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S-CO₂ Brayton Loop Transient Modeling Kevin D Rahner

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Kevin D. Rahner received a B.S. in physics from University at Albany, SUNY and an M.S. degree in electrical engineering from Binghamton University, SUNY. In 2002 he joined the Knolls Atomic Power Laboratory, Niskayuna NY (operated by Bechtel Marine Propulsion Corporation for the U.S. Government). His development and work efforts have covered a wide range of engineering disciplines including electrical performance modeling and radiative heat transfer modeling of thermophotovoltaic (TPV) systems. Since 2007 he has been actively involved in transient modeling S-CO₂ Brayton cycles.

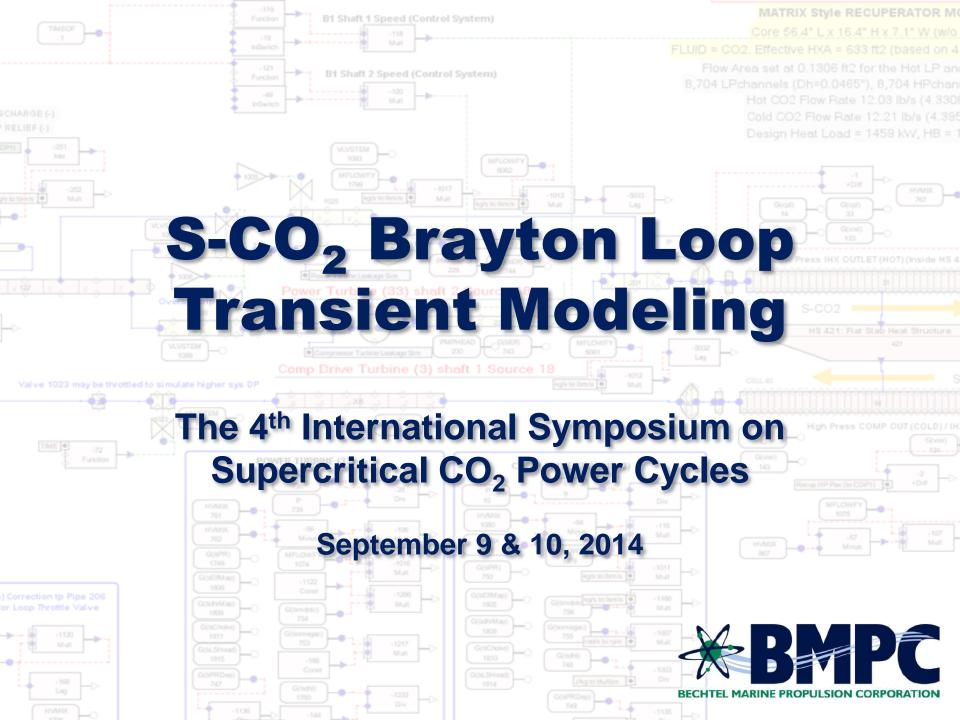
Abstracts

The Integrated System Test (IST) is a complete 100 kWe supercritical carbon dioxide (S-CO₂) Brayton system constructed and operated to validate design and control strategies. A full plant TRACE (TRAC/RELAP Advanced Computational Engine) model is the primary tool for thermal-hydraulic and control system design of this test facility. The model has been used to specify control strategy, control device characteristics and test procedures for safe and effective operation. While the model suggests which control methods are most effective, actual operation is needed to validate the predictions and gain valuable experience during nominal, off-nominal and faulted conditions. By qualifying the code and model using IST data the best design features and control methods will be applied to future applications. IST control strategy focuses on maintaining a constant compressor surge margin. At a constant surge margin high compressor efficiency and resilience to planned and unplanned transients is provided. Constant surge margin is achieved by matching compressor speed to system power output and matching system flow resistance to compressor speed. Changes in compressor speed and system resistance are best accomplished using a compressor recirculation (or recycle) valve, potentially in combination with turbine throttle valves. A compressor motor is available for startup, initial loop heatup, and special test purposes only.

