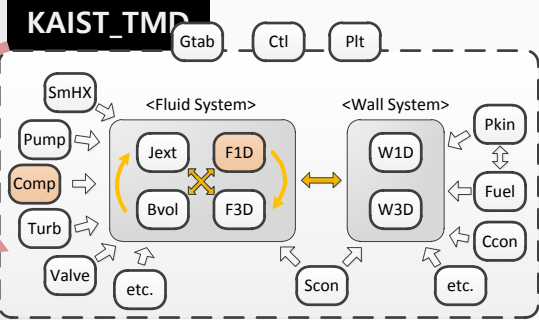


Calculated values	Recuperated	iso-Brayton
Heat (MW)	49.8	49.8
Effectiveness (%)	95.7	90
Volume (m <sup>3</sup> )	3.34	1.17
UA (MW/K)	1.99	0.48
CO <sub>2</sub> mass flow rate (kg/s)	194.75	86.07

# Turbomachinery Design & Analysis

## Transient analysis

- ✓ Turbomachinery performance maps support transient analysis for abnormal system operation scenarios

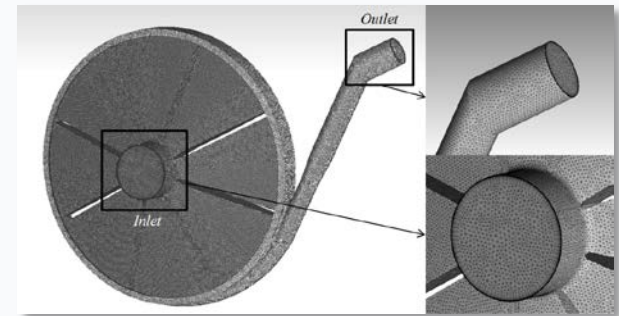
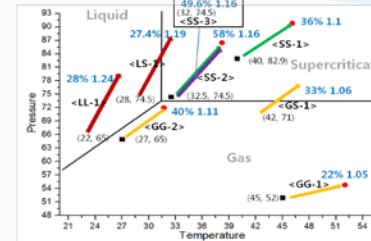
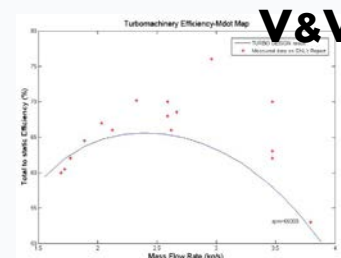
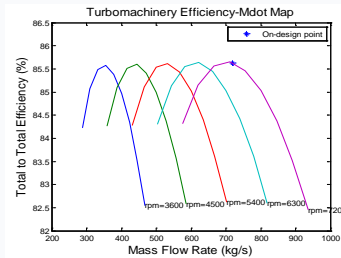


