

OXY-COAL-FIRED CIRCULATING FLUID BED COMBUSTION WITH A COMMERCIAL UTILITY-SIZE SUPERCRITICAL CO<sub>2</sub> POWER CYCLE

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March 29, 2016

# Presentation Outline



- **Overall Plant Cycle: Oxy-Coal-Fired Circulating Fluid Bed (CFB) + Power Cycle**
  - *SOA (Commercially Available) SuperCritical (SC) Steam Rankine (3500 psig/1110°F/1150°F)*
  - *Recompression SuperCritical Carbon Dioxide (sCO<sub>2</sub>) Brayton (~5000 psig /1148°F)*
  - *Advanced Ultra-SuperCritical (AUSC) Steam Rankine (3500 psig/1400°F/1400°F)*
- **Alternate sCO<sub>2</sub> Recompression Cycle Configurations**
  - *Reheat sCO<sub>2</sub> Case*
  - *Intercooled sCO<sub>2</sub> Case*
  - *Reheat and Intercooled Case*
- **Sensitivity Analyses to sCO<sub>2</sub> Operating Parameters**
  - *Overview of earlier sensitivity analysis*
- **Elevated Turbine Inlet Temperature Case (increases TIT to 1400°F)**
- **Summary and Conclusions**
- **Next Steps**
- **Acknowledgements**
  - Study Group, Generic Heat Source Cycles, NETL Programs

# Site Characteristics and Design Coal



- Generic Midwestern U.S. Plant,
- ISO ambient conditions
- Illinois No. 6

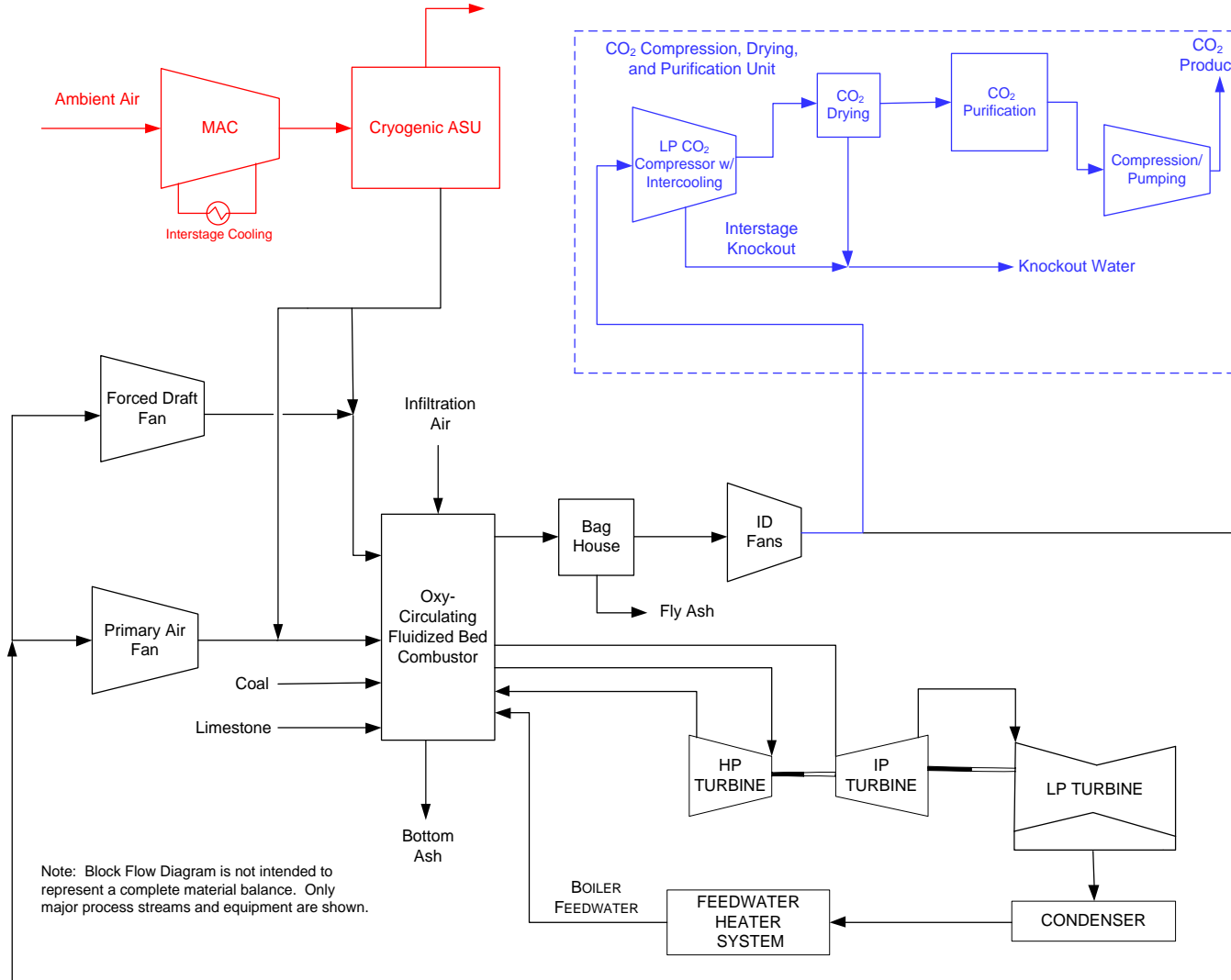
Elevation, ft	0
Barometric Pressure, psia	14.696
Design Ambient Temperature, Dry Bulb, °F	59
Design Ambient Temperature, Wet Bulb, °F	51.5
Design Ambient Relative Humidity, %	60