Testing to date has confirmed the effectiveness of the overall IST control strategy and shown the TRACE model to be a highly effective tool for design and operation of an S-CO₂ closed Brayton power loop.

The Integrated System Test (IST) is a complete 100 kWe supercritical carbon dioxide (S-CO₂) Brayton system constructed and operated to validate design and control strategies. The IST turbomachinery was designed and manufactured by Barber-Nichols Inc (BNI). Predicted turbomachinery performance maps were also provided by BNI that relates mass flow, turbine/compressor speed, with enthalpy rise/drop. These performance maps are incorporated into a TRACE transient model used for thermal-hydraulic and control system design.

Recent testing performed over a wide range of operating conditions provides the opportunity for comparing predicted turbomachinery performance with data at off-nominal conditions. Because operational S-CO₂ power cycles are relatively new, there is limited data for empirically derived loss models and design tools to have been validated for use with operating turbomachinery near the working fluid critical point. The operation of radial inflow turbines and radial compressor at off-design conditions necessitate the use of "corrected" conditions to interrogate the performance maps. The pressure losses and need to correct for variations in inlet fluid conditions add to the uncertainty of predicted turbomachinery performance. IST test data will be compared to performance predictions to assess turbomachinery performance maps.





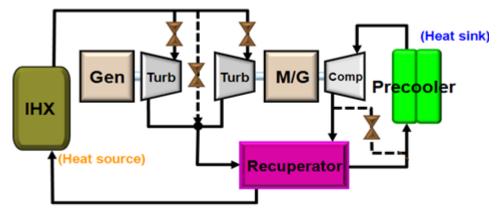
Background

- Model Results and Comparisons with Test Data
 - Steady State Heat Balance
 - Transient
 - Turbomachinery Start-up
 - Power Transients
- Next Steps/Model Updates
 - NIST REFPROP/FIT
 - Test data

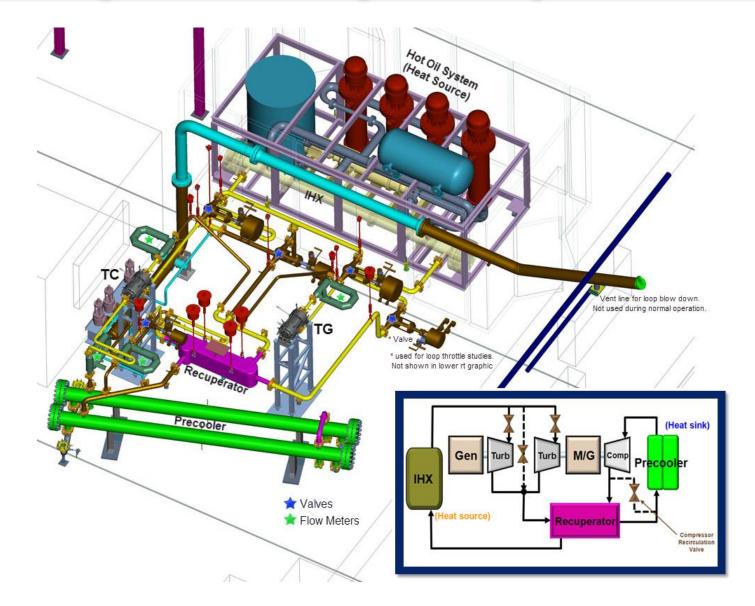
Summary



- Integrated Systems Test (IST)
 - Characteristics
 - Recuperated Closed Cycle Brayton
 - Rated power 100kWe
 - Power and Compressor Turbines in Parallel
 - Constant Speed Turbine Generator
 - Generated power ∞ Compressor Speed
 - Fixed inventory
 - Purpose
 - Operational experience
 - Demonstrate system control
 - Validate transient model