## KAIST\_TMD - 1D Meanline Analysis -

$$\dot{m} = \rho(T_i, P_i)AV$$

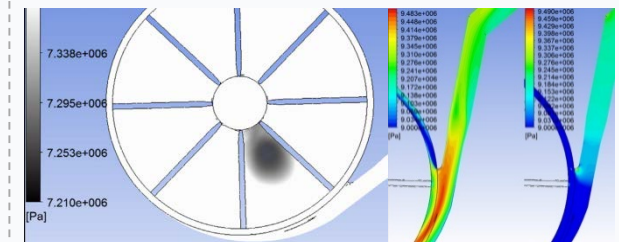
$$h_0 = h_i + \frac{V^2}{2}$$

$$P_i(h_i, s) \quad T_i(h_i, s)$$



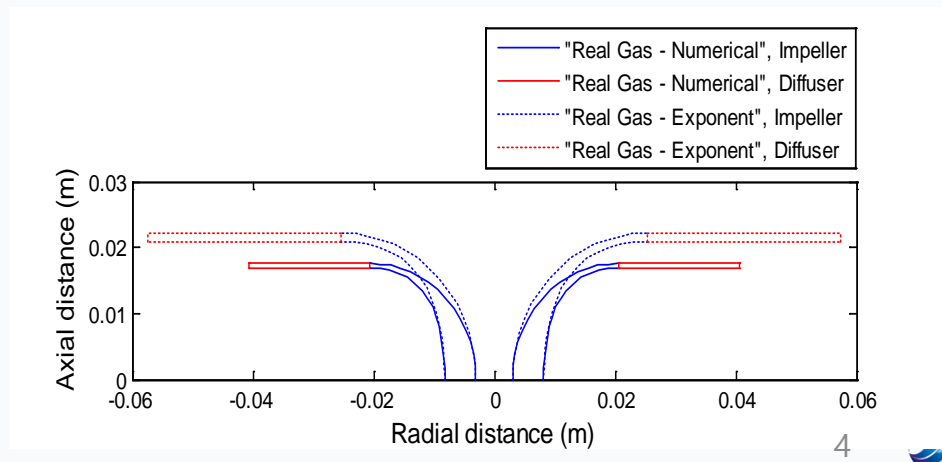
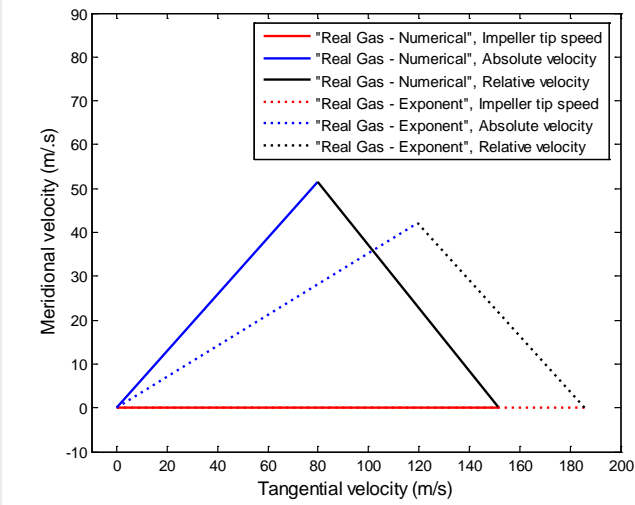
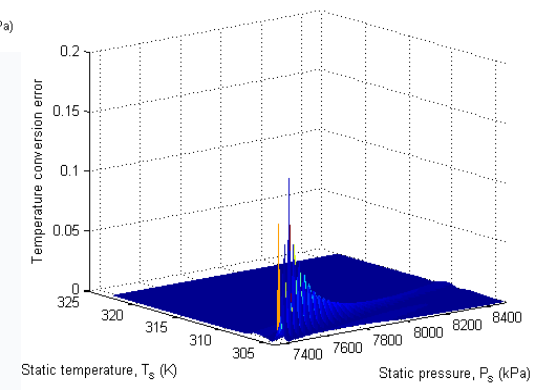
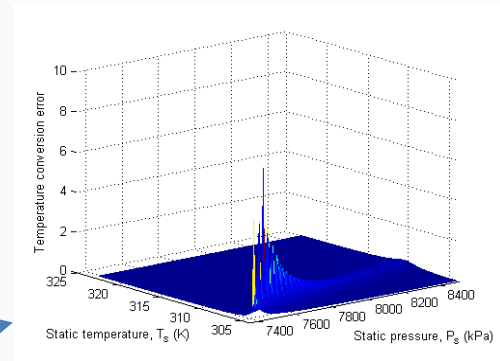
## 3D CFD analysis

- ✓ Internal flow analysis can be supported by 3D CFD analysis
- ✓ Complementary assistance platform can be constructed from 3D model information generation

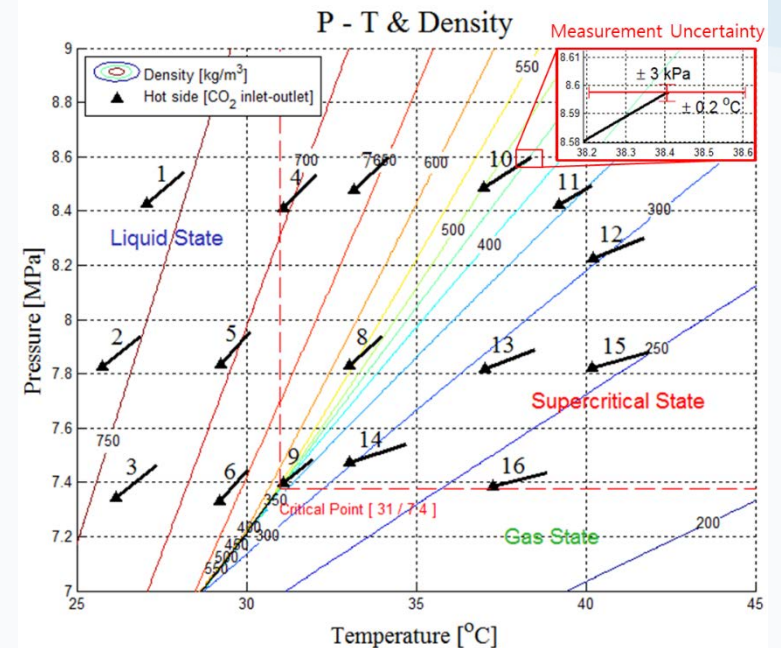
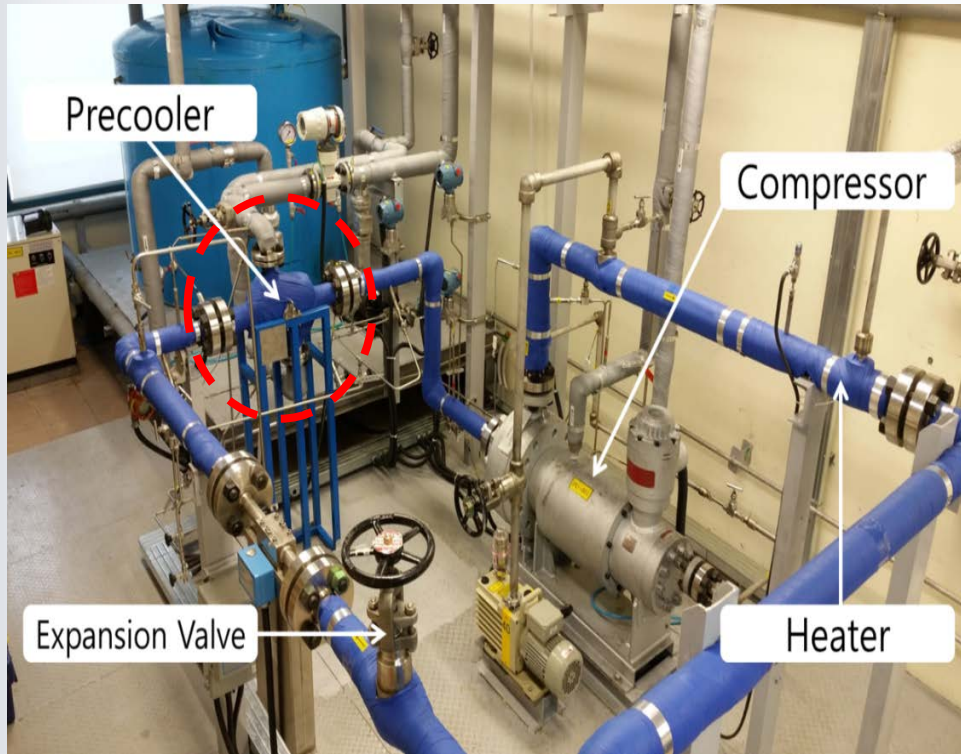


