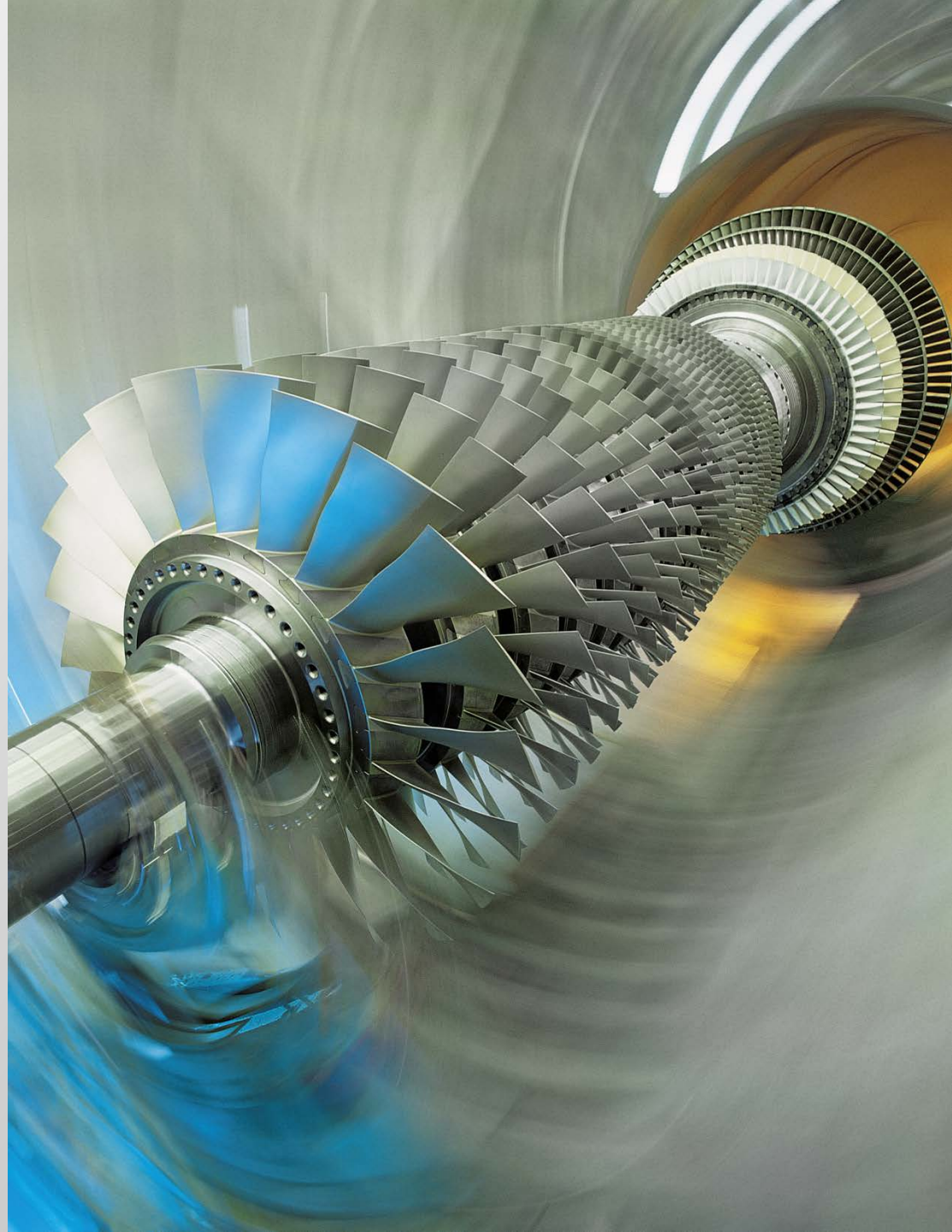




Technology Needs for Fossil Fuel Supercritical CO₂ Power Systems

**Pete Strakey, Omer Dogan,
Gordon Holcomb and Geo
Richards**

4th International Symposium
Supercritical CO₂ Power
Cycles, Sep. 9-10, 2014,
Pittsburgh, PA.