Coal name	Illinois No. 6	
ASTM D388 Rank	High Volatile A Bituminous	
Proximate Analysis	As-received %	Dry %
Moisture	11.12	0.00
Volatile Matter	34.99	39.37
Ash	9.70	10.91
Fixed Carbon	44.19	49.72
Total	100.00	100.00
Ultimate Analysis	As-received %	Dry %
Carbon	63.75	71.73
Hydrogen	4.50	5.06
Nitrogen	1.25	1.41
Sulfur	2.51	2.82
Chlorine	0.29	0.33
Ash	9.70	10.91
Moisture	11.12	0.00
Oxygen	6.88	7.74
Total	100.00	100.00
Reported Heating Value	As-received Btu/lb (kJ/kg)	Dry Btu/lb (kJ/kg)
HHV	11,666 (27,135)	13,126 (30,531)
LHV	11,252 (26,171)	12,660 (29,447)

Location	A Greenfield site in the Midwestern United States <sup>a</sup>
Topography	Level
Size, acres	300
Transportation	Rail and Road
Ash Disposal	Off Site
Water	Municipal (50%) / Groundwater (50%)
Access	Land locked, having access by rail and highway
CO <sub>2</sub>	Compressed to 15.3 MPa (2,215 psia), transported, and sequestered in a saline formation at a depth of 4,055 feet

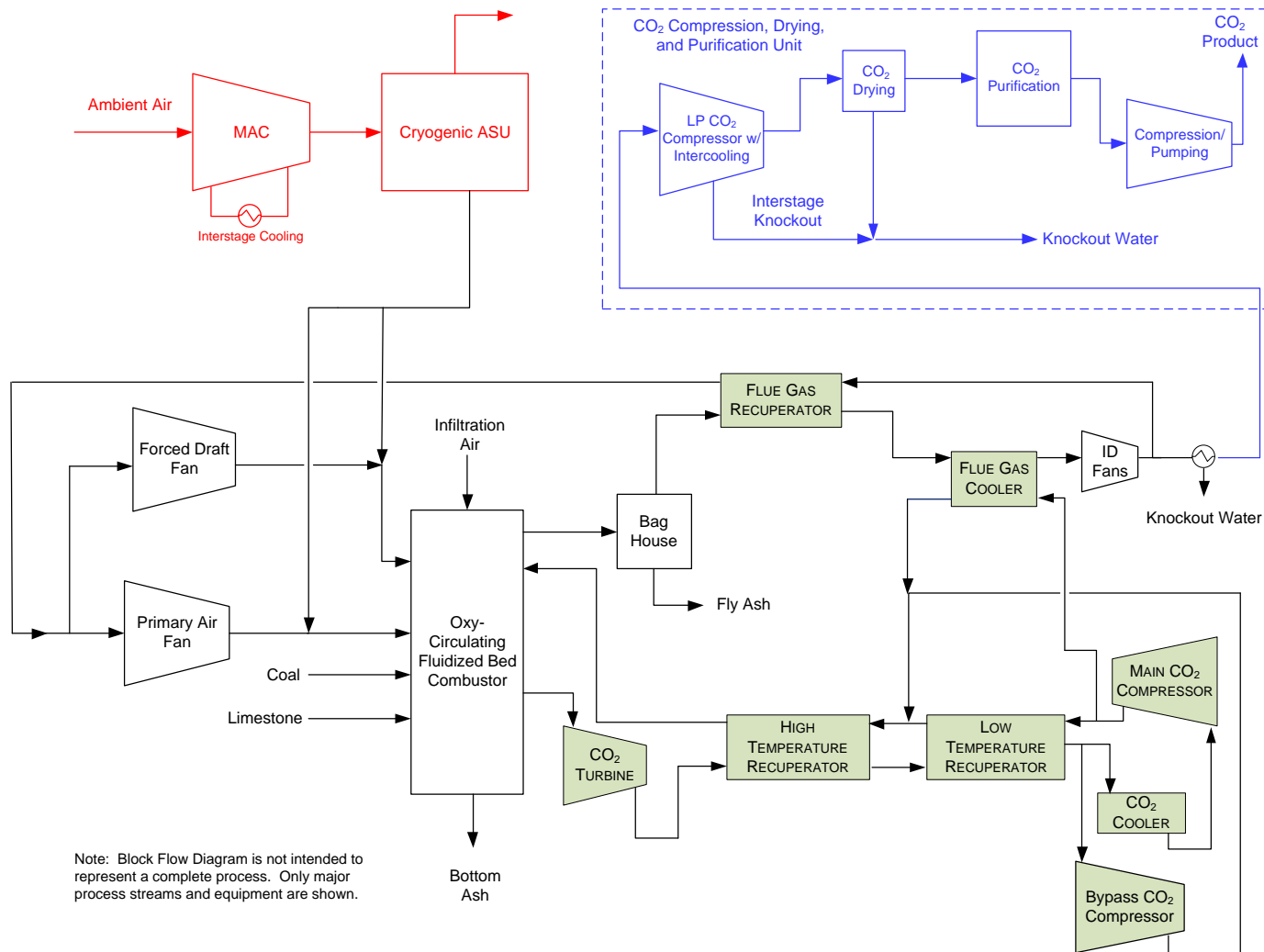
<sup>a</sup>Champaign County, Illinois, is assumed for assessment of construction costs.