# Turbomachinery Design Issues

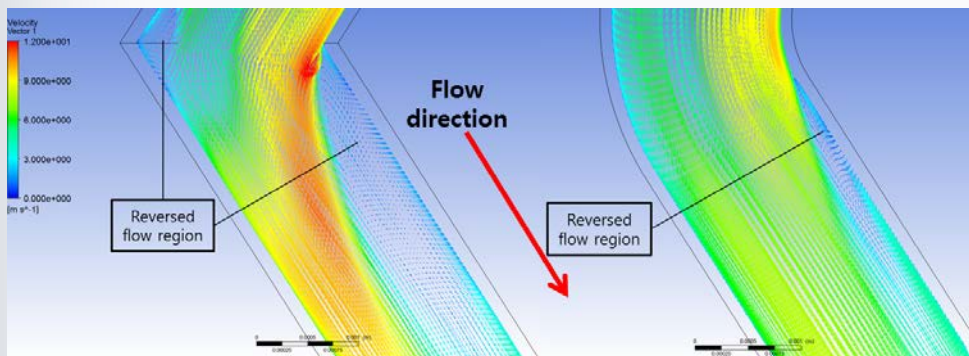
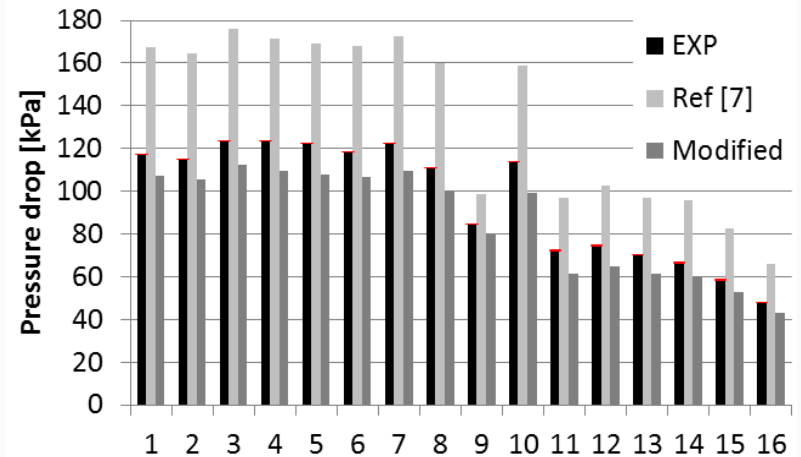
Conversion method	Equations
Definition based	$h_o = h_s + \frac{v^2}{2}$
Ideal gas based	$\frac{p_o}{p_s} = \left(1 + \frac{\gamma - 1}{2} M^2\right)^{\frac{\gamma}{\gamma - 1}}$ $\frac{T_o}{T_s} = 1 + \frac{\gamma - 1}{2} M^2$
Real gas isentropic exponent based	$\frac{p_o}{p_s} = \left(1 + \frac{n_s - 1}{2} M^2\right)^{\frac{1}{n_s - 1}}$ $\frac{T_o}{T_s} = \left(1 + \frac{n_s - 1}{2} M^2\right)^{\frac{m_s n_s}{n_s - 1}}$



# Heat Exchanger Design & Analysis



Hot side pressure drop comparison



# New Component

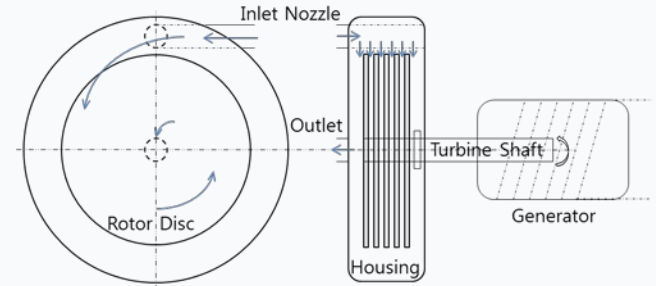
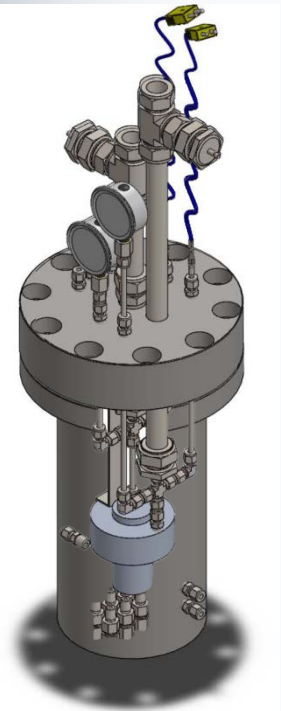