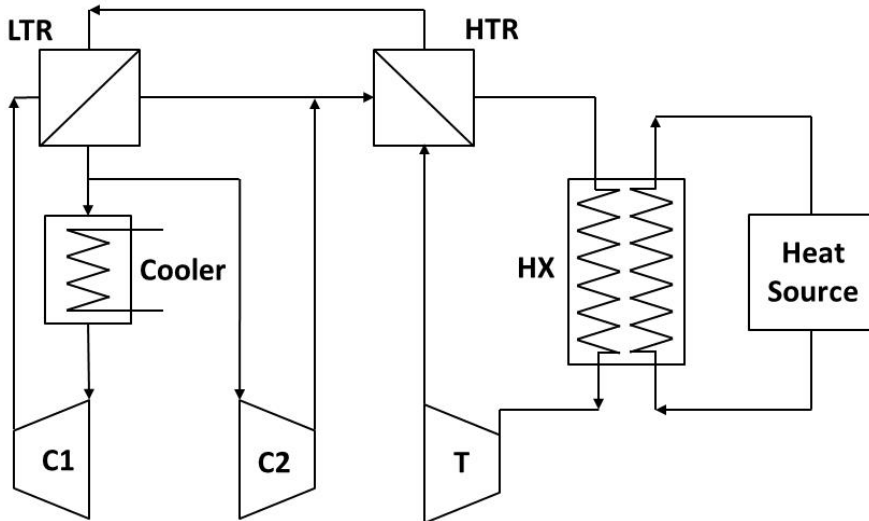
U.S. DEPARTMENT OF

ENERGY

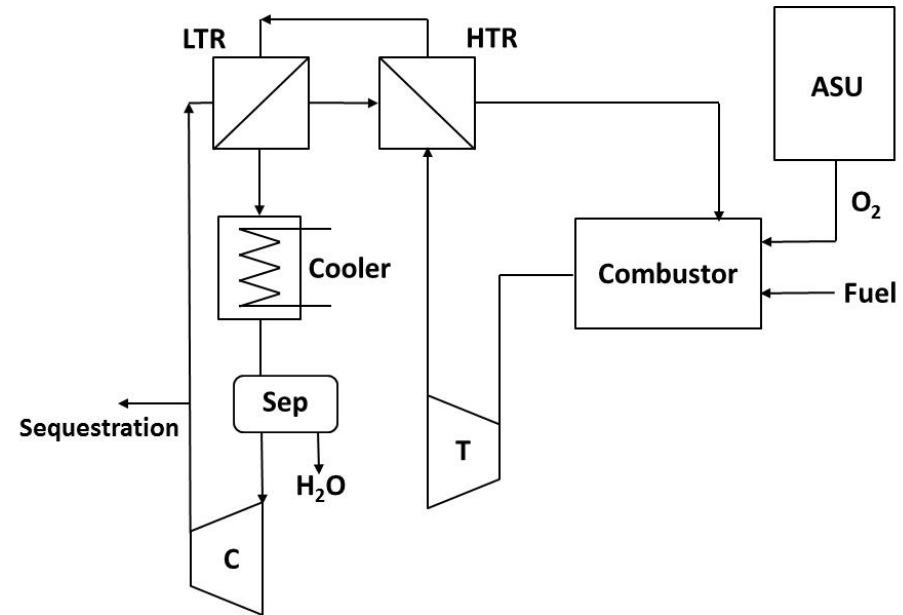
National Energy
Technology Laboratory

sCO₂ Cycles for Fossil Energy

Indirect or "Closed" Recompression Cycle



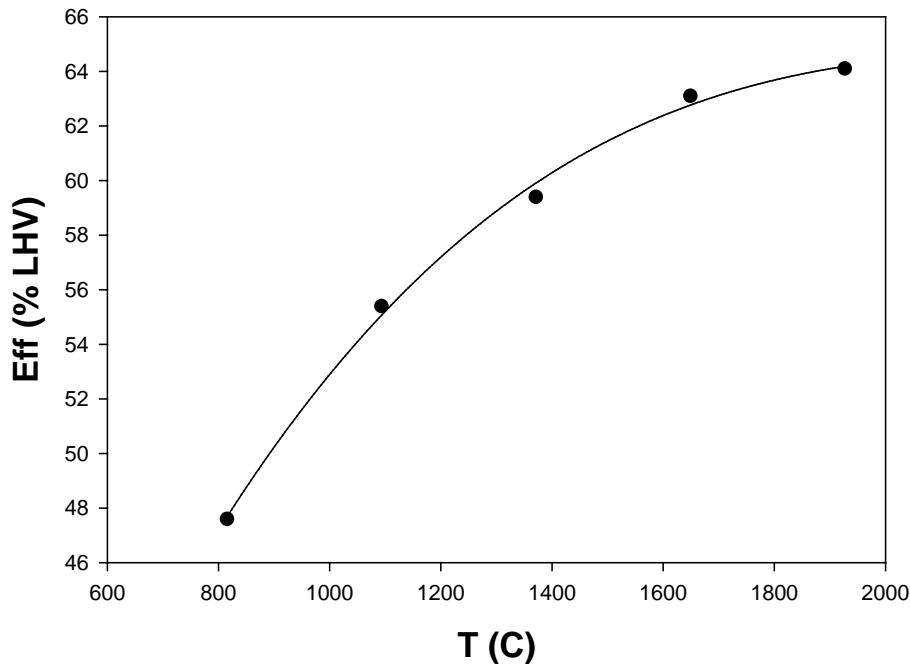
Direct or "Open" Simple Cycle



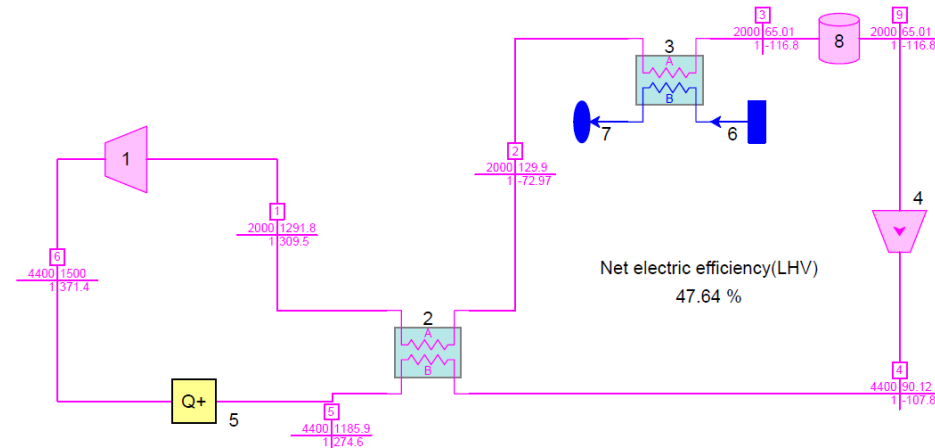
- Both Closed and Open cycles being investigated.
 - Open cycles attractive due to potential for higher TiT (>700°C).
 - Open cycle is also well suited for carbon capture and sequestration.

Effect of Turbine Inlet Temperature on Cycle Efficiency

Simple Recuperated sCO₂ Cycle
Pr=2.2, Pmax=4400 psi



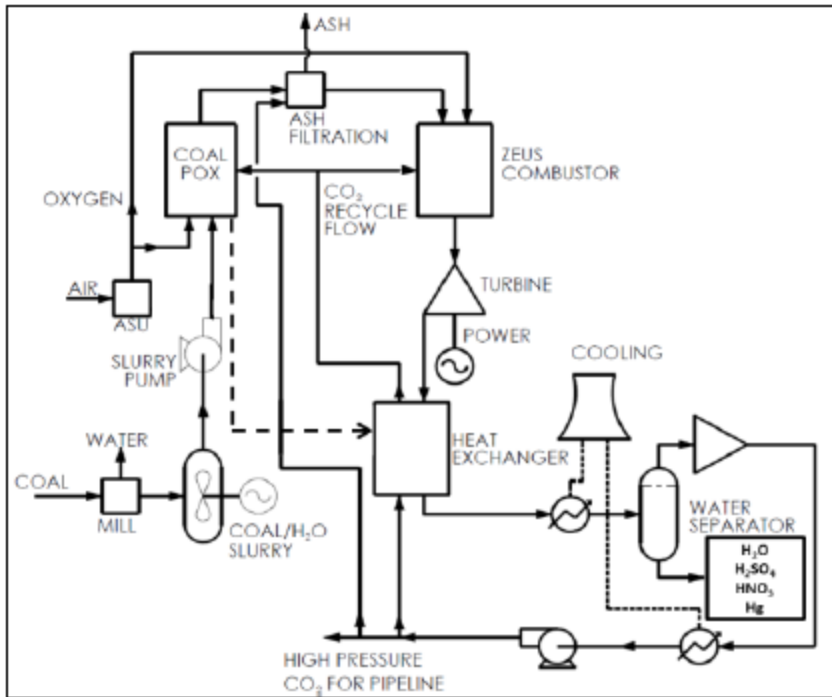
Closed, Recuperated
T_b=18 °C
Pmax=4400 psi
Pr=2.2



- Significant efficiency gains observed up to 2000°C

Recuperators

- Compact heat exchangers are the favored technology.
- At 2000°C turbine inlet temperature the recuperator inlet temperature would be around 1500°C!
- For coal syngas applications the recuperator would see H_2SO_4 and HNO_3 along with H_2O .