# Oxy-Coal-Fired Circulating Fluid Bed (CFB) SOA SuperCritical (SC) Steam Rankine (3500 psig/1110°F/1150°F)



# Oxy-Coal-Fired Circulating Fluid Bed (CFB)

## Recompression SuperCritical Carbon Dioxide (sCO<sub>2</sub>) Brayton (5000 psig / 1148°F)



# Oxy-Coal-Fired Circulating Fluid Bed (CFB)

## Recompression sCO<sub>2</sub> Brayton Cycle Parameters for Baseline Plant



Parameter	Value
Turbine Inlet Temperature	620 °C (1148 °F)
Nominal Compressor Pressure	5,015 psia
Turbine Exit Pressure	1,350 psia
Nominal Pressure Ratio	3.8
CO <sub>2</sub> Cooler Temperature	35 °C (95 °F)
Turbine Isentropic Efficiency	92.7 %
Compressor Isentropic Efficiency	85.0 %
Cycle Pressure Drop	60 psia
Minimum Temperature Approach	6 °C (10 °F)
Nominal CO <sub>2</sub> Cooler Bypass Fraction	To maximize recuperation

# Oxy-Coal-Fired Circulating Fluid Bed (CFB)

Performance comparison between  
sCO<sub>2</sub> Brayton and Steam Rankine cycle plants



Parameter	Rankine Steam Cycle (593 °C, 1100 °F)	sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)
CFB Coal Flow Rate (klb/hr)	484	489
CFB Coal Flow Rate/Limestone Flow Rate	4.1	4.1
<b>Turb Flow Rate / Rankine Steam Turb Flow Rate</b>	<b>1</b>	<b>9.9</b>
Coal Thermal Input (MWt)	1655	1670
Power Cycle Thermal Input (MWt)	1497	1528
Fractional Thermal Input to Power Cycle	0.905	0.915
Net Power Cycle Output	723	727
Total Auxiliary Power Load	173	177
Net Power Output	550	550
<b>Power Cycle Efficiency (%)</b>	<b>48.3</b>	<b>47.6</b>
<b>Net Plant Efficiency (HHV %)</b>	<b>33.2</b>	<b>32.9</b>

## **Objectives**

- *Increase the fraction of plant thermal input that is captured in the sCO<sub>2</sub> cycle*
- *Increase the sCO<sub>2</sub> power cycle efficiency*
- *Decrease the sCO<sub>2</sub> plant auxiliary power requirement*
- *Provide some combination of above effects*