KAIST – SCO<sub>2</sub>PE



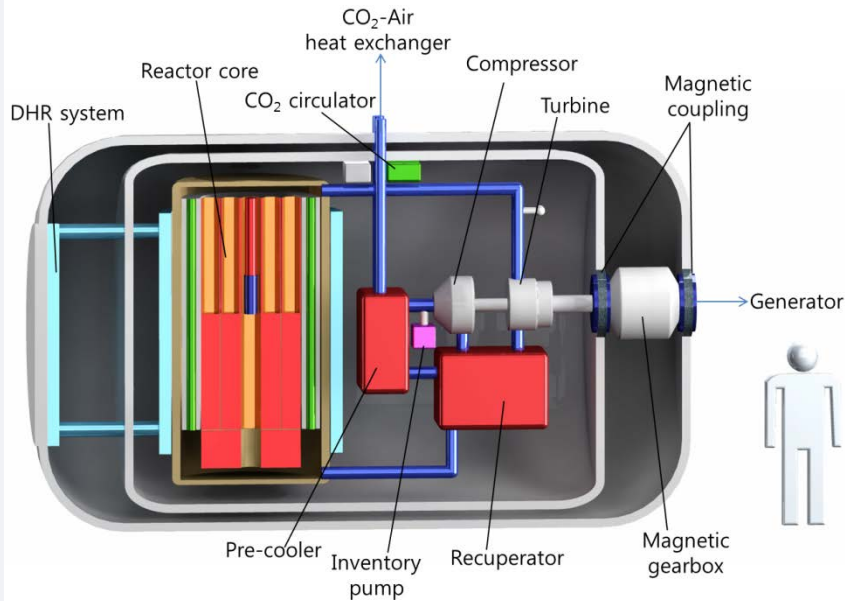
Tesla turbine

- A **Tesla turbine** will be tested in S-CO<sub>2</sub> power cycle expander operating conditions.
- The external pressure vessel allows to test in high pressure (>7.4 MPa)

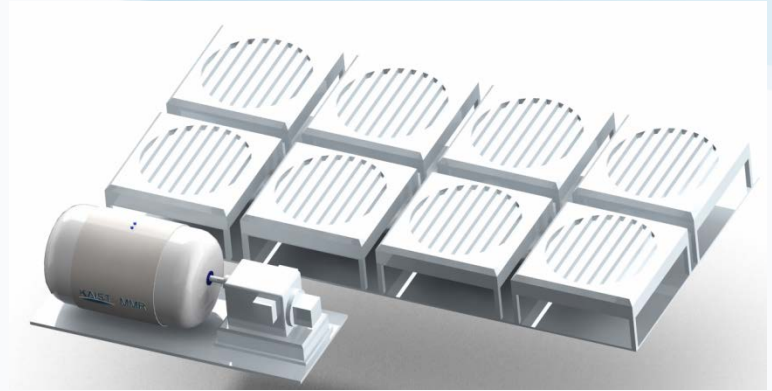


	Conventional Turbine	Tesla turbine
Characteristics	Blade	<b>Bladeless</b> disc
	Impulse & reaction force	<b>Friction</b> force
	Well experienced, optimized	<b>Low Pressure ratio</b> (S-CO <sub>2</sub> cycle)
	Need high quality clearance	<b>Manufacturing</b> - easy and modularized design
	No phase change allowed	<b>Robust</b> - Two phase, Sludge flow
	Maintenance Difficulties	Easy <b>maintenance</b>