Netpower Coal Cycle (Energy Procedia, 37, 2013, pp. 1135-1149)



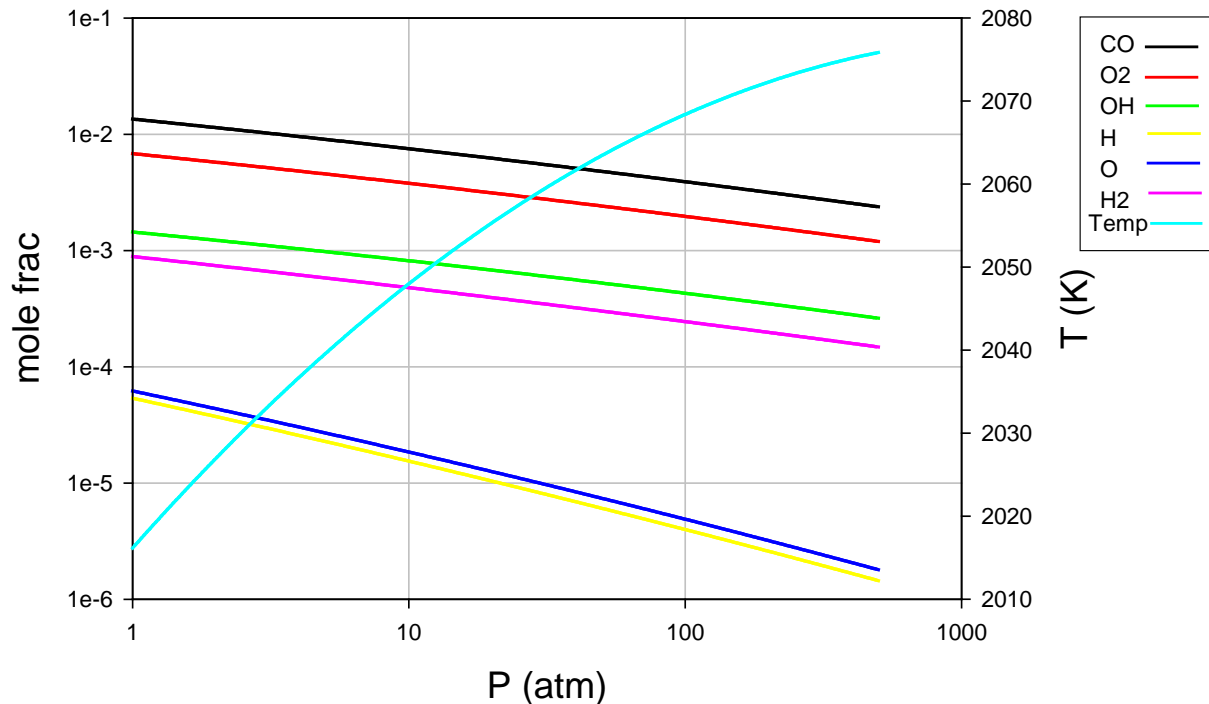
several micro channel heat exchanger designs...

Combustion Dynamics

- High energy release density of $s\text{CO}_2$ oxy-fuel combustor more like a rocket engine than a gas turbine.
- Rocket engines have a long history of dynamics problems.
- Resonant frequency inversely proportional to combustor size.
 - Small combustor = high resonant frequency and large dampening.
 - Rocket engine most damaging frequencies in the 1-10 kHz range due to transverse modes.
- Saturn F-1 instability required 750 full scale tests to solve at \$1M/test.



Combustion Kinetics



*Equilibrium calculation
for stoichiometric
 $\text{CH}_4/\text{O}_2/\text{CO}_2$ mixture*

- Increasing pressure shifts equilibrium to product side through 3-body recombination reactions.
- Most methane oxidation models based on GRI Mech, which is only validated below 10 atm.
- Direct fired system combustor pressure as high as 300 bar!
 - Uncertainty in heat release rates, CO concentration ...