Background: Integrated Systems Test



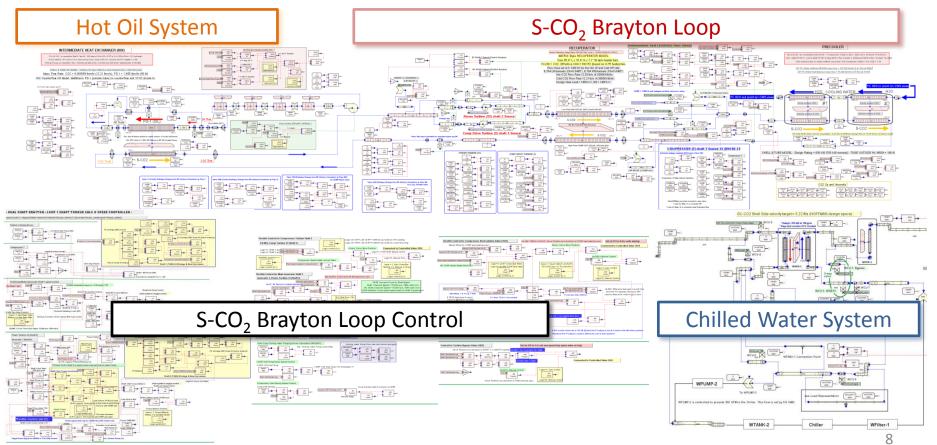
Background: Integrated Systems Test



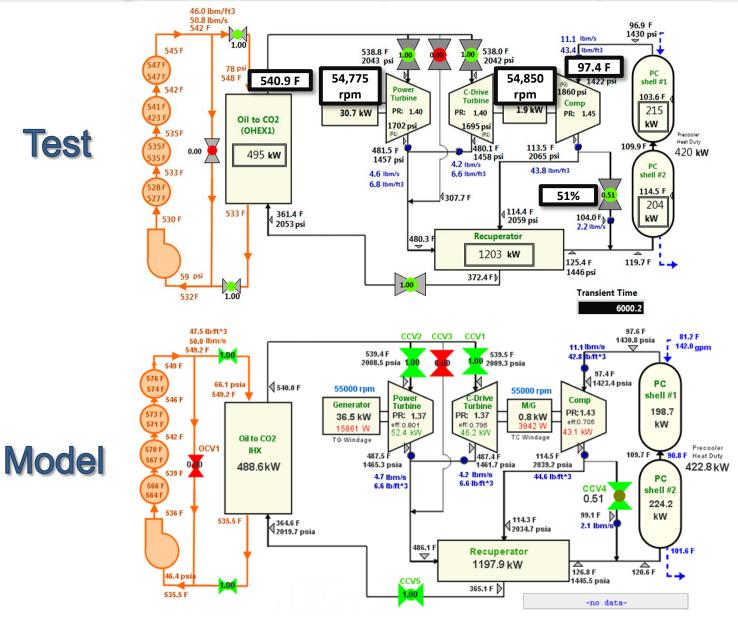
Background: IST Transient Model

IST Transient Model

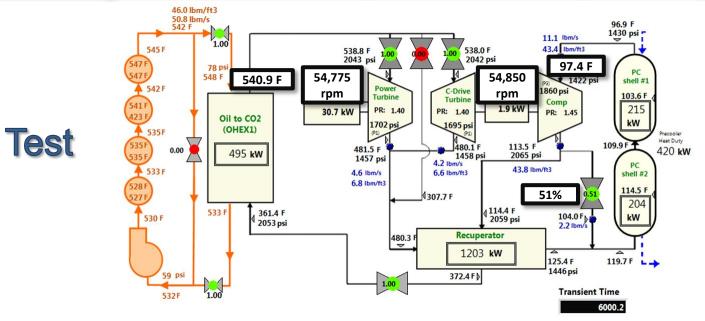
- Built using TRACE and SNAP GUI
- Heat Source to Heat Sink
- Developed compressible fluid modeling methods
- Developed control systems