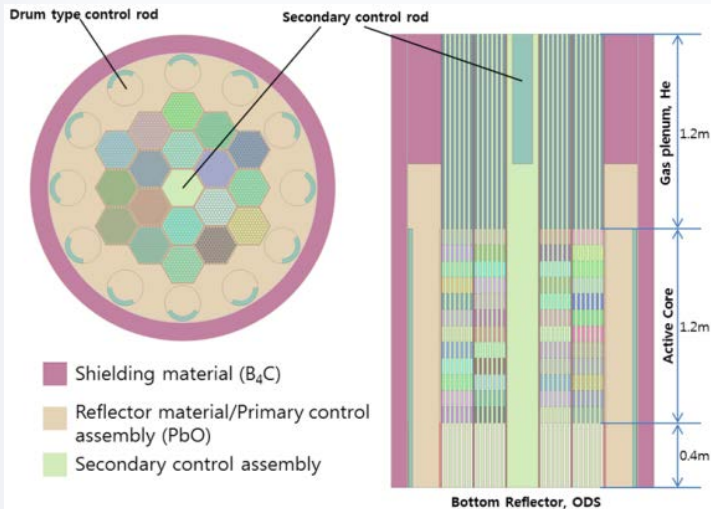
# New System



<Conceptual figure of KAIST MMR>



<With 8 fans and generator>

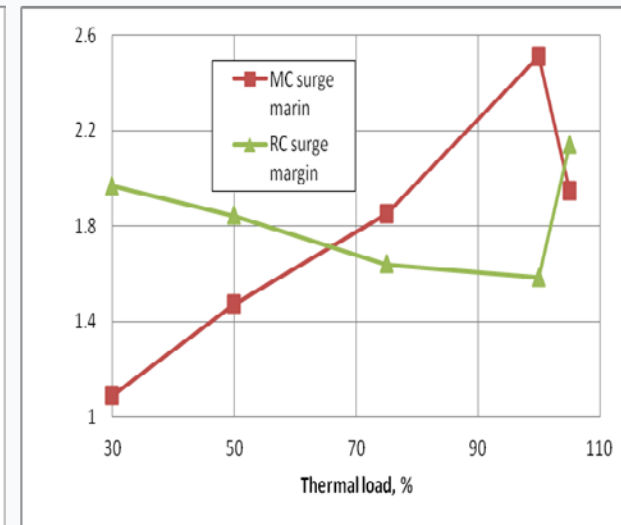
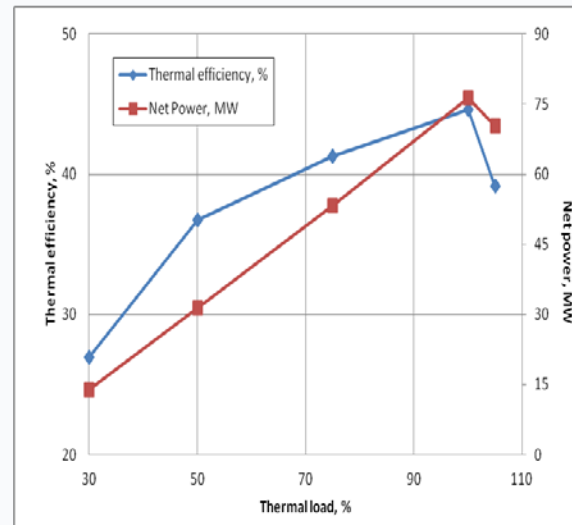
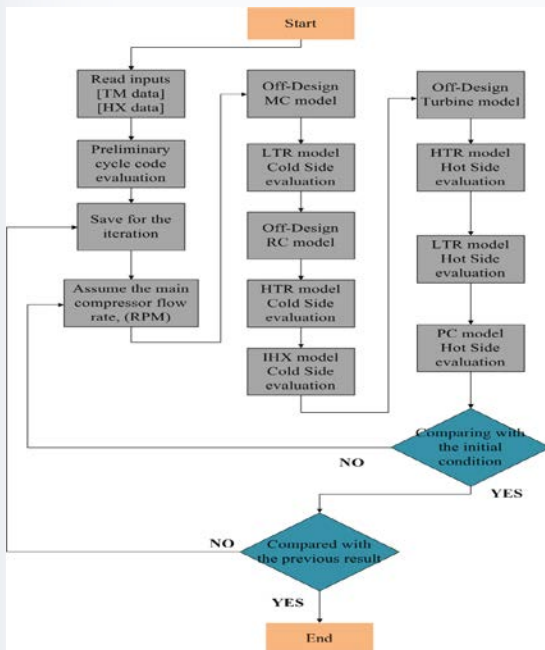
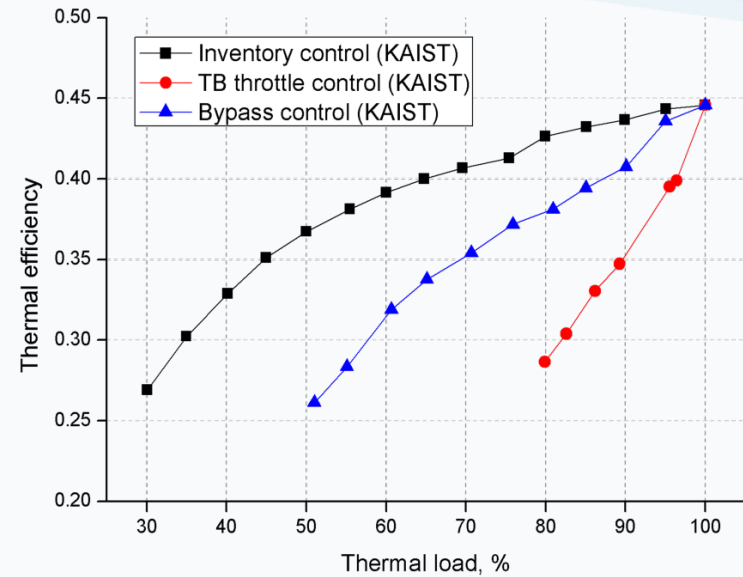
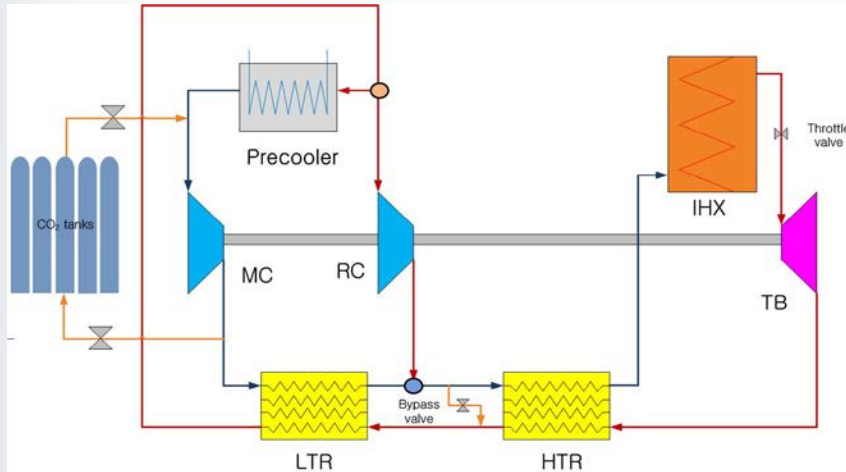