Combustion CFD Modeling

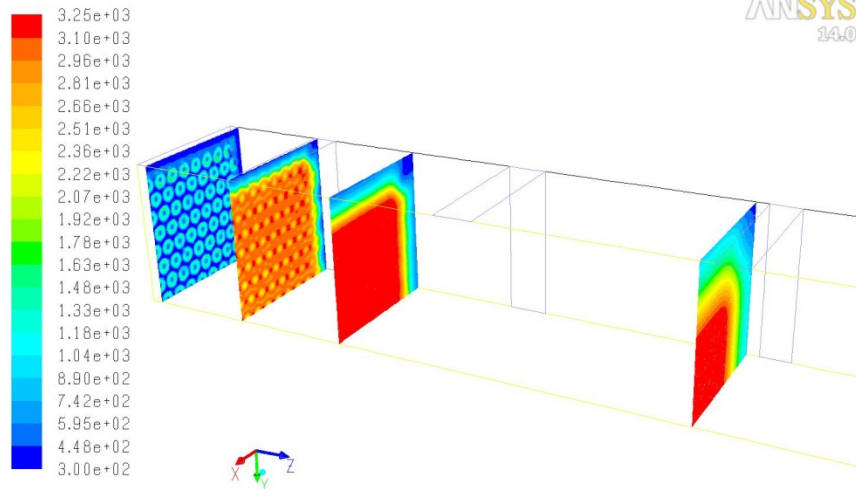
300 bar, 1MW

CH₄/O₂/CO₂

Coax array injector

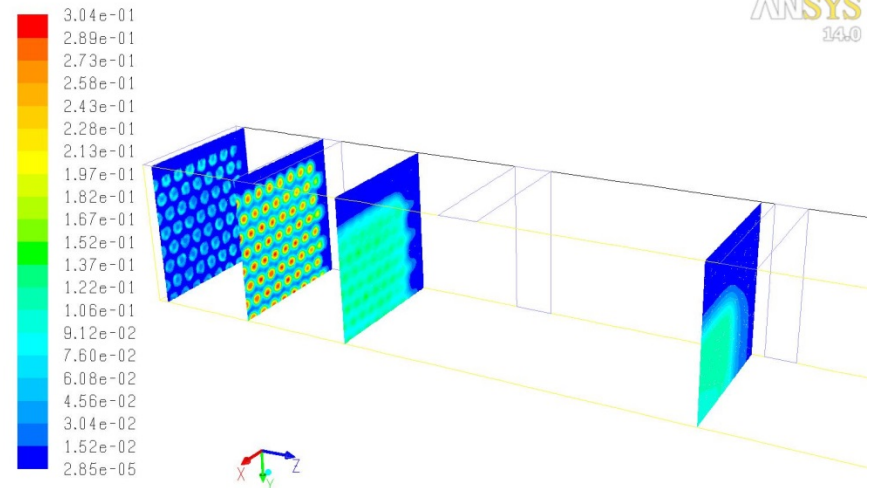
Detailed chemistry

Slot injection wall Cooling



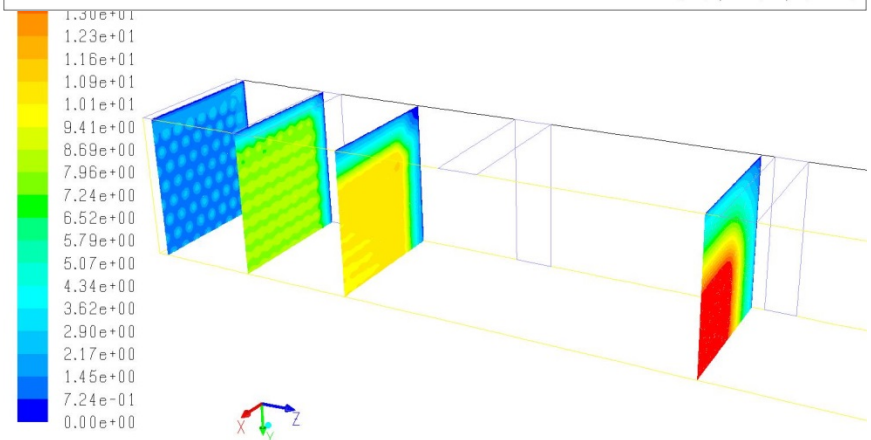
Contours of Static Temperature (k)

Sep 03, 2014
ANSYS FLUENT 14.0 (3d, pbns, spe, ske)



Contours of Mass fraction of co

Sep 03, 2014
ANSYS FLUENT 14.0 (3d, pbns, spe, ske)



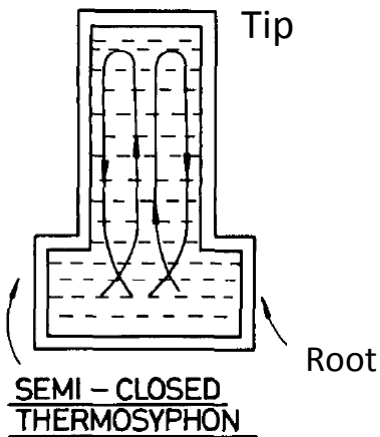
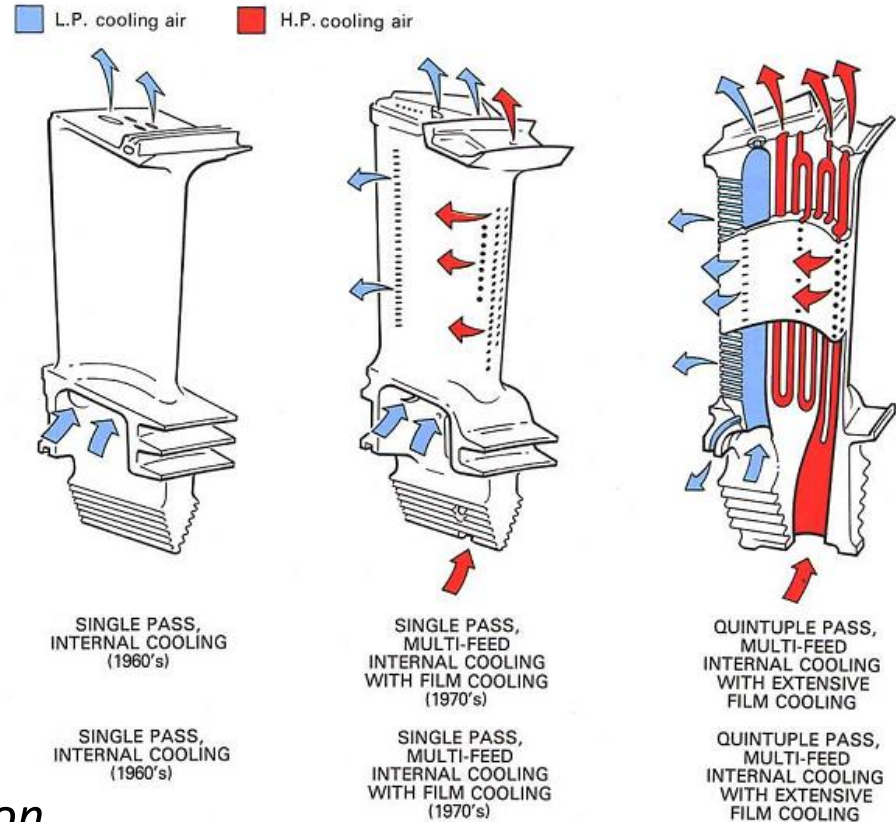
Contours of Z Velocity (m/s)

Sep 03, 2014
ANSYS FLUENT 14.0 (3d, pbns, spe, ske)

CFD used to assess pressure effects on injector mixing, chemistry and wall cooling.

Turbine Blade Cooling

- Turbine inlet temperatures much above 700 C require cooling strategies.
 - Internal or regen cooling with CO₂ attractive for sCO₂ cycles.
- Thermosyphon might be an option for rotating blades.