Steady State Comparison: Updated Model



Steady State Comparison: Updated Model



Parameter	Test	Pretest TRACE Model	TRACE Model With adjusted compressor map	
Compressor Mass Flow (Ibm/s) [kg/s]	11.1 [5.0]	10.1 [4.6]	11.1 [5.0]	
Compressor PR	1.45	1.37	1.43	
Compressor Exit Temperature (F) [K]	113.5 [318.3]	113.2 [318.1]	114.5 [318.8]	

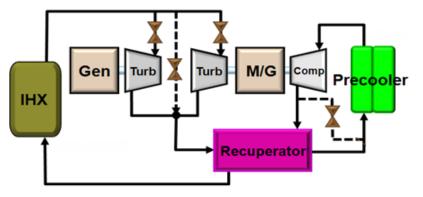


>Phenomenon considered during turbomachinery startup

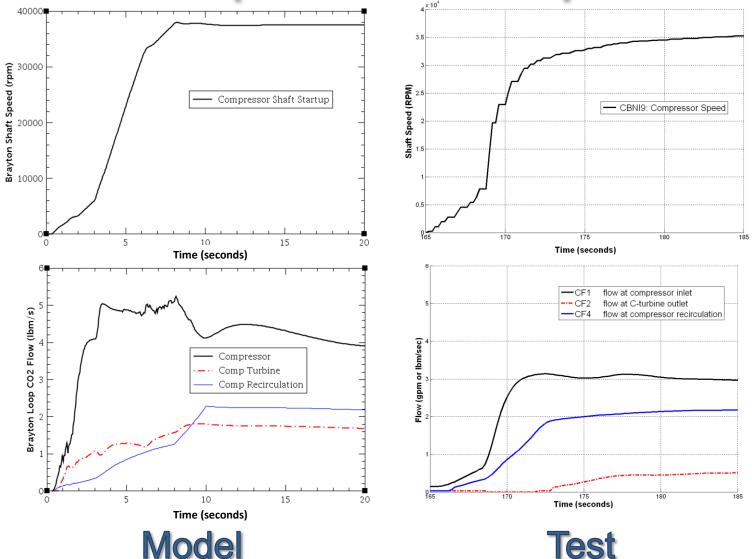
- Compressor surge
- Reverse Turbine Flow
- Gas Foil Bearing Lift-off

Target Conditions for IST Turbomachinery Startup

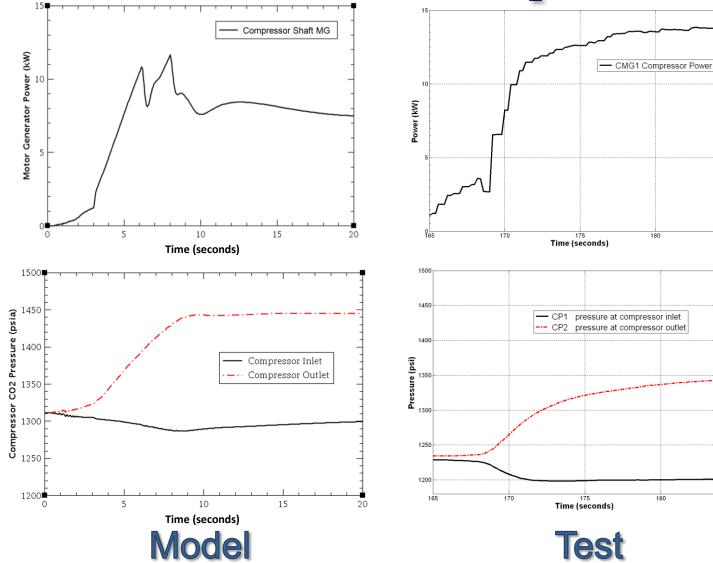
Parameter	Target Value		
Turbine inlet temperatures	165°F (Z = 0.7)		
Compressor inlet temperature	100°F		
Compressor inlet pressure	1230 psia		
Turbine bypass valve	Shut		
Compressor recirculation valve	83% open		



<u>IST Startup</u>: Comparison between Model (left) and Test data (right) for Compressor Startup – Shaft Speed and Main Loop Flows