<MMR core design>

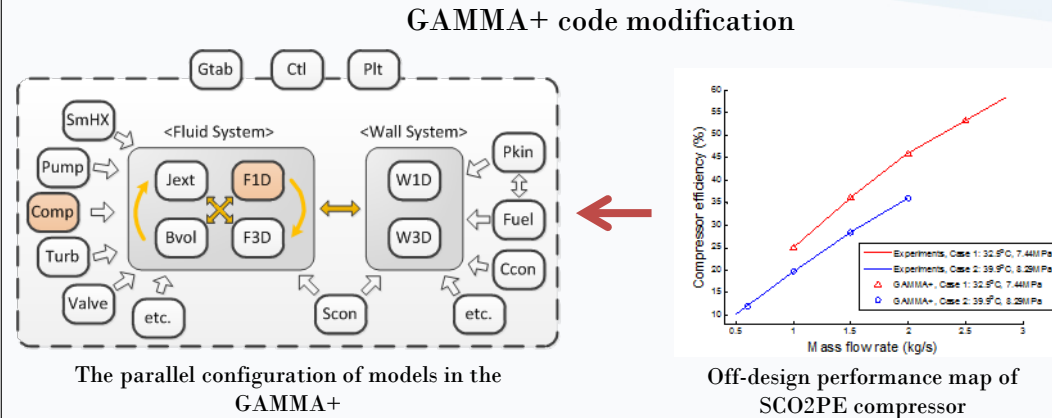
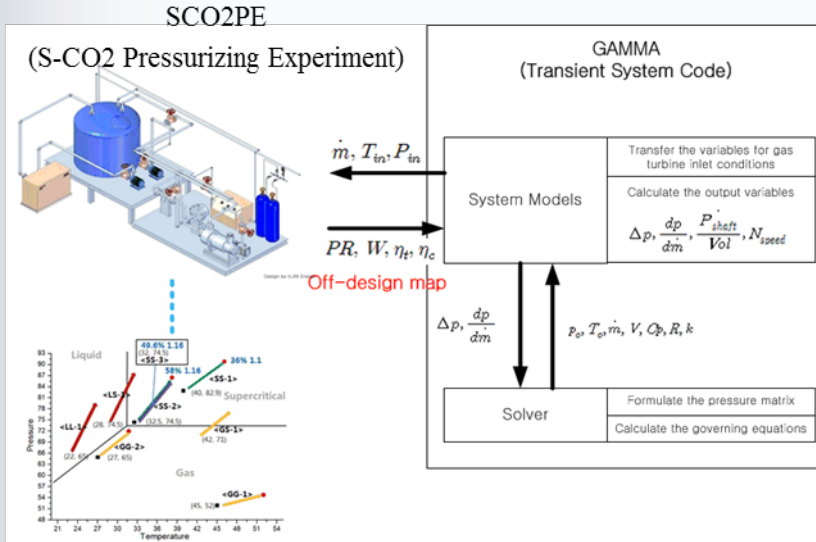