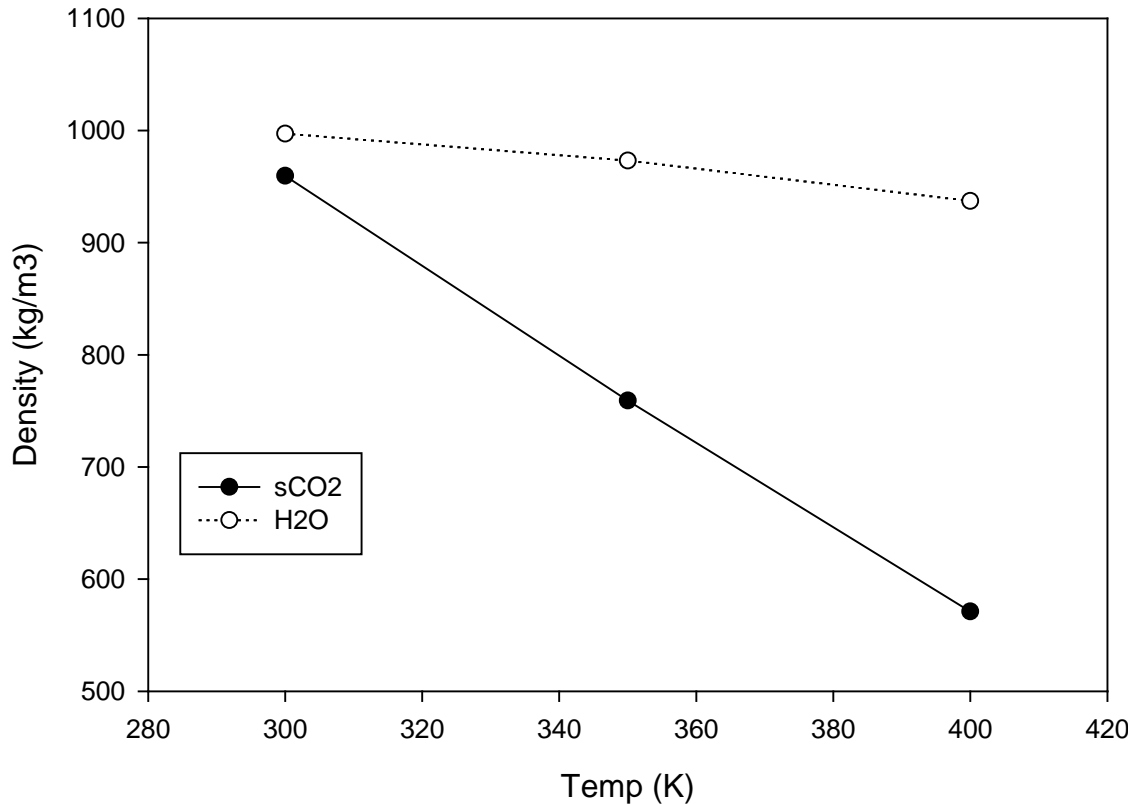


Potential Issues

- *Fouling and corrosion.*
- *Heat and efficiency loss to coolant.*
- *Manufacturing (blind holes, welding, etc.).*
- *Blade failure (cracking, leaking).*
- *Manifolding and sealing on rotating parts.*

sCO₂ Properties vs. H₂O (l)

Density of CO₂ @ 300 bar vs H₂O



T=300K	sCO ₂ @300 bar	H ₂ O (l)
C _p (J/Kg°K)	1919	4179
k (w/m°K)	120 e-3	613 e-3
μ (m ² /s)	109 e-6	855 e-6
Pr # (ν/α)	1.75	5.83

- Much higher temperature dependence for sCO₂ means larger thermosyphon effect. Centripetal acceleration: $a_c = (2\pi\omega)^2 r$, $dp = \rho(r)(2\pi\omega)^2 r dr$ ($\omega = \text{rev/s}$). @40,000 rpm & $r = 10$ cm $a_c = 180,000$ g's

CFD Modeling of Blade Cooling

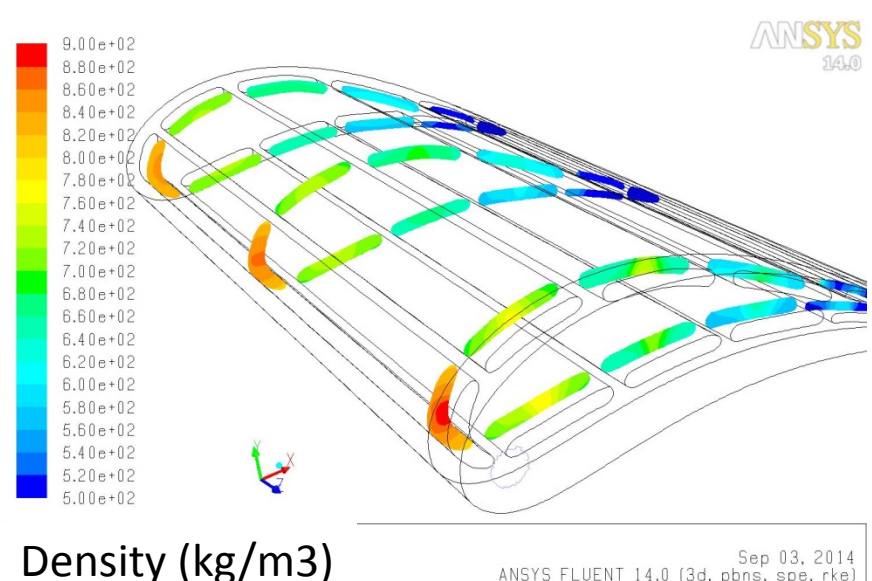
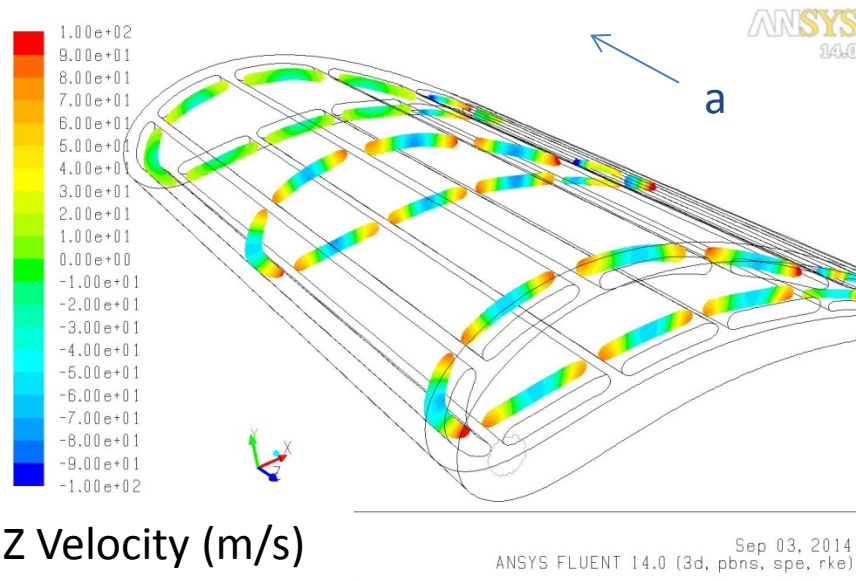
1" long airfoil