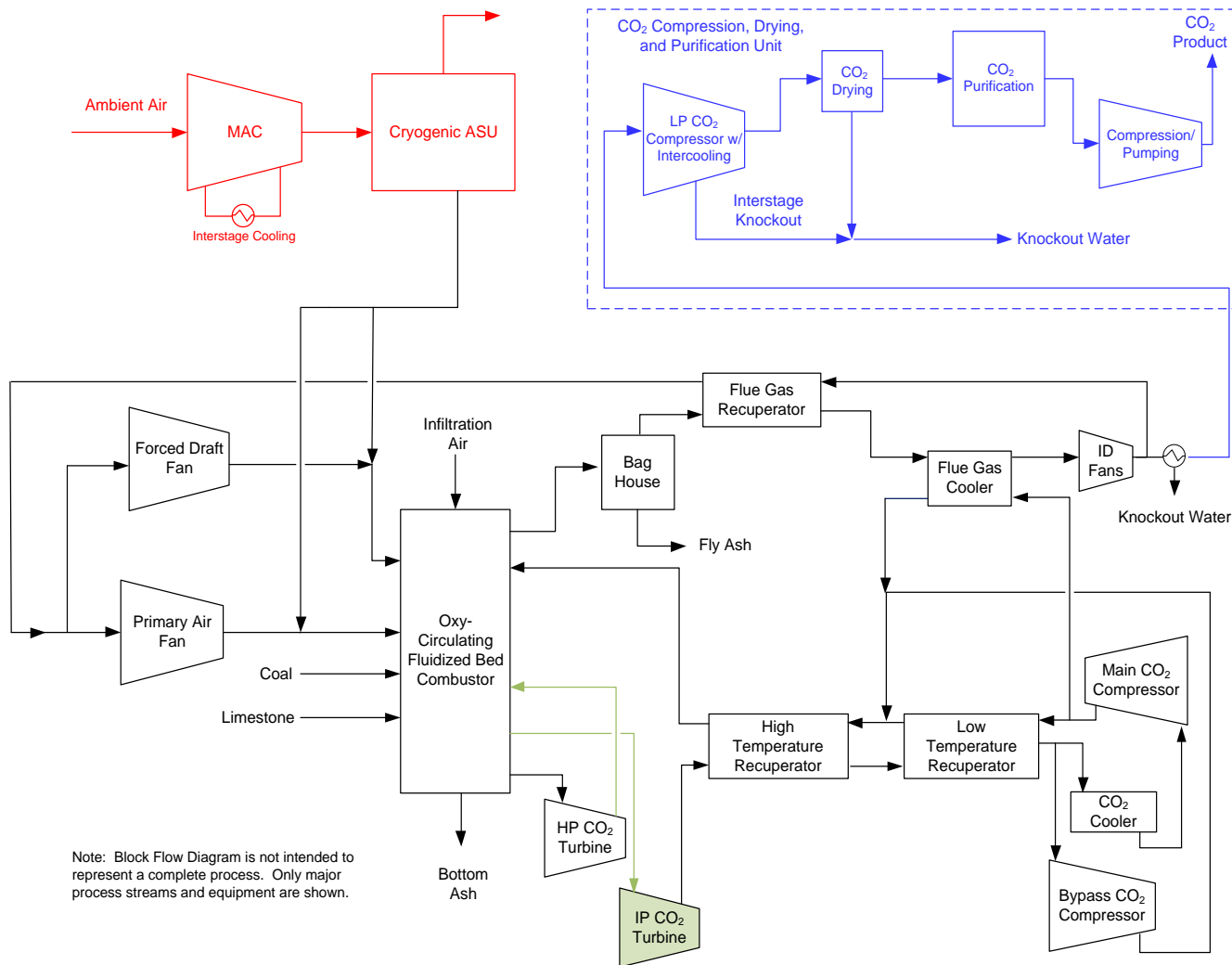
## **Alternate Cycles**

- *Reheat sCO<sub>2</sub> Case*
- *Intercooled sCO<sub>2</sub> Case*
- *Reheat and Intercooled Case*



# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

## Reheat sCO<sub>2</sub> Case



# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

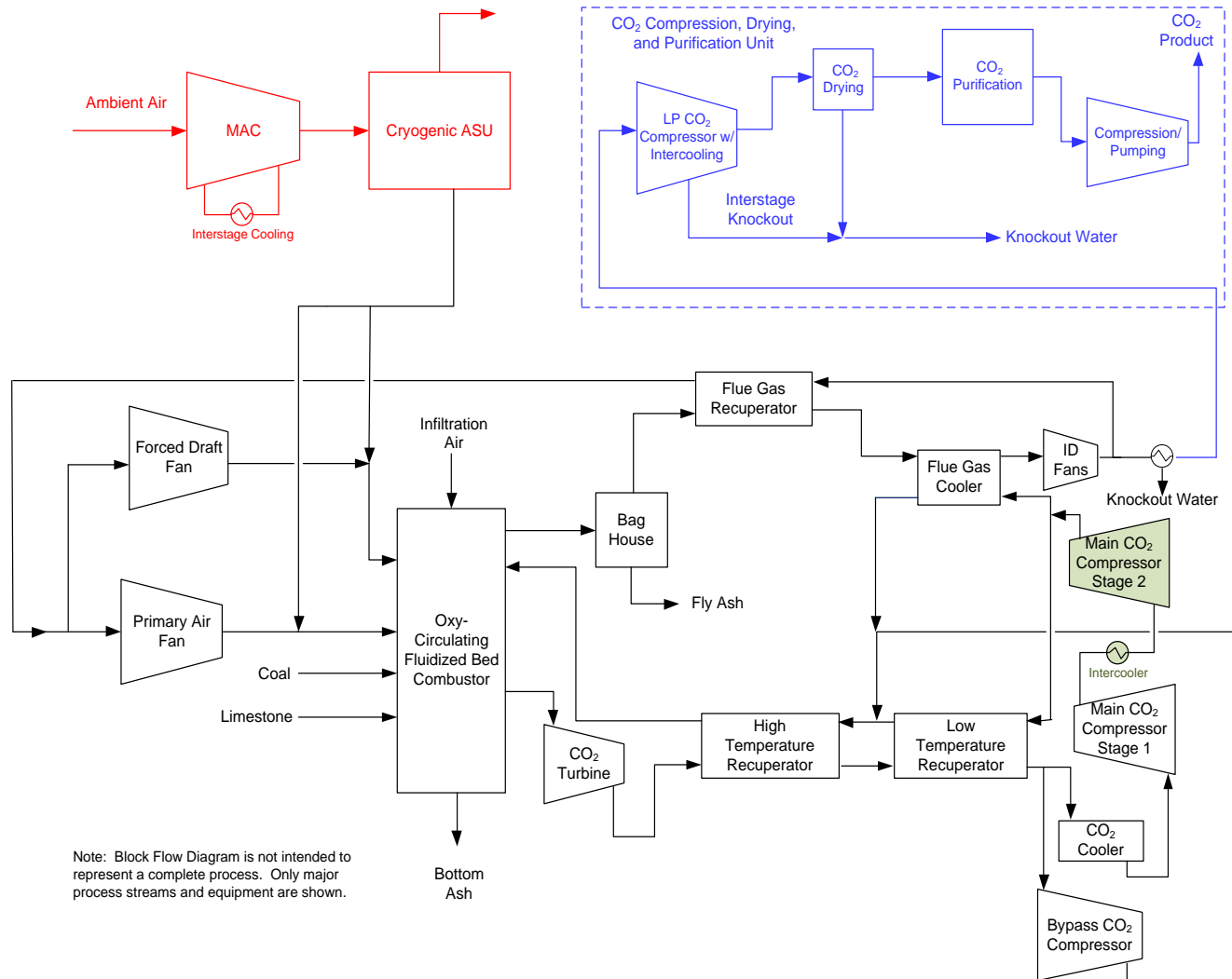
## Performance comparison between Rankine and Recompression sCO<sub>2</sub> Brayton cycles with and without reheat



Parameter	Rankine Steam Cycle (593 °C, 1100°F)	Baseline sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)	Reheat sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)
CFB Coal Flow Rate (klb/hr)	484	489	467
CFB Coal Flow Rate/Limestone Flow Rate	4.1	4.1	4.1
<b>Turb Flow Rate / Rankine Steam Turb Flow Rate</b>	<b>1</b>	<b>9.9</b>	<b>9.1</b>
Coal Thermal Input (MWt)	1655	1670	1597
Power Cycle Thermal Input (MWt)	1497	1528	1461
Fractional Thermal Input to Power Cycle	0.905	0.915	0.915
Net Power Cycle Output	723	727	719
Total Auxiliary Power Load	173	177	169
Net Power Output	550	550	550
<b>Power Cycle Efficiency (%)</b>	<b>48.3</b>	<b>47.6</b>	<b>49.3</b>
<b>Net Plant Efficiency (HHV %)</b>	<b>33.2</b>	<b>32.9</b>	<b>34.4</b>

# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

## Intercooled sCO<sub>2</sub> Case



# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

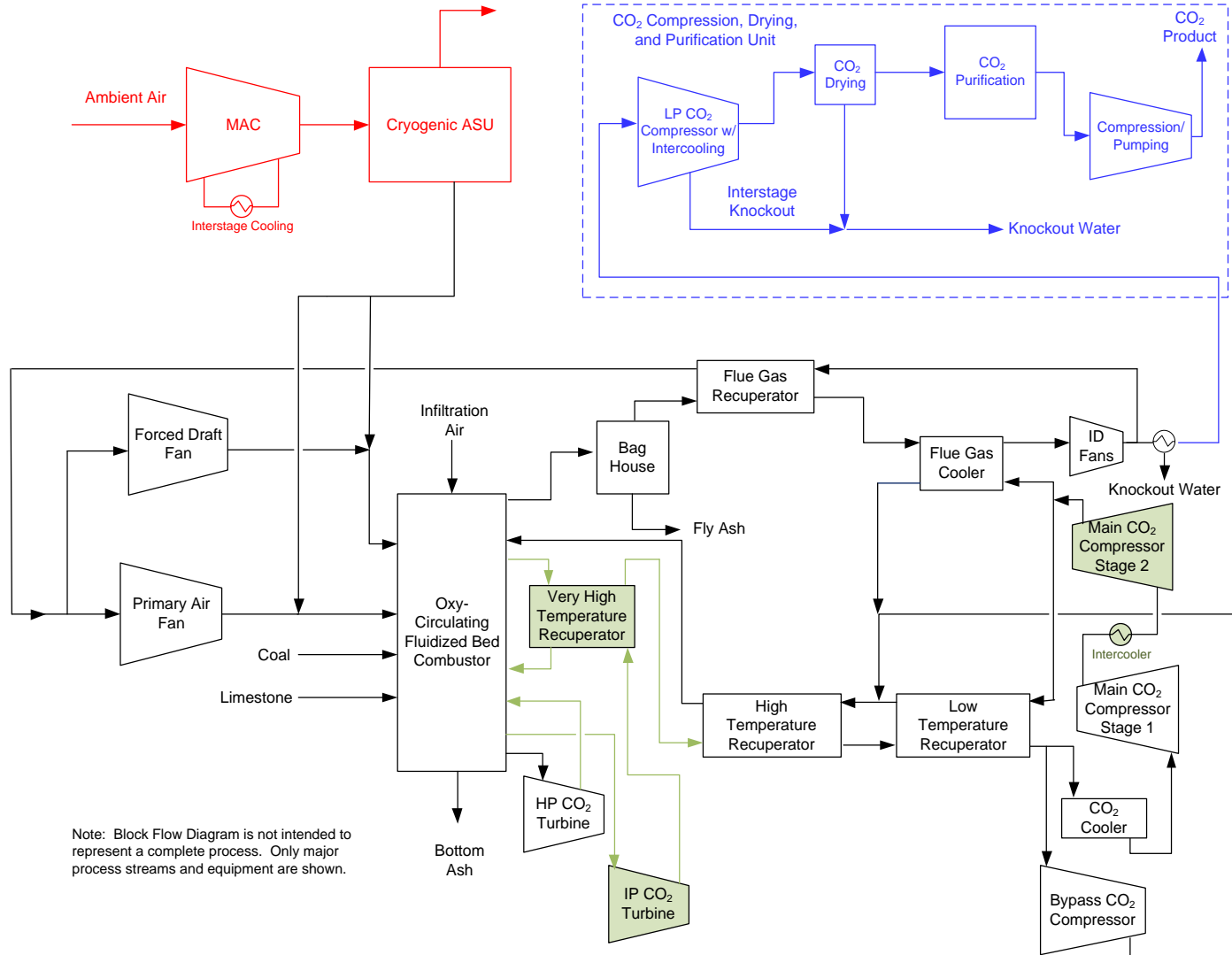
Performance comparison between Rankine and recompression sCO<sub>2</sub> Brayton cycles with and without main compressor intercooling



Parameter	Rankine Steam Cycle (593 °C, 1100°F)	Baseline sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)	Intercooled sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)
CFB Coal Flow Rate (klb/hr)	484	489	473
CFB Coal Flow Rate/Limestone Flow Rate	4.1	4.1	4.1
<b>Turb Flow Rate / Rankine Steam Turb Flow Rate</b>	<b>1</b>	<b>9.9</b>	<b>9.1</b>
Coal Thermal Input (MWt)	1655	1670	1619
Power Cycle Thermal Input (MWt)	1497	1528	1501
<b>Fractional Thermal Input to Power Cycle</b>	<b>0.905</b>	<b>0.915</b>	<b>0.927</b>
Net Power Cycle Output	723	727	722
Total Auxiliary Power Load	173	177	172
Net Power Output	550	550	550
<b>Power Cycle Efficiency (%)</b>	<b>48.3</b>	<b>47.6</b>	<b>48.1</b>
<b>Net Plant Efficiency (HHV %)</b>	<b>33.2</b>	<b>32.9</b>	<b>34.0</b>

# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

## Reheat and Intercooled Case



# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

Performance comparison between Rankine, baseline sCO<sub>2</sub> recompression, and sCO<sub>2</sub> Brayton with reheat and main compressor intercooling