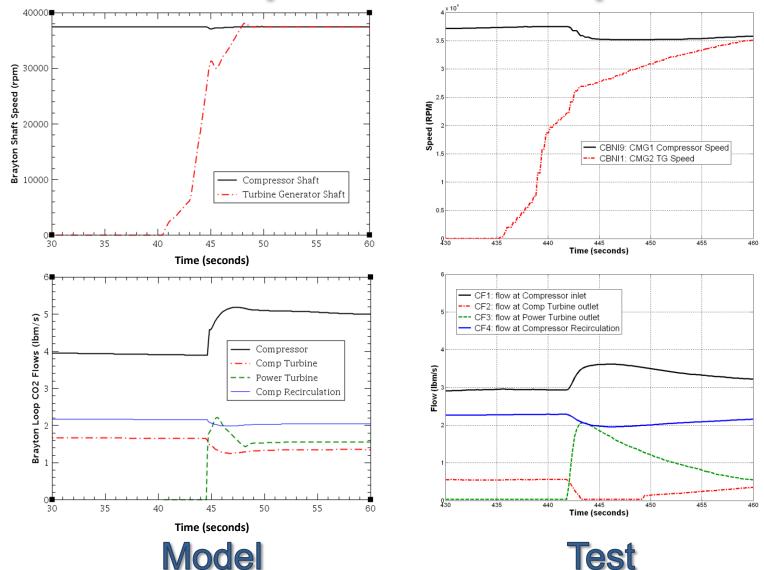
<u>IST Startup</u>: Comparison between Model and Test for Turbine Compressor Startup – Shaft Motor Generator Powers and CO₂ Pressures



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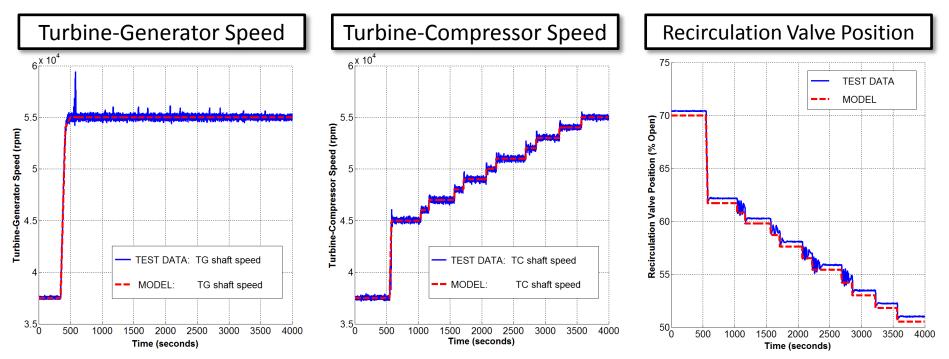
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<u>IST Startup</u>: Comparison between Model and Test for Turbine Generator Startup – Shaft Speed and Main Loop Flows