1.5 M Cells

Hot Gas: 300 bar, 1400K, 150 m/s

Coolant: sCO₂ @ 300 bar, 300K

Acceleration: 1e6 g's

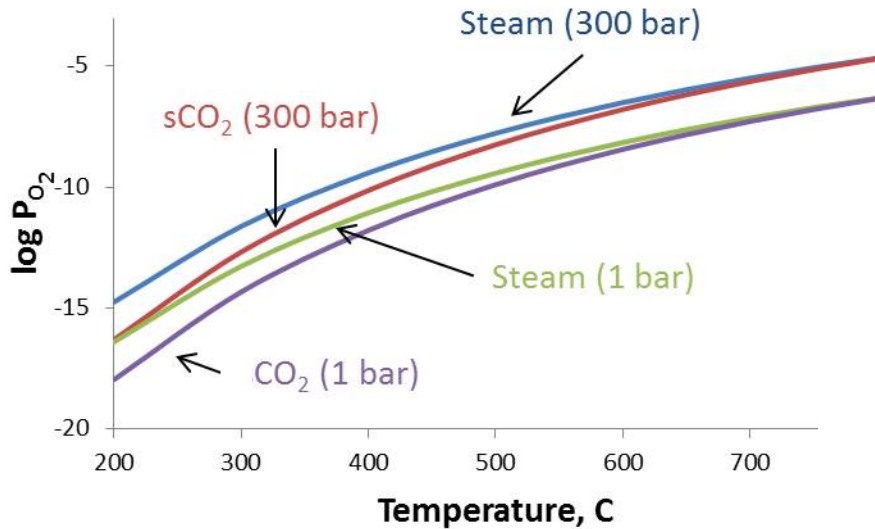


Thermosyphon effect observed to be very strong for sCO₂: excellent heat transfer.

Materials Issues in sCO₂ Service

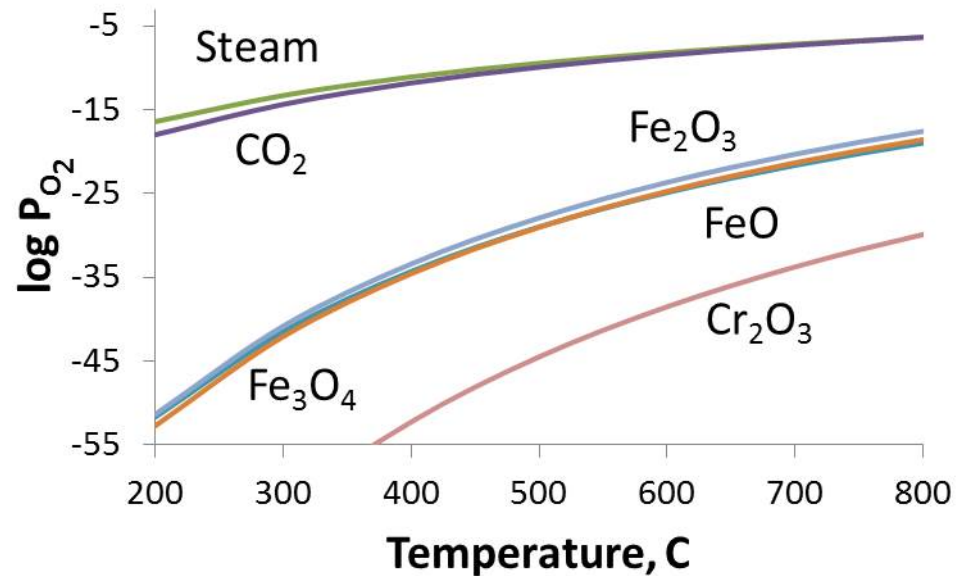
- High-temperature oxidation
- Carburization
- Low cycle fatigue and creep-fatigue (effect of oxidation on the crack surface mechanical behavior)

Oxidizing Potentials Steam vs. CO₂



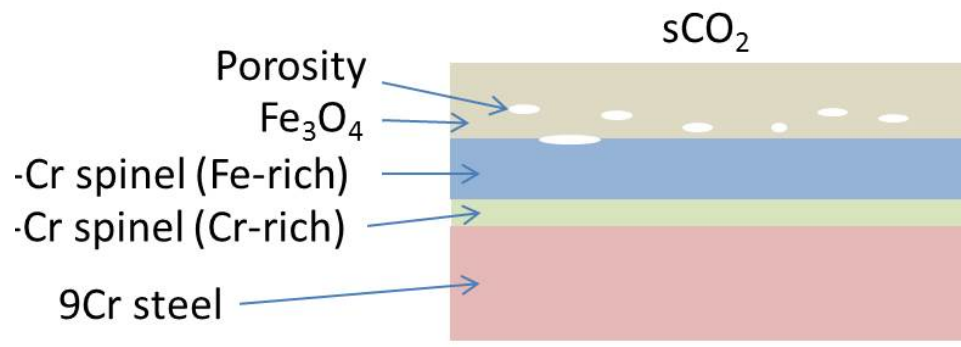
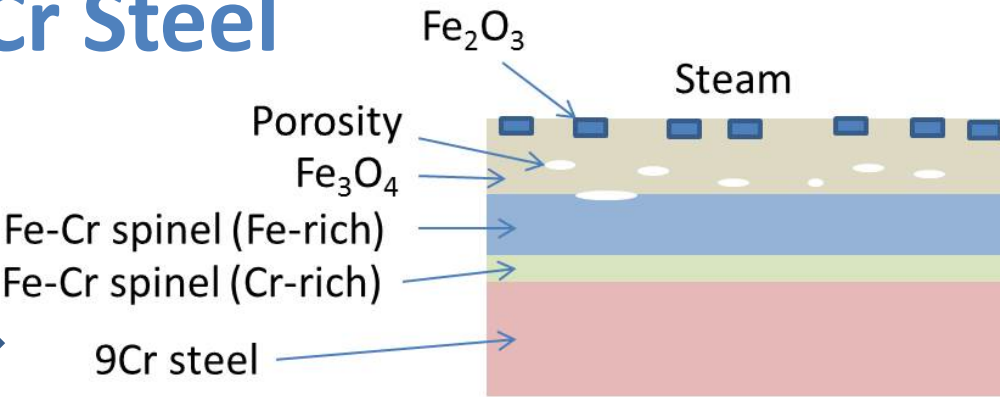
$H_2O = H_2 + \frac{1}{2} O_2$	$\Delta G^\circ \text{ (J/mol)} = 239,500 - 8.14T \ln T + 9.25T$
$CO_2 = CO + \frac{1}{2} O_2$	$\Delta G^\circ \text{ (J/mol)} = 282,400 - 86.81T$

- Oxidizing potentials of steam and CO₂ are similar.
- pO₂ in both steam and CO₂ is much higher than required for relevant oxidation mechanisms.