Parameter	Rankine Steam Cycle (593 °C, 1100°F)	Baseline sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)	Reheat and Intercooled sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)
CFB Coal Flow Rate (klb/hr)	484	489	457
CFB Coal Flow Rate/Limestone Flow Rate	4.1	4.1	4.1
<b>Turb Flow Rate / Rankine Steam Turb Flow Rate</b>	<b>1</b>	<b>9.9</b>	<b>8.5</b>
Coal Thermal Input (MWt)	1655	1670	1562
Power Cycle Thermal Input (MWt)	1497	1528	1448
<b>Fractional Thermal Input to Power Cycle</b>	<b>0.905</b>	<b>0.915</b>	<b>0.927</b>
Net Power Cycle Output	723	727	716
Total Auxiliary Power Load	173	177	166
Net Power Output	550	550	550
<b>Power Cycle Efficiency (%)</b>	<b>48.3</b>	<b>47.6</b>	<b>49.4</b>
<b>Net Plant Efficiency (HHV %)</b>	<b>33.2</b>	<b>32.9</b>	<b>35.2</b>

# Sensitivity Analyses to sCO<sub>2</sub> Operating Parameters

## *Overview of earlier sensitivity analyses*



- NETL – has conducted or reviewed multiple studies analyzing the performance of indirect cycles and the dependence on operating parameters. These studies examined the impact on cycle and system efficiencies for changes to operating parameters that include:
  - Turbine Inlet Temperature (TIT)
  - Maximum and minimum cycle pressures
  - CO<sub>2</sub> cooler temperature
  - Cycle pressure drop
  - Minimum approach temperature for recuperators
  - Turbo-machinery efficiencies
- Result – TIT exerts the strongest impact on cycle efficiencies
- Additional Case – changing the TIT from 620 °C, (1148 °F) to 760 °C, (1400 °F)

# Alternate sCO<sub>2</sub> Recompression Cycle Configurations

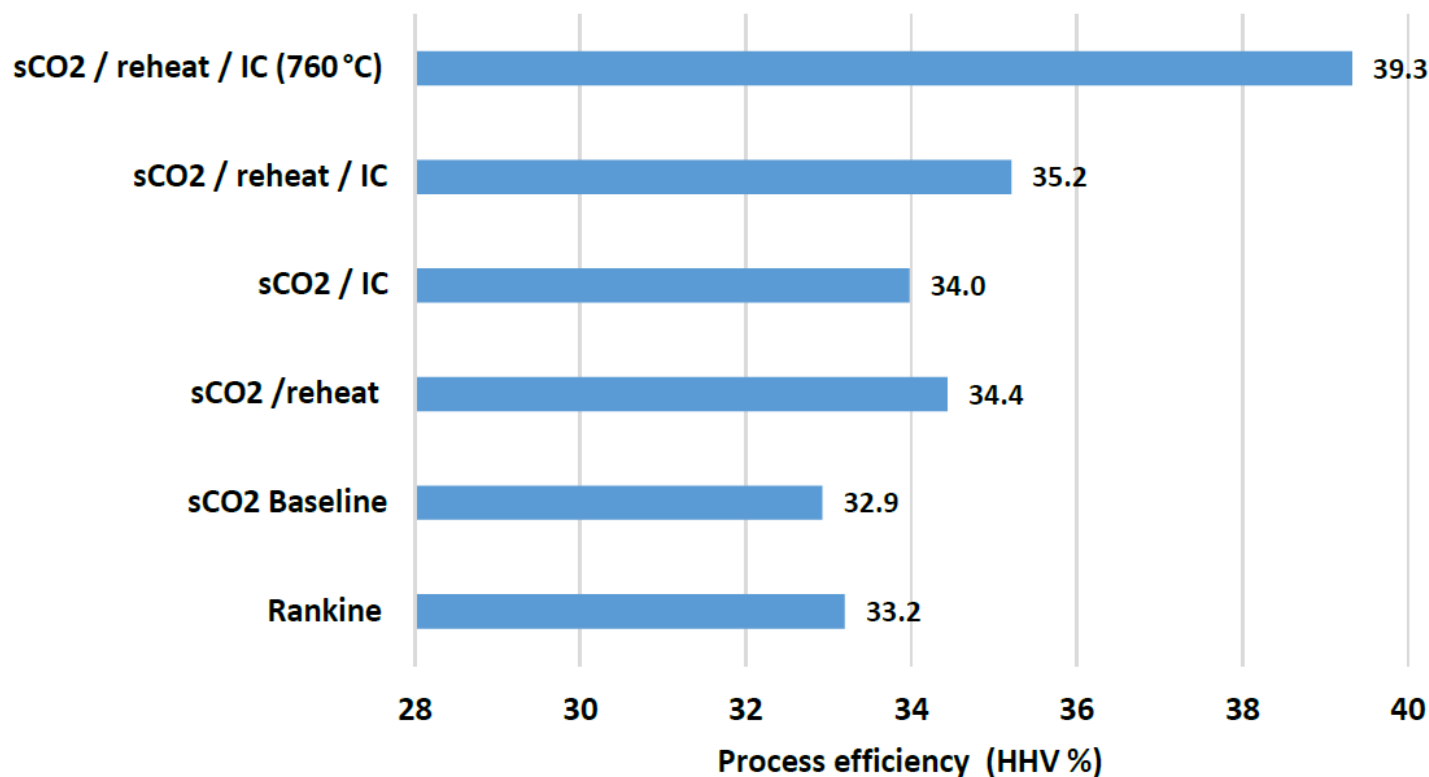
## Performance Comparison with Elevated Turbine Inlet Temperature Case