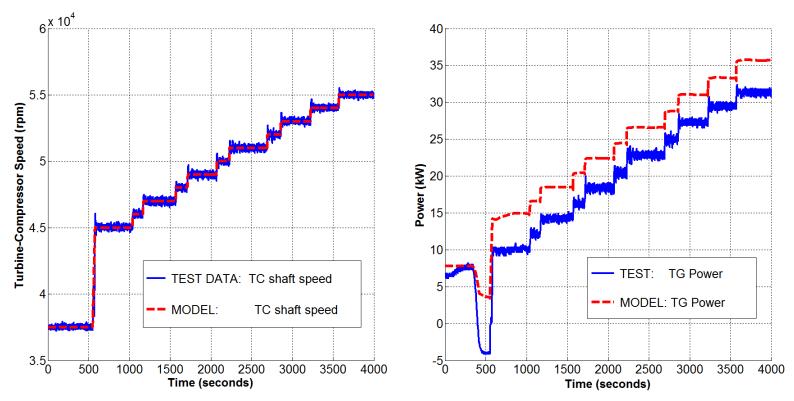


Power Increase Transient

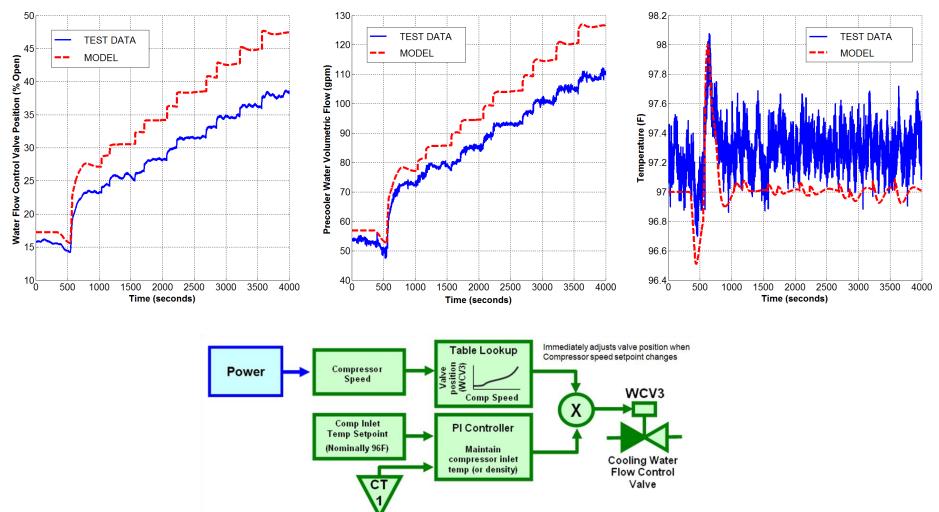
- Initial Conditions: Hot Idle (540°F/37,500 rpm)
- TG speed increased
- TC speed increased in steps
- Compressor recirculation valve decreased in steps
- Water flow automatically controlled to maintain compressor inlet T



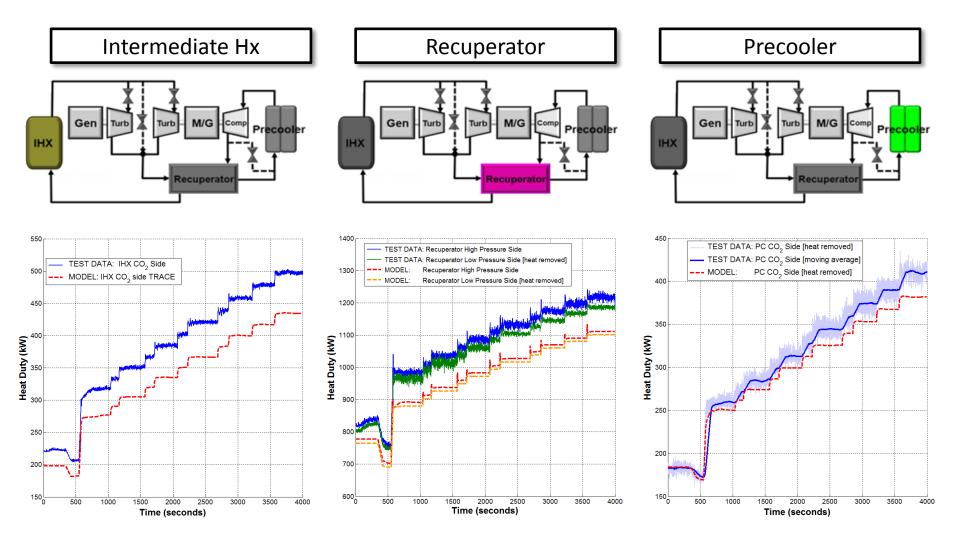
Power Increase Transient: Turbine Generator Power