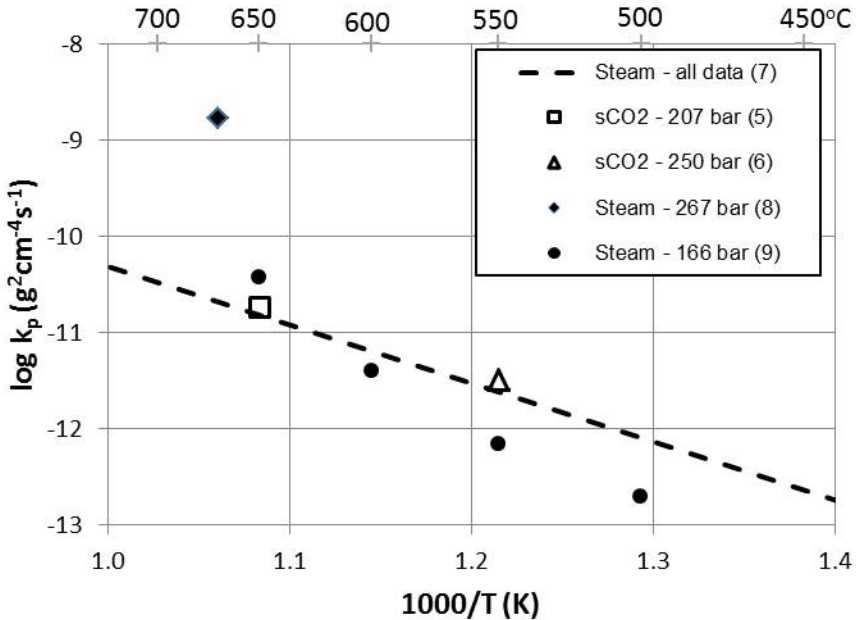


Ferritic/Martensitic 9Cr Steel

Oxidation Products on 9Cr Steels in Steam and CO₂



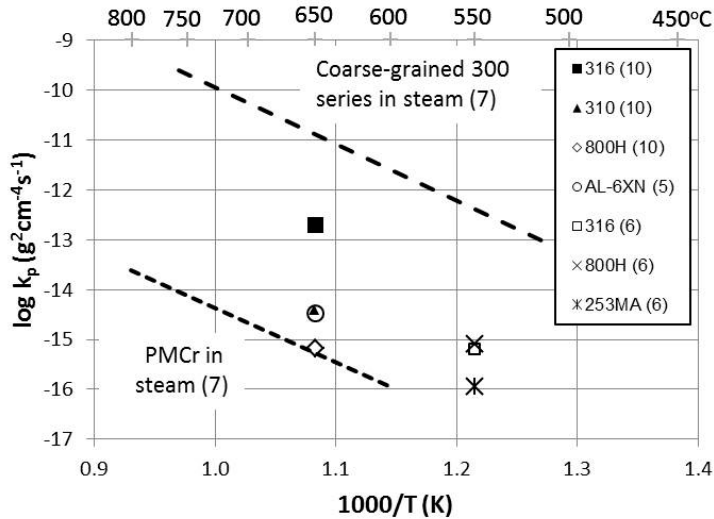
Note – exposure times for CO₂ short (~400 hrs)



Oxidation Kinetics of 9Cr Steels in Steam and CO₂

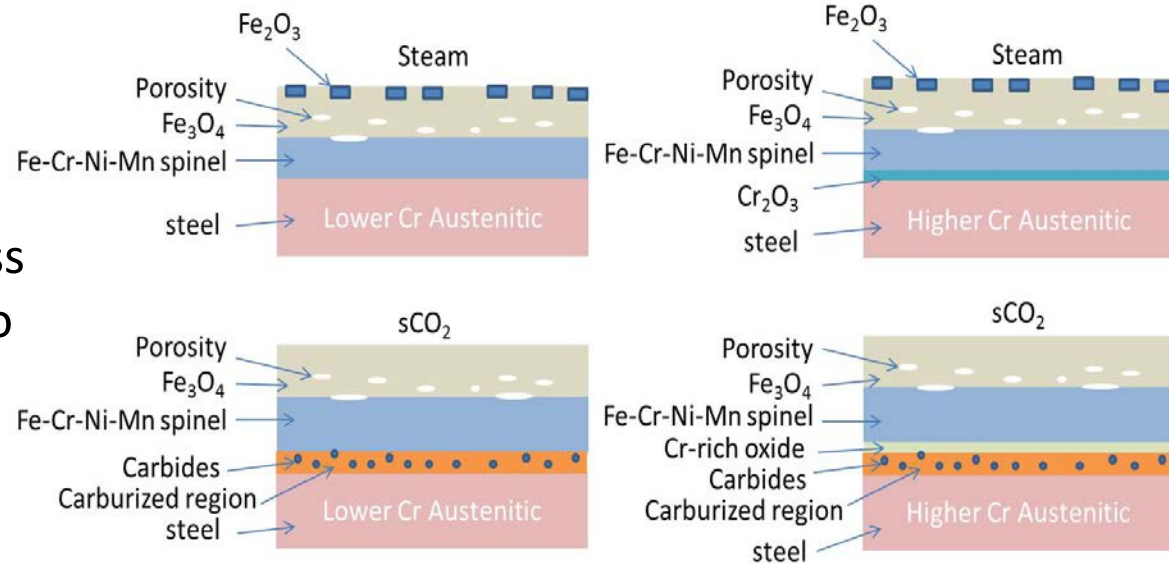
$k_p = \Delta W^2 / 2t$, where ΔW is mass gain and t is time of exposure