Parameter	Rankine Steam Cycle (593 °C, 1100°F)	Reheat and Intercooled sCO <sub>2</sub> Brayton Cycle (620 °C, 1148 °F)	Reheat and Intercooled sCO <sub>2</sub> Brayton Cycle (760 °C, 1400 °F)
CFB Coal Flow Rate (klb/hr)	484	457	409
CFB Coal Flow Rate/Limestone Flow Rate	4.1	4.1	4.1
<b>Turb Flow Rate / Rankine Steam Turb Flow Rate</b>	<b>1</b>	<b>8.5</b>	<b>6.8</b>
Coal Thermal Input (MWt)	1655	1562	1398
Power Cycle Thermal Input (MWt)	1497	1448	1296
<b>Fractional Thermal Input to Power Cycle</b>	<b>0.905</b>	<b>0.927</b>	<b>0.927</b>
Net Power Cycle Output	723	716	698
Total Auxiliary Power Load	173	166	148
Net Power Output	550	550	550
<b>Power Cycle Efficiency (%)</b>	<b>48.3</b>	<b>49.4</b>	<b>53.9</b>
<b>Net Plant Efficiency (HHV %)</b>	<b>33.2</b>	<b>35.2</b>	<b>39.3</b>



## Overall Plant Efficiencies (% HHV)



- Objective - compare sCO<sub>2</sub> Recompression Brayton Cycle(s) to a SOA Steam Rankine Cycle.
- Performance determined for four configurations, all showing performance improvement.
- At the lower temperature (620 °C, 1100 °F), the most comparable sCO<sub>2</sub> Case (reheat and intercooled) to the Steam Rankine Case shows improvement in overall process efficiency of ~ 2 percentage points.
- At the higher temperature (760 °C, 1400 °F), the comparison to the Steam Rankine Cycle (620 °C, 1100 °F) improves in overall efficiency to ~ 6 percentage points.
- Further optimizations of the configurations considered may be required to demonstrated an economic advantage.

# Next Steps

- **Advanced Ultra-SuperCritical (AUSC) Steam Rankine Case**
  - (3500 psig/1400°F/1400°F)
- **Economic Analysis**
  - Information from NETL sponsored programs + other sources for
  - Component costs for key sCO<sub>2</sub> Cycle Components
  - Cost sensitivity studies for key components
- **Alternate Cycles**
  - *Direct sCO<sub>2</sub> Cycles based on coal*
  - *Hybrid Cycles, Cascade Cycles*
  - *Condensing CO<sub>2</sub> Cycles*
- **Possible designs for pilot/demo plants**

# Acknowledgements



- **Study Group:**
  - *Charles White, John Plunkett, David Gray (ESPA/Noblis Inc.)*
  - *Walter Shelton, Nathan Weiland (NETL/DOE)*
- **Generic Heat Source sCO<sub>2</sub> Cycles**
  - *White, C., Shelton, W., Dennis, R. (2014, September 9-10). An Assessment of Supercritical CO<sub>2</sub> Power Cycles Integrated with Generic Heat Sources. 4<sup>th</sup> International Symposium – Supercritical CO<sub>2</sub> Power Cycles: Pittsburgh, Pennsylvania.*
- **PFBC sCO<sub>2</sub> Cycles**
  - *G. Subbaraman, J. A. Mays, B. Jazayeri, K. M. Sprouse, A. H. Eastland, S. Ravishankar and C. G. Sonwane, Energy Systems, Pratt and Whitney Rocketdyne, ZEPS Plant Model: A High Efficiency Power Cycle with Pressurized Fluidized Bed Combustion Process, 2nd Oxyfuel Combustion Conference, Queensland, Australia, September 2011.*
- **NETL Programs / Financial Support**
  - *sCO<sub>2</sub> Component Development (references 1 – 8 of conference paper)*
  - *Material Research and Thermodynamic Properties (e.g. programs with ORNL)*
  - *NETL Internal sCO<sub>2</sub> System Studies (indirect and direct cycles, STEP program, reviews of literature studies)*

# Questions ??



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