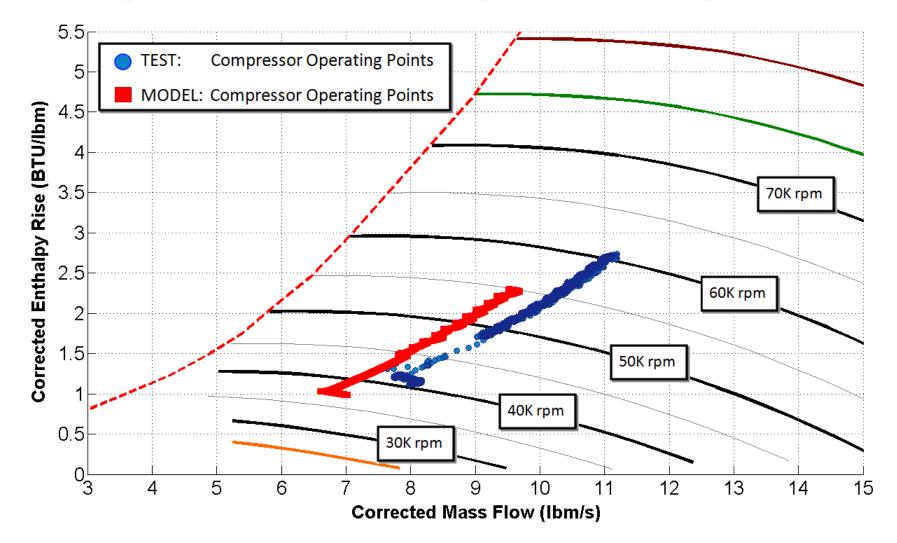
Power Increase Transient: Cooling Water Control Valve Position, Flow Rate and Compressor Inlet Temperature



<u>Power Increase Transient</u>: Heat Exchanger Heat Duties



<u>Power Increase Transient:</u> Comparison of Compressor Operation



Factors that Influence Runtime

<u>CPU time</u> (clock time) is a function of

- Computer Hardware (RAM speed, etc.)
- Model Complexity
 - Component nodalization
 - Fluid property models and interrogation (PG-1[®], Water, CO₂, etc.)
- Transient Rate of Change
 - Heat up/Power Transients/Turbomachinery startup/etc.
- *Model/Physical time*: time of actual transient (hour heat up)
- Up until now: Model Time << CPU time</p>
 - Root cause largest contributor was fluid property calls
- ➤ Now: Model Time ≈ CPU time
 - <u>Change is the replacement of NIST property calculations with commercial</u> <u>package (FIT) [Northland Numerics]</u>

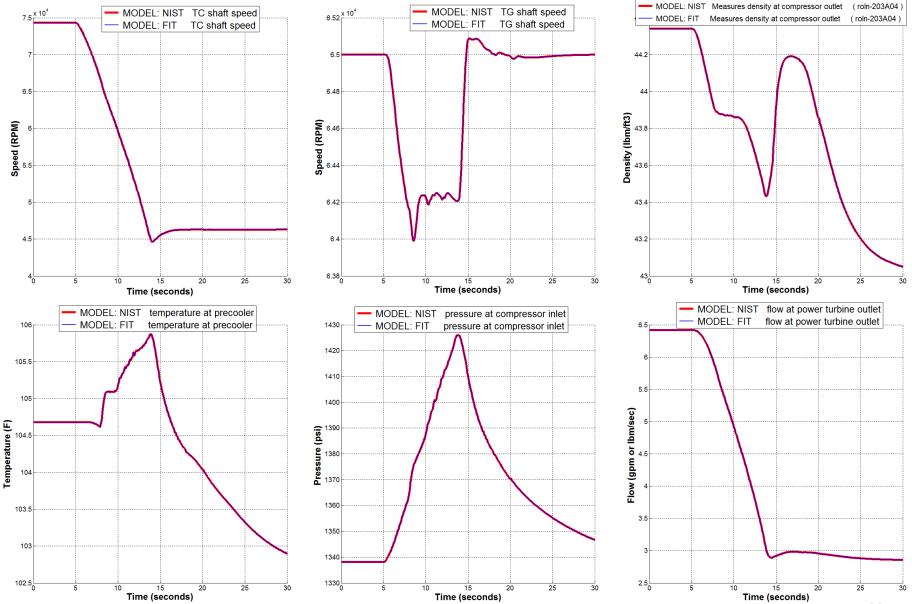
NIST/FIT Comparison: Benchmarking

Suite of 15 transient runs

- Range in duration from 50 to 4000 seconds (physical time)
- Include entire range of operations
 - Cold (150°F) with both shafts off
 - Start up
 - Configuration of CWS
 - Heat up/Power Transients