Austenitic Steels



Oxidation Kinetics of Austenitic Steels in Steam and CO_2

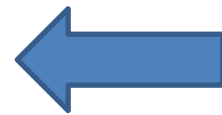
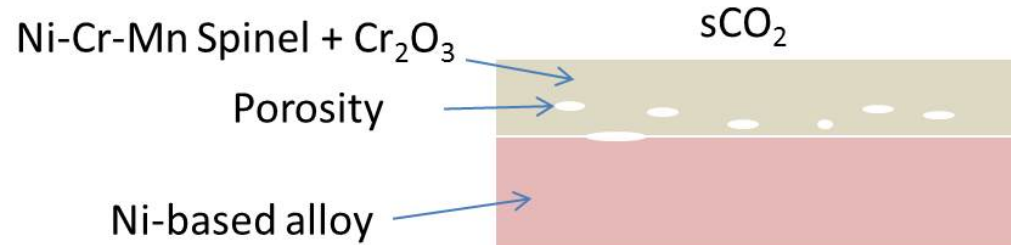
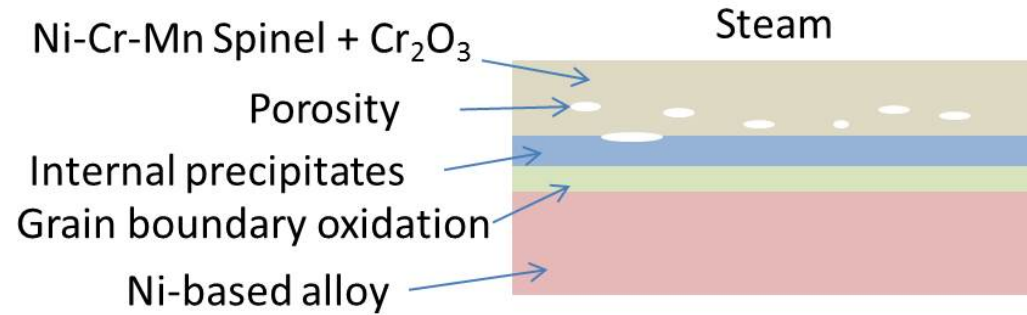
Oxidation Products on Austenitic Steels in Steam and CO_2



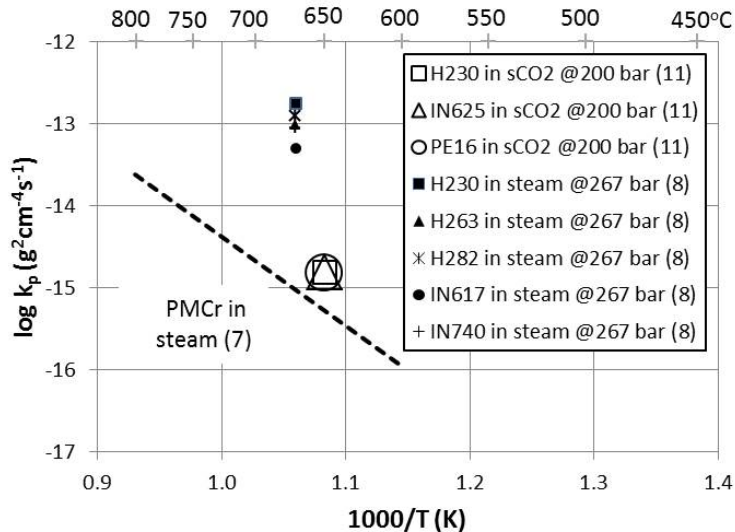
- 316 ss demonstrates fastest oxidation in sCO_2 .
- High Cr steels exhibit much less mass gain in sCO_2 compared to 316.
- Carbided layer forms below oxide layers for sCO_2 .

Nickel Based Alloys

Oxidation Products on Ni-Based Alloys in Steam and CO₂



Oxidation Kinetics of Ni-Based Alloys in Steam and CO₂

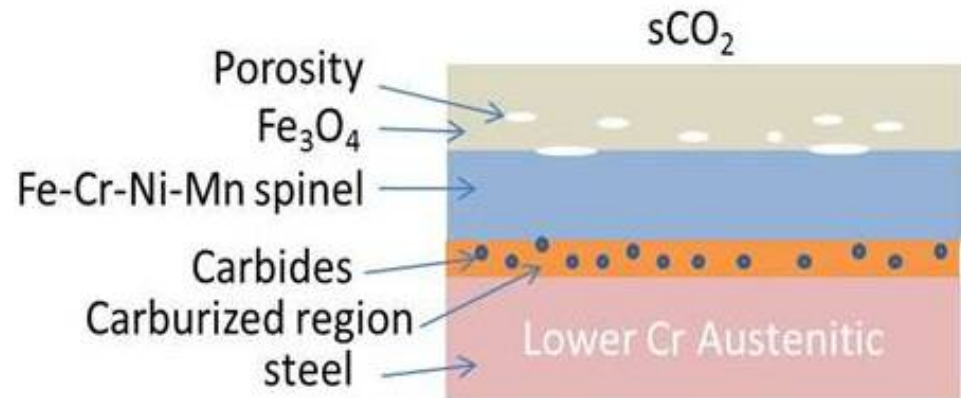


- Ni-based alloys generally show much less mass gain in sCO₂ compared to steam at 650 C.
- No internal oxidation observed for sCO₂ exposure. Could be due to relatively short exposure (~3000 hrs).

Carburization

- The free carbon on the alloy surface can reach the scale-alloy interface via cracks and grain boundaries in the scale and either dissolve or form carbides in alloys.
- Carburization of 9Cr-1Mo steel increases with pressure from 1 bar to 250 bars in CO₂ at 550°C.
- Increasing pressure increases the deposition of carbon in the inner spinel scale.

Need more data with long term exposure!



Low Cycle Fatigue and Creep-Fatigue

- Given that $s\text{CO}_2$ is an effective oxidizer, it is expected that exposure of power plant materials to the $s\text{CO}_2$ conditions will influence their LCF and creep-fatigue life. However, there are no reports of investigation of this subject in the open literature.
- Intergranular crack initiation can be facilitated if the grain boundaries near the stress concentration are oxidized.
- The effect of oxidation in the crack propagation stage is also observed. Oxidation-assisted intergranular crack growth occurs if the cyclic oxidation damage is greater than the fatigue damage.

Need more data with long term exposure!

Conclusions

- Some significant technology challenges need to be addressed for FE based sCO₂ power cycles.
 - Recuperators
 - Combustion
 - Turbine cooling
 - Materials
- Good news is that none appear to be show stoppers!