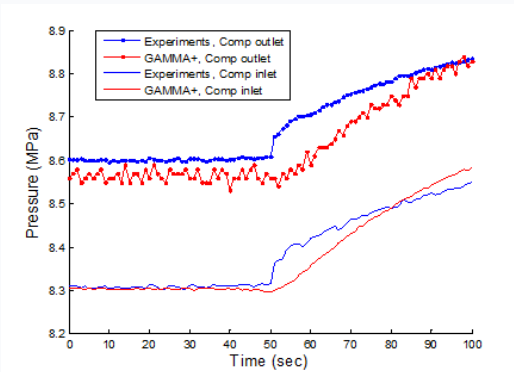
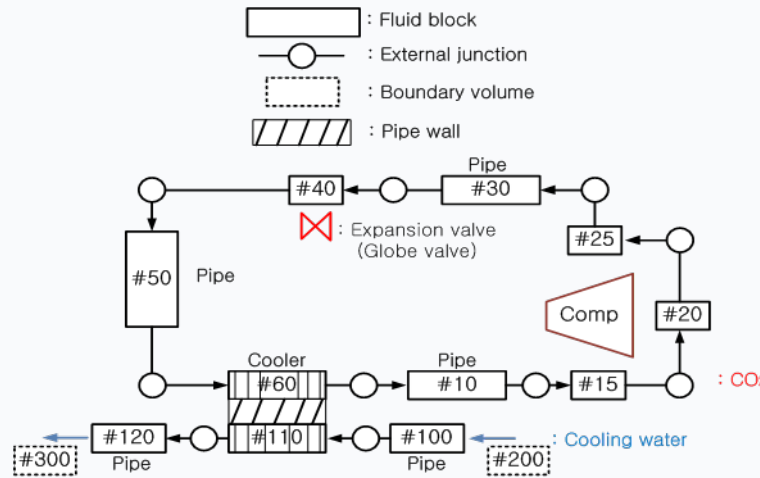
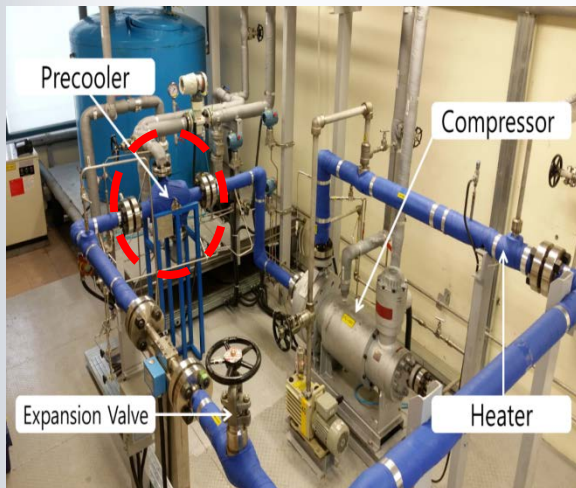
# Transient Analysis for Control



# Transient Analysis for Prediction



V&V between GAMMA+ code and SCO2PE test data



Transient pressure data comparison

Nodalization diagram of the SCO2PE loop for GAMMA+ code

# Specific Technical Issues to Sodium-cooled Fast Reactor Application

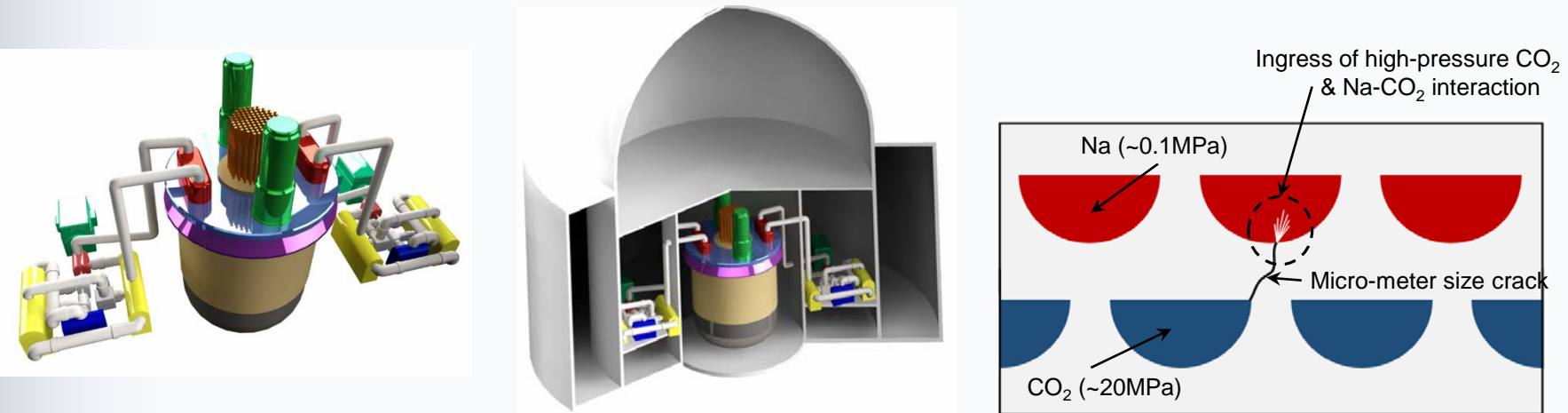
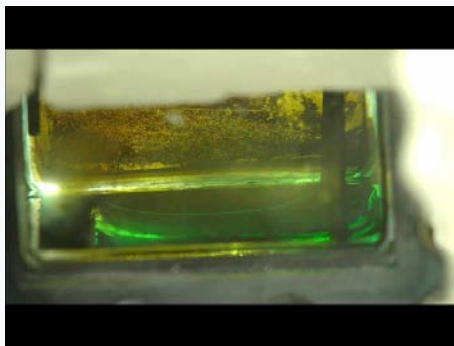


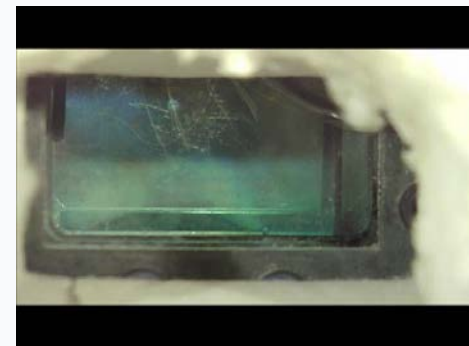
Fig. Potential Na-CO<sub>2</sub> interaction in Printed Circuit Heat Exchanger(PCHE)



$T_{Na} = 598.3 \text{ } ^\circ\text{C}$



$T_{Na} = 599.9 \text{ } ^\circ\text{C}$   
Ignition case



$T_{Na} = 585 \text{ } ^\circ\text{C}$   
Na-air reaction

# Critical Flow and Phase Change

## ◆ CO<sub>2</sub> critical flow modeling process

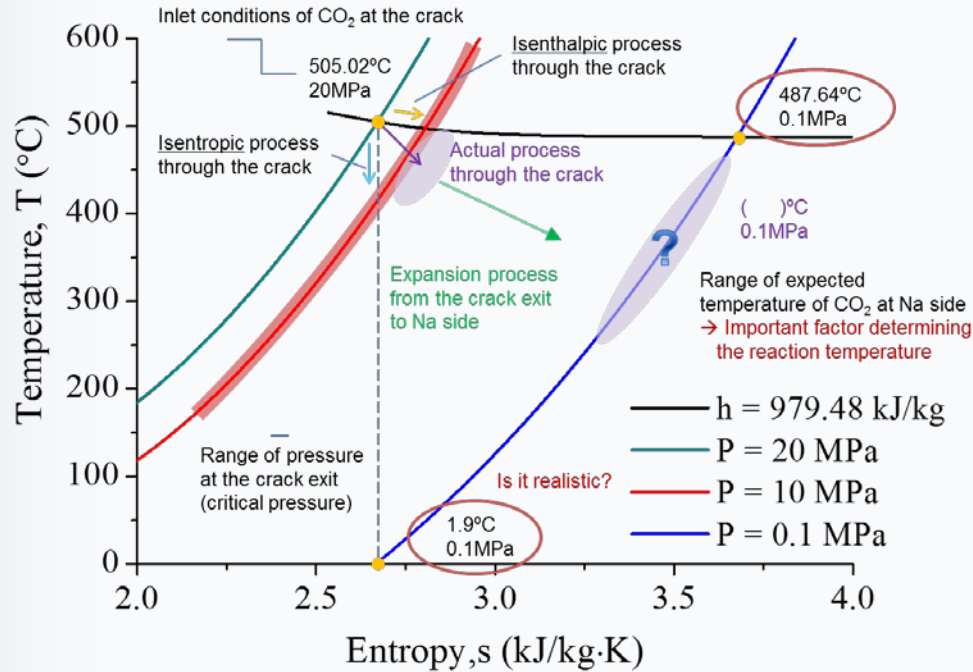
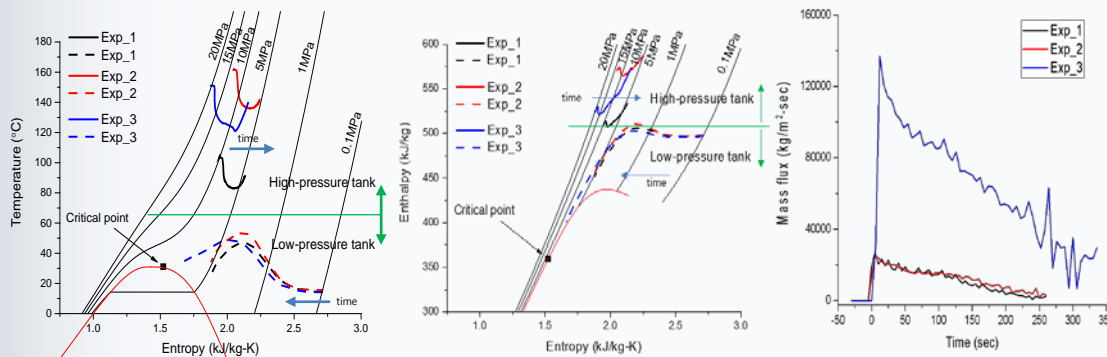


Fig. CO<sub>2</sub> critical speed measure instrument

## ◆ CO<sub>2</sub> leak simulation results (T-s, h-s diagram, Mass flux of leaked CO<sub>2</sub>)



		Exp_1	Exp_2	Exp_3
High Pressure Tank	P (MPa)	10.01	13.43	20.16
	T (°C)	103.3	161.5	151.2
Low Pressure Tank	P (MPa)	0.101	0.101	0.101
	T (°C)	14.5	15.6	14.1

# Materials

## ❖ Corrosion and carburization behavior in S-CO<sub>2</sub> environments

- ✓ Corrosion tests in S-CO<sub>2</sub> environments (550-650°C, 200bar, max. 3000h)
- ✓ Evaluate the corrosion and carburization resistance in S-CO<sub>2</sub> environments
- ✓ Materials: Fe-base austenitic alloys, Ni-base alloys, FMS (9Cr)

## ❖ Long-term properties of materials after exposure to S-CO<sub>2</sub>

- ✓ Microstructure evolution and resulting mechanical property (tensile test)
- ✓ Creep test in S-CO<sub>2</sub> environments (550-650°C, 200bar)

## ❖ Corrosion and long-term properties of diffusion-bonded PCHE materials

- ✓ Development of diffusion-bonding process for PCHE-type IHX
- ✓ Corrosion tests and mechanical property evaluation of diffusion bonded joints in S-CO<sub>2</sub> environments