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Run Name	Run Id	Model Run Description	model time (seconds)	NIST CPU time (seconds)	NIST to Real Time	FIT CPU time (seconds)	FIT to Real Time
IST_v4p017_START_TG65K.med	START	Model startup at full power conditions. Thot = 570F.	50	495	9.91	63	1.26
Rs1ss_THL_TG65K	Restart 1	Reduce TG speed to 65krpm. CCV4 open from 0.00 to 0.06	400	3006	7.51	358	0.90
Rs2ss_Speed_TG65K	Restart 2	Control switches changed to transition from T/H LEAD to SPEED ctrl.	400	3444	8.61	397	0.99
Rs3DP_10pps_MG_TG65K	Restart 3	Down power. Recirculation valve open from 0.06 to 0.59.	400	4126	10.32	461	1.15
Rs4DP_HIdle_CD300_MG_TG65K	Restart 4	TC speed dropped to idle then Thot reduced from 570F to 300F.	3700	31300	8.46	3530	0.95
Rs5_CD150_MG_TG65K	Restart 5	Cool down from 300F to 150F with TC/TG idle.	3700	33377	9.02	3521	0.95
Rs6CWS_OL_lloop_Cidle	Restart 6	Configure CWS to heating mode (isolate inner loop and start Pump1)	400	4777	11.94	510	1.28
Rs7S1S2SD_150F_CWS100F	Restart 7	TC and TG shut down from idle. Turbine inlet T = 150F.	200	2011	10.05	249	1.24
Rs8S1S2SU_150F	Restart 8	TC and TG start up from 0 rpm. Turbine inlet T = 150F.	120	1838	15.31	218	1.82
Rs9ILoopSD_150F	Restart 9	CWS inner loop pump ON to OFF. CWS to cooling config.	240	3044	12.69	353	1.47
Rs10_WCV3auto_Cidle	Restart 10	Transition to cold idle. Comp inlet temp 100F. WCV3 in auto.	1400	13694	9.78	1321	0.94
Rs11HU300F_1Hr_TG65Ktab	Restart 11	Brayton loop heated to 300F from cold idle.	4000	36197	9.05	3790	0.95
Rs12HU435F_1Hr_TG65Ktab	Restart 12	Brayton loop heated to 435F from 300F.	4000	34304	8.58	3786	0.95
Rs13HU540F_1Hr_TG65Ktab	Restart 13	Brayton loop heated to 540F from 435F.	4000	39875	9.97	3852	0.96
Rs14_TCTG55K_540F_TG65Ktab	Restart 14	Raise TC and TG speeds from idle to 55 krpm.	300	3080	10.27	299	1.00

Transient Comparisons: NIST vs. FIT



Summary

> TRACE has been demonstrated as an effective tool for S-CO₂ Brayton analysis

- SNAP GUI/AptPlot enables
 - efficient model building
 - interpretation of results (animation views)
- predicts loop steady state conditions
- transient predictions support control system development and operation
- minimizes risks (trial and error approach) during testing

➢ High fidelity transient modeling on a PC can approach real time execution by replacing NIST REFPROP with Northland Numerics FIT

- > IST transient model still evolving: as-designed \rightarrow as-built \rightarrow as-tested
 - Update performance maps
 - Update windage correlation
 - Update component performance (e.g. valve C_{SUBV}, Hx's dP)

Future: complete qualification of TRACE code for use as an effective tool for scale-up